## **Electronic Supplementary Information**

## Exact calculation of corrosion rates by the weight-loss method

Francisco Malaret,\*

\* Research and Development Centre at Nanomox Ltd. 21 Albemarle St. London W1S 4BS, United Kingdom. <u>francisco.malaret@gmail.com</u>

Dissolution profile of regular n-gonal prism



**Figure S1.** Symbol nomenclature for cylindrical and rectangular objects and cross-section of a regular n-gonal prism.



**Figure S2.** Initial gradients  $(\Delta A/A_0)/(\Delta m/m_0)$  as a function of the s/h ratio for dissolving square prisms calculated with arbitrary values: initial area of 1 cm<sup>2</sup>,  $\rho$  = 7.05 g/cm<sup>3</sup>, CR of 0.1 cm/y. Nota bene: initial surface area, density and CR do not affect the results, as the values in the plot are relatives.

| Designation    | Title  |  |  |  |  |  |
|----------------|--|--|--|--|--|--|
| ASTM G31       | Standard Practice for Laboratory Immersion Corrosion Testing of Metals   |  |  |  |  |  |
| ASTM G48       | Standard Test Methods for Pitting and Crevice Corrosion Resistance of Stainless Steels and Related Alloys by Use of Ferric Chloride Solution                       |  |  |  |  |  |
| ASTM G36       | Standard Practice for Evaluating Stress-Corrosion-Cracking Resistance of Metals and Alloys in a Boiling Magnesium Chloride Solution                                |  |  |  |  |  |
| ASTM G49       | Standard Practice for Preparation and Use of Direct Tension Stress-<br>Corrosion Test Specimens  |  |  |  |  |  |
| ASTM G30       | Standard Practice for Making and Using U-Bend Stress-Corrosion Test Specimens  |  |  |  |  |  |
| ASTM G38       | Standard Practice for Making and Using C-Ring Stress-Corrosion Test Specimens  |  |  |  |  |  |
| ASTM G41       | Standard Practice for Determining Cracking Susceptibility of Metals Exposed<br>Under Stress to a Hot Salt Environment  |  |  |  |  |  |
| ASTM G44       | Standard Practice for Exposure of Metals and Alloys by Alternate Immersion in Neutral 3.5% Sodium Chloride Solution  |  |  |  |  |  |
| ASTM G78       | Standard Guide for Crevice Corrosion Testing of Iron-Base and Nickel-Base<br>Stainless Alloys in Seawater and Other Chloride-Containing Aqueous<br>Environments    |  |  |  |  |  |
| ASTM G35       | Standard Practice for Determining the Susceptibility of Stainless Steels and Related Nickel-Chromium-Iron Alloys to Stress-Corrosion Cracking in Polythionic Acids |  |  |  |  |  |
| NACE MR0174-95 | Recommendations for Selecting Inhibitors for Use as Sucker-Rod Thread Lubricants   |  |  |  |  |  |
| NACE TM0198-98 | Slow strain rate test method for screening corrosion-resistant alloys for stress corrosion cracking in sour oilfield service                                       |  |  |  |  |  |
| NACE TM0169    | Laboratory Corrosion Testing of Metals   |  |  |  |  |  |
| NACE TM0171    | Autoclave corrosion testing in high-temperature water  |  |  |  |  |  |
| USFS 5100      | Standard Test Procedures For the Evaluation of Wildland Fire Chemical<br>Products  |  |  |  |  |  |
| NACE TM0177    | Standard Practice for Determining the Susceptibility of Stainless Steels and Related Nickel-Chromium-Iron Alloys to Stress-Corrosion Cracking in Polythionic Acids |  |  |  |  |  |

 Table S1. Partial List of Standardized Immersion Tests (Kutz 2005).

**Table S2.** Relative errors in the corrosion rate as a function of the mass loss fraction if Eq. 1 is used (constant area), calculated with arbitrary values: initial area of 1 cm2,  $\rho$  = 7.05 g/cm3, CR of 0.1 cm/y. Nota bene: initial surface area, density and CR do not affect the results, as the values in the plot are relatives.

| uo                  |       | Error [%] |      |      |      |      |      |      |      |       |  |  |  |  |
|---------------------|-------|-----------|------|------|------|------|------|------|------|-------|--|--|--|--|
| lass<br>ss<br>actic | s/h   |           |      |      |      |      |      |      |      |       |  |  |  |  |
| E 5 E               | 0.001 | 0.01      | 0.1  | 0.5  | 1    | 2    | 8    | 10   | 100  | 1000  |  |  |  |  |
| 0.01                | 0.3   | 0.3       | 0.3  | 0.4  | 0.4  | 0.4  | 0.2  | 0.2  | 0.02 | 0.002 |  |  |  |  |
| 0.02                | 0.6   | 0.6       | 0.6  | 0.7  | 0.7  | 0.7  | 0.4  | 0.3  | 0.04 | 0.004 |  |  |  |  |
| 0.03                | 0.8   | 0.8       | 0.9  | 1.0  | 1.1  | 1.0  | 0.5  | 0.5  | 0.06 | 0.006 |  |  |  |  |
| 0.04                | 1.1   | 1.1       | 1.1  | 1.4  | 1.4  | 1.3  | 0.7  | 0.6  | 0.08 | 0.008 |  |  |  |  |
| 0.05                | 1.3   | 1.3       | 1.4  | 1.7  | 1.7  | 1.6  | 0.9  | 0.7  | 0.1  | 0.01  |  |  |  |  |
| 0.06                | 1.6   | 1.6       | 1.7  | 2.0  | 2.1  | 1.9  | 1.0  | 0.9  | 0.1  | 0.01  |  |  |  |  |
| 0.07                | 1.8   | 1.8       | 1.9  | 2.3  | 2.4  | 2.2  | 1.2  | 1.0  | 0.1  | 0.01  |  |  |  |  |
| 0.08                | 2.1   | 2.1       | 2.2  | 2.6  | 2.8  | 2.6  | 1.4  | 1.2  | 0.2  | 0.02  |  |  |  |  |
| 0.09                | 2.4   | 2.3       | 2.5  | 3.0  | 3.1  | 2.9  | 1.6  | 1.3  | 0.2  | 0.02  |  |  |  |  |
| 0.1                 | 2.6   | 2.6       | 2.8  | 3.3  | 3.5  | 3.2  | 1.7  | 1.5  | 0.2  | 0.02  |  |  |  |  |
| 0.11                | 2.9   | 2.9       | 3.1  | 3.6  | 3.8  | 3.6  | 1.9  | 1.6  | 0.2  | 0.02  |  |  |  |  |
| 0.12                | 3.1   | 3.1       | 3.4  | 4.0  | 4.1  | 3.9  | 2.1  | 1.8  | 0.2  | 0.02  |  |  |  |  |
| 0.13                | 3.4   | 3.4       | 3.7  | 4.3  | 4.5  | 4.2  | 2.3  | 1.9  | 0.3  | 0.03  |  |  |  |  |
| 0.14                | 3.7   | 3.7       | 4.0  | 4.7  | 4.9  | 4.6  | 2.4  | 2.1  | 0.3  | 0.03  |  |  |  |  |
| 0.15                | 4.0   | 4.0       | 4.3  | 5.0  | 5.2  | 4.9  | 2.6  | 2.2  | 0.3  | 0.03  |  |  |  |  |
| 0.16                | 4.2   | 4.3       | 4.5  | 5.3  | 5.6  | 5.2  | 2.8  | 2.4  | 0.3  | 0.03  |  |  |  |  |
| 0.17                | 4.5   | 4.5       | 4.9  | 5.7  | 6.0  | 5.5  | 3.0  | 2.5  | 0.3  | 0.03  |  |  |  |  |
| 0.18                | 4.8   | 4.8       | 5.2  | 6.0  | 6.4  | 5.9  | 3.1  | 2.7  | 0.4  | 0.04  |  |  |  |  |
| 0.19                | 5.0   | 5.1       | 5.4  | 6.4  | 6.6  | 6.2  | 3.3  | 2.8  | 0.4  | 0.04  |  |  |  |  |
| 0.20                | 5.3   | 5.4       | 5.8  | 6.7  | 7.0  | 6.6  | 3.5  | 3.0  | 0.4  | 0.04  |  |  |  |  |
| 0.22                | 5.9   | 5.9       | 6.3  | 7.5  | 7.8  | 7.3  | 3.9  | 3.3  | 0.4  | 0.04  |  |  |  |  |
| 0.24                | 6.5   | 6.5       | 7.0  | 8.2  | 8.5  | 8.0  | 4.2  | 3.6  | 0.5  | 0.05  |  |  |  |  |
| 0.26                | 7.0   | 7.1       | 7.6  | 8.9  | 9.3  | 8.7  | 4.6  | 3.9  | 0.5  | 0.05  |  |  |  |  |
| 0.28                | 7.6   | 7.7       | 8.2  | 9.6  | 10.0 | 9.4  | 4.9  | 4.2  | 0.5  | 0.06  |  |  |  |  |
| 0.30                | 8.2   | 8.3       | 8.9  | 10.4 | 10.9 | 10.1 | 5.3  | 4.5  | 0.6  | 0.06  |  |  |  |  |
| 0.35                | 9.7   | 9.8       | 10.5 | 12.3 | 12.8 | 11.9 | 6.2  | 5.3  | 0.7  | 0.07  |  |  |  |  |
| 0.40                | 11.3  | 11.4      | 12.2 | 14.3 | 14.9 | 13.9 | 7.2  | 6.1  | 0.8  | 0.08  |  |  |  |  |
| 0.45                | 13.0  | 13.1      | 13.9 | 16.3 | 17.0 | 15.9 | 8.1  | 6.9  | 0.9  | 0.09  |  |  |  |  |
| 0.50                | 14.7  | 14.8      | 15.8 | 18.5 | 19.3 | 17.9 | 9.1  | 7.7  | 1.0  | 0.10  |  |  |  |  |
| 0.55                | 16.5  | 16.6      | 17.7 | 20.7 | 21.6 | 20.0 | 10.1 | 8.6  | 1.1  | 0.11  |  |  |  |  |
| 0.60                | 18.4  | 18.6      | 19.7 | 23.0 | 24.1 | 22.3 | 11.1 | 9.4  | 1.2  | 0.12  |  |  |  |  |
| 0.65                | 20.5  | 20.6      | 21.9 | 25.5 | 26.7 | 24.7 | 12.1 | 10.3 | 1.3  | 0.13  |  |  |  |  |
| 0.70                | 22.7  | 22.8      | 24.2 | 28.2 | 29.4 | 27.2 | 13.2 | 11.1 | 1.4  | 0.14  |  |  |  |  |
| 0.75                | 25.0  | 25.2      | 26.8 | 31.0 | 32.5 | 29.9 | 14.3 | 12.0 | 1.5  | 0.15  |  |  |  |  |
| 0.80                | 27.7  | 27.9      | 29.5 | 34.2 | 35.8 | 32.8 | 15.4 | 12.9 | 1.6  | 0.16  |  |  |  |  |
| 0.85                | 30.7  | 30.9      | 32.6 | 37.7 | 39.6 | 36.0 | 16.5 | 13.8 | 1.7  | 0.17  |  |  |  |  |
| 0.90                | 34.2  | 34.4      | 36.3 | 41.9 | 44.0 | 39.7 | 17.6 | 14.8 | 1.8  | 0.18  |  |  |  |  |
| 0.95                | 38.9  | 39.1      | 41.1 | 47.3 | 49.9 | 44.1 | 18.8 | 15.7 | 1.9  | 0.19  |  |  |  |  |

$$V = \frac{1}{4}n \cdot s^2 \cdot h \cdot \cot(\pi/n)$$
 Eq. S1

$$s = 2 \cdot r \cdot \tan(\pi/n)$$
 Eq. S2

$$\frac{\partial V}{\partial t} = \frac{\partial V}{\partial s} \cdot \frac{\partial s}{\partial r} \cdot \frac{\partial r}{\partial t} + \frac{\partial V}{\partial h} \cdot \frac{\partial h}{\partial t}$$
 Eq. S3

$$\frac{\partial r}{\partial t} = -CR \qquad \qquad \text{Eq. S4}$$

$$\frac{\partial h}{\partial t} = -2CR \qquad \qquad \text{Eq. S5}$$

$$\frac{\partial V}{\partial s} = \frac{\partial}{\partial s} \left( \frac{1}{4} n \cdot s^2 \cdot h \cdot \cot\left(\frac{\pi}{n}\right) \right) = \frac{1}{2} n \cdot s \cdot h \cdot \cot\left(\frac{\pi}{n}\right)$$
Eq. S6

$$\frac{\partial s}{\partial r} = \frac{\partial}{\partial r} (2 \cdot r \cdot \tan(\pi/n)) = 2 \cdot \tan(\pi/n)$$
 Eq. S7

$$\frac{\partial V}{\partial h} = \frac{\partial}{\partial h} \left( \frac{1}{4} n \cdot s^2 \cdot h \cdot \cot\left(\frac{\pi}{n}\right) \right) = \frac{1}{4} n \cdot s^2 \cdot \cot\left(\frac{\pi}{n}\right)$$
 Eq. S8

$$\frac{\partial V}{\partial t} = \frac{1}{2}n \cdot s \cdot h \cdot \cot(\frac{\pi}{n}) \cdot 2 \cdot \tan(\frac{\pi}{n}) \cdot (-CR) + \frac{1}{4}n \cdot s^{2}$$
  
$$\cdot \cot(\frac{\pi}{n}) \cdot (-2CR)$$
Eq. S9

$$\frac{\partial V}{\partial t} = -CR \cdot n \cdot s \cdot h - \frac{1}{2} \cdot CR \cdot n \cdot s^2 \cdot \cot(\frac{\pi}{n})$$
 Eq. S10

$$s(t) = s_0 - 2RC \cdot \tan(\pi/n) \cdot t \qquad \qquad \text{Eq. S11}$$

$$h(t) = h_0 - 2RC \cdot t \qquad \qquad \text{Eq. S12}$$

$$\frac{\partial V}{\partial t} = -CR \cdot n \cdot (s_0 - 2RC \cdot t) \cdot (h_0 - 2RC \cdot t) - \frac{1}{2} \cdot CR$$
  
$$\cdot n \cdot (s_0 - 2RC \cdot t)^2 \cdot \cot(\frac{\pi}{n})$$
 Eq. S13

$$\frac{\partial V}{\partial t} = (-6 \cdot CR^3 \cdot n \cdot \tan(\pi/n)) \cdot t^2 + (2 \cdot CR^2 \cdot n \cdot h_0 \cdot \tan(\pi/n) + 4 \cdot CR^2 \cdot n \cdot s_0) \cdot t - CR \cdot n \cdot h_0 \cdot s_0 - 1/2 \cdot CR \cdot n \cdot s_0^2 \cdot \cot(\pi/n)$$
Eq. S14

$$\int_{V_{ini}}^{V_f} \partial V = \int_{t_{ini}=0}^t (-6 \cdot CR^3 \cdot n \cdot \tan(\pi/n)) \cdot t^2 + (2 \cdot CR^2 \cdot n \cdot h_0 \cdot \tan(\pi/n)) + 4 \cdot CR^2 \cdot n \cdot s_0) \cdot t - CR \cdot n \cdot h_0 \cdot s_0 - 1/2 \cdot CR \cdot n \cdot s_0^2 \cdot \cot(\pi/n) \partial t$$
Eq. S15

$$\int_{V_{ini}}^{V_f} \partial V = V_f - V_{ini} = \Delta V$$
 Eq. S16

$$\int_{t_{ini}=0}^{t} (-6 \cdot CR^{3} \cdot n \cdot \tan(\pi/n)) \cdot t^{2} + (2 \cdot CR^{2} \cdot n \cdot h_{0} \cdot \tan(\pi/n) + 4 \cdot CR^{2} \cdot n \cdot s_{0}) \cdot t - CR \cdot n \cdot h_{0} \cdot s_{0} - \frac{1}{2} \cdot CR \cdot n \cdot s_{0}^{2} \cdot \cot(\pi/n) \partial t = (-2 \cdot n \cdot \tan(\pi/n)) \cdot CR^{3} \cdot t^{3} + (n \cdot h_{0} \cdot \tan(\pi/n) + 2 \cdot n \cdot s_{0}) \cdot CR^{2} \cdot t^{2}$$
 Eq. S17  
 -  $(n \cdot h_{0} \cdot s_{0} + \frac{1}{2} \cdot n \cdot s_{0}^{2} \cdot \cot(\pi/n)) \cdot CR \cdot t$ 

$$\Delta V = \frac{\Delta m}{\rho} = (-2 \cdot n \cdot \tan(\pi/n)) \cdot CR^3 \cdot t^3 + (n \cdot h_0 \cdot \tan(\pi/n) + 2 \cdot n \cdot s_0) \cdot CR^2 \cdot t^2 - (n \cdot h_0 \cdot s_0 + 1/2 \cdot n \cdot s_0^2 \cdot \cot(\pi/n)) \cdot CR \cdot t$$
Eq. S18

$$(-2 \cdot n \cdot \tan{(\pi/n)}) \cdot CR^{3} \cdot t^{3} + (n \cdot h_{0} \cdot \tan{(\pi/n)} + 2 \cdot n \cdot s_{0}) \cdot CR^{2}$$
$$\cdot t^{2} - (n \cdot h_{0} \cdot s_{0} + 1/2 \cdot n \cdot s_{0}^{2} \cdot \cot{(\pi/n)}) \cdot CR \cdot t$$
$$-\frac{\Delta m}{\rho} = 0$$
Eq. S19