# Supplementary Information 

# Quantification of Solid State Impurity with Powder X-ray Diffraction using Laboratory Source 

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## 1. Calculation of degree of crystallinity of BPO

Three sample preparations were analysed in a low background holder by an initial PXRD method (tables S1 and S2). Degree of crystallinity was calculated using EVA software suite (Bruker, DIFFRAC.EVA, User Manual, version 09.2017) as follows:

$$
\% \text { Amorphous }=\frac{\text { Global area }- \text { Reduced area }}{\text { Global area }} \times 100
$$

\% Crystallinity = $100-$ \%Amorphous

Table S1. Degree of crystallinity calculation using EVA v.4.3.0

| Degree of crystallinity of BPO |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| BPO | Preparation-1 | Preparation-2 | Preparation-3 | Average Degree of <br> Crystallinity (\%) |
| \% Crystallinity | 94.7 | 94.6 | 94.1 | 94.47 |

Table S2. Method parameters for initial PXRD method

| Parameter | Parameter Values |
| :--- | :--- |
| Instrument Configuration | Bragg-Brentano geometry (e.g. Theta-theta) |
| Tube | Ceramic X-ray Cu anode (LFF) tube |
| Generator power | $40 \mathrm{kV} / 40 \mathrm{~mA}$ |
| Detector | LYNXEYE |
| Soller slit | axial $2.5^{\circ}$ primary/secondary |
| Divergent slit | $0.3^{\circ}$ primary |
| Active length of detector | $2.949^{\circ} 2 \theta$ |
| Diffracted beam anti scattering slit | 8 mm (not automated) |
| Diffracted beam filter | Nickel $K \beta$ filter |
| Phi rotation (spinner) | On $(15$ rpm) |
| Scan Range | 2 to $40^{\circ} 2 \theta$ |
| Scan mode | Continuous |
| Step size | $0.0388^{\circ} 2 \theta$ |
| Time/Step | 1.0 second |

## 2. Preparation of BPO and API standard mixture

The batch of API used for preparing standard compositions of BPO spiked API samples contained $0.03 \% \mathrm{w} / \mathrm{w}(259 \mathrm{ppm})$ BPO as confirmed by HPLC analysis. Potency of the batch of BPO used for spiking studies was $90 \% \mathrm{w} / \mathrm{w}$. The weight correction to the API and BPO samples were performed as follows:

$$
\text { Weight of BPO in API taken in } \mathrm{mg}=\frac{\text { Weight of API taken } \times \text { Percentage of BPO present in the API }}{100}
$$

The content of BPO in standard mixtures was calculated using the corrected weights of API and BPO:

$$
\text { Content of BPO }\left(\% \frac{\mathrm{w}}{\mathrm{w}}\right)=\frac{\text { Corrected BPO weight in } \mathrm{mg}}{\text { Total weight }} \times \% \text { Potency }
$$

## Table S3. BPO and API stock standard mixture preparation

| Weight <br> of BPO <br> $(\mathbf{m g})$ | Weight of <br> API <br> $(\mathbf{m g})$ | Weight of <br> BPO in API <br> $(\mathbf{m g})$ | Corrected <br> BPO weight <br> $(\mathbf{m g})$ | Corrected <br> API weight <br> $(\mathbf{m g})$ | Total <br> weight <br> $(\mathbf{m g})$ | Content of BPO <br> $(\% \mathbf{w} / \mathbf{w})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101.38 | 893.50 | 0.27 | 101.65 | 893.23 | 994.88 | 9.236 |

## 3. PXRD Method development



Figure S1. PXRD Overlay of $\mathbf{\sim 0 . 4 5 \%} \mathbf{w} / \mathbf{w}$ BPO in API standard mixture analysed with different step times (exposure time, seconds per step) with constant step size of $\mathbf{0 . 0 5}{ }^{\circ}$


Figure S2. PXRD Overlay of $\sim 0.45 \% ~ w / w ~ B P O ~ i n ~ A P I ~ s t a n d a r d ~ m i x t u r e ~ a n a l y s e d ~ w i t h ~$ different step sizes with constant step time of 5 seconds per step


Figure S3. PXRD Overlay of $\mathbf{\sim 0 . 9 0 \%} \mathbf{w} / \mathbf{w}$ BPO in API standard mixture analysed with different divergence slit widths

## 4. Preparation of calibration curve

Table S4. Intensities (areas) of BPO and API peaks and calculation of area ratio for the preparation of calibration curve using different BPO and API standard mixtures



Figure S4. Measurement of BPO and API peak area of a $0.866 \%$ w/w BPO in API standard mixture using MDI JADE v. 9.5.0


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Figure S11. Measurement of API peak area of a $0.027 \% ~ w / w ~ B P O ~ i n ~ A P I ~ s t a n d a r d ~$ mixture using MDI JADE v. 9.5.0

### 4.1. Profile fitting (peak decomposition) analysis

A PXRD pattern from each of the spiking levels was analysed for profile fitting and peak decomposition. It was observed that all the peaks in the range 5-10 $2 \theta$ could be profile fitted satisfactorily for all the samples (Figures S12-S19). The resolution between the two closely spaced peaks namely, a peak at $8.48^{\circ} 2 \theta$ of API and a peak at $8.86^{\circ} 2 \theta$ of BPO was found to be greater than 1 in each case [1]. Area ratios obtained by intensity values from profile fitted peaks are comparable to that obtained from the manual integration and follow similar trend i.e. increase in the area ratio value with increase in BPO spiking concentration (Table S5).

Table S5. Comparison of the area ratios obtained by using intensity values (area under the curve) from profile fitted peaks ( $7.38^{\circ} 2 \theta$ of API and $8.86^{\circ} 2 \theta$ of BPO) and that from manual integration

| S. No. | Sample |  |  |
| :---: | :---: | :---: | :---: |
|  |  | Area ratio |  |
|  | \% w/w BPO in API) | Using intensity value <br> from profile fitted peaks | Using intensity value <br> from manual integration |
| 1 | 0.866 | 0.1299 | 0.1198 |
| 2 | 0.443 | 0.0600 | 0.0592 |
| 3 | 0.340 | 0.0395 | 0.0431 |
| 4 | 0.239 | 0.0318 | 0.0325 |
| 5 | 0.133 | 0.0161 | 0.0168 |
| 6 | 0.099 | 0.0112 | 0.0132 |
| 7 | 0.068 | 0.0072 | 0.0070 |
| 8 | 0.027 | 0 | 0 |

[1] Resolution with next adjacent peak $\left(R_{s}\right)$ was calculated as:

$$
R_{S}=\frac{X_{c 2}-X_{c 1}}{0.5\left(w_{2}+w_{1}\right)}
$$

Where $X_{c 1}$ and $X_{c 2}$ are peak centers, and $w_{1}$ and $w_{2}$ are constructed base widths.


Figure S12. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 8 6 6 \%}$ w/w BPO in API standard mixture sample


Figure S13. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 4 4 3 \%}$ w/w BPO in API standard mixture sample


Figure S14. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 3 4 0 \%}$ w/w BPO in API standard mixture sample


Figure S15. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 2 3 9 \%}$ w/w BPO in API standard mixture sample


Figure S16. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 1 3 3 \%}$ w/w BPO in API standard mixture sample


Figure S17. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 0 9 9 \%}$ w/w BPO in API standard mixture sample


Figure S18. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 0 6 8 \%}$ w/w BPO in API standard mixture sample


Figure S19. Profile fitting (peak decomposition) analysis for a PXRD pattern of $\mathbf{0 . 0 2 7 \%}$ w/w BPO in API standard mixture sample

## 5. PXRD method validation

Table S6. Range studies at $\mathbf{0 . 9 0 \%}$ and $\mathbf{0 . 1 0 \%} \mathbf{w} / \mathrm{w}$ BPO in API standard mixtures

| Range at $0.90 \%$ w/w BPO in API standard mixture |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S.No. | \% w/w of BPO content | Area in counts $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio |
| 1 |  | 1101029 | 150516 | 0.1203 |
| 2 |  | 1103768 | 152452 | 0.1214 |
| 3 | 0.866 | 1106388 | 149215 | 0.1188 |
| 4 | 0.866 | 1104540 | 153624 | 0.1221 |
| 5 |  | 1107447 | 146016 | 0.1165 |
| 6 |  | 1101337 | 144264 | 0.1158 |
| Mean <br> st.DEV <br> \%RSD |  |  |  | 0.119 |
|  |  |  |  | 0.0026 |
|  |  |  |  | 2.18 |
| Range at 0.10\% w/w BPO in API standard mixture |  |  |  |  |
| S.No. | \% w/w of BPO content | Area in counts $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio |
| 1 |  | 1049862 | 15184 | 0.0143 |
| 2 |  | 1058913 | 14908 | 0.0139 |
| 3 | 0.099 | 1052540 | 14603 | 0.0137 |
| 4 |  | 1058293 | 12582 | 0.0117 |
| 5 |  | 1055215 | 13067 | 0.0122 |
| 6 |  | 1045791 | 13837 | 0.0131 |
| Meanst.DEV |  |  |  | 0.013 |
|  |  |  |  | 0.0010 |
| \%RSD |  |  |  | 7.69 |

Table S7. Method precision determined using $\mathbf{0 . 4 5 \%}, \mathbf{0 . 3 5 \%}$ and $\mathbf{0 . 2 5 \%} \mathbf{w} / \mathrm{w}$ BPO in API standard mixtures

| S.No. | $\%$ <br> w/w of BPO <br> content | Area in counts Area in counts <br> at 7.38 <br> $\mathbf{2 \theta} \boldsymbol{\theta}$ <br> at $\mathbf{8 . 8 6}^{\circ} \mathbf{2 \theta}$ | Area ratio | Mean | st.DEV | \%RSD |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 1113860 | 71710 | 0.0605 |  |  |  |
| 2 | 0.443 | 1116109 | 71374 | 0.0601 | 0.060 | 0.001 | $\mathbf{1 . 8 3}$ |
| 3 |  | 1118092 | 69409 | 0.0584 |  |  |  |
| 4 |  | 1090902 | 48456 | 0.0425 |  |  |  |
| 5 | 0.340 | 1117212 | 50965 | 0.0436 | 0.043 | 0.001 | $\mathbf{1 . 8 6}$ |
| 6 |  | 1117067 | 51556 | 0.0441 |  |  |  |
| 7 |  | 1083216 | 38575 | 0.0344 |  |  |  |
| 8 | 0.239 | 1080844 | 34991 | 0.0314 | 0.033 | 0.002 | $\mathbf{4 . 5 5}$ |
| 9 |  | 1082934 | 37228 | 0.0332 |  |  |  |

Table S8. Precision determination for standard mixture corresponding to LOQ ( $\mathbf{0 . 1 3 3 \%}$ w/w BPO in API) and for next available lower level ( $\mathbf{0 . 0 9 9 \%} \mathbf{w / w ~ B P O ~ i n ~ A P I ) ~}$

| 0.133\% w/w BPO in API binary mixture Precision |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| S.No. | \% w/w of BPO content | Area in counts at $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio |
| 1 | 0.133 | 1129288 | 17627 | 0.0154 |
| 2 |  | 1126209 | 20252 | 0.0177 |
| 3 |  | 1126390 | 20565 | 0.0179 |
| 4 |  | 1129758 | 19574 | 0.0170 |
| 5 |  | 1126454 | 18039 | 0.0158 |
| 6 |  | 1096074 | 19306 | 0.0173 |
| Mean st.DEV \%RSD |  |  |  | 0.017 |
|  |  |  |  | $0.0010$ |
|  |  |  |  | 5.88 |
| Limit of Quantification level ( $0.099 \%$ w/w BPO in API binary mixture) precision |  |  |  |  |
| S.No. | \% w/w of BPO content | Area in counts at $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio |
| 1 | $0.099$ | 1049862 | 15184 | 0.0143 |
| 2 |  | 1058913 | 14908 | 0.0139 |
| 3 |  | 1052540 | 14603 | 0.0137 |
| 4 |  | 1058293 | 12582 | 0.0117 |
| 5 |  | 1055215 | 13067 | 0.0122 |
| 6 |  | 1045791 | 13837 | 0.0131 |
| Meanst.DEV |  |  |  | 0.013 |
|  |  |  |  | $0.0010$ |
| \%RSD |  |  |  | 7.69 |

Table S9. Precision determination for standard mixture corresponding to LOD ( $\mathbf{0 . 0 6 8 \%}$ w/w BPO in API)

| S.No. | \% w/w of BPO content | Area in counts at $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0.068 | 999919 | 7834 | 0.0078 |
| 2 |  | 1001434 | 7330 | 0.0073 |
| 3 |  | 1006071 | 5992 | 0.0059 |
| 4 |  | 1006820 | 7996 | 0.0079 |
| 5 |  | 1006302 | 6775 | 0.0067 |
| 6 |  | 946956 | 7156 | 0.0075 |
| Mean st.DEV \%RSD |  |  |  | 0.007 |
|  |  |  |  | 0.0007 |
|  |  |  |  | 10.00 |

Table S10. Accuracy determination using $\mathbf{0 . 4 5 \%}, \mathbf{0 . 1 5 \%}$ and $\mathbf{0 . 1 0 \%} \mathbf{w} / \mathrm{w}$ BPO in API
 calibration curve

| S.No. | \% w/w of BPO content | Area in counts at $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio | Average Area ratio | Calculated $\% \mathrm{w} / \mathrm{w}$ of BPO | \% <br> Recovery |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.443 | 1113860 | 71710 | 0.0605 | 0.060 | 0.460 | 99.59 |
|  |  | 1116109 | 71374 | 0.0601 |  |  |  |
|  |  | 1118092 | 69409 | 0.0584 |  |  |  |
| 2 | 0.133 | 1126209 | 20252 | 0.0177 | 0.018 | 0.149 | 91.15 |
|  |  | 1126390 | 20565 | 0.0179 |  |  |  |
|  |  | 1129758 | 19574 | 0.0170 |  |  |  |
| 3 | 0.099 | 1049862 | 15184 | 0.0143 | 0.014 | 0.119 | 84.30 |
|  |  | 1058913 | 14908 | 0.0139 |  |  |  |
|  |  | 1052540 | 14603 | 0.0137 |  |  |  |

Table S11. Estimation of assay errors such as Instrument Repeatability with $\mathbf{0 . 9 0 \%}$ w/w BPO in API standard mixture and Intra/Inter Day Repeatability with $\mathbf{0 . 4 5 \%}$ w/w BPO in API standard mixture


## 6. HPLC method details and validation

Table S12. HPLC method of analysis for BPO

| Column | Waters Xbridge C18, $100 \mathrm{~mm} \times 4.6 \mathrm{~mm}$ i.d., $3.5 \mu \mathrm{~m}$ particle size |  |
| :--- | :--- | :--- |
| Column Part No. | 186003033 |  |
| Column Temperature | $25^{\circ} \mathrm{C}$ |  |
| Sample Temperature | $25^{\circ} \mathrm{C}$ |  |
| Detector Wavelength | 205 nm |  |
| Pump Configuration | Gradient |  |
| Flow Rate | $1.0 \mathrm{~mL} /$ minute |  |
| Injection Volume | $10.0 \mu \mathrm{~L}$ |  |
| Run Time | 20 minutes |  |
| Mobile Phase A | $0.05 \%$ v/v TFA MilliQ Water: Acetonitrile/ $90: 10 \mathrm{v} / \mathrm{v}$ |  |
| Mobile Phase B | $0.05 \%$ v/v TFA MilliQ Water: Acetonitrile/ $10: 90 \mathrm{v} / \mathrm{v}$ |  |
| Needle Wash | Acetonitrile: Water $(1: 1 \mathrm{v} / \mathrm{v})$ |  |
| Diluent | DMSO |  |
|  | Time (min) | $\%$ of Mobile phase A $\%$ of Mobile phase B |
|  | 0 | 40 |
| Gradient Programme | 5 | 0 |
|  | 15 | 0 |
|  | 17 | 40 |
| Retention Time of BPO |  | 40 |

## Standards Preparation:

Standard Stock Solution: Weighed about 110 mg of BPO (corrected for potency) in 100 mL volumetric flask, dissolved and diluted to volume with acetonitrile

Standard solution-1 ( $1 \% \mathrm{w} / \mathrm{v}$ level): Pipetted out 10 mL of standard stock solution in 100 mL volumetric flask, diluted to volume with diluent

Standard solution-2 ( $0.1 \% \mathrm{w} / \mathrm{v}$ level): Pipetted out 10 mL of standard solution-1 in 100 mL volumetric flask, diluted to volume with diluent

Standard solution-3 ( $0.05 \% \mathrm{w} / \mathrm{v}$ level): Pipetted out 5 mL of standard solution-1 in 100 mL volumetric flask, diluted to volume with diluent

Standard solution-4 ( $0.01 \% \mathrm{w} / \mathrm{v}$ level): Pipetted out 1 mL of standard solution-1 in 100 mL volumetric flask, diluted to volume with diluent

Sample concentration: Weighed about 100 mg of sample in 10 mL , dissolved and diluted to volume with diluent

Table S13. HPLC data for preparation of linearity curve using standard solutions with different levels of BPO

| Linearity |  |  |  |
| :---: | :---: | :---: | :---: |
| Weight of BPO (mg) <br> Potency of BPO (\%) |  |  | 110.08 |
|  |  |  | 90 |
| Level | Concentration | Area | Average Area |
| 0.01\% | 0.001101 | 7695 | 7658 |
|  |  | 7621 |  |
| 0.05\% | 0.005504 | 41111 | 41632 |
|  |  | 42153 |  |
| 0.10\% | 0.011008 | 83912 | 84137 |
|  |  | 84361 |  |
| 0.30\% | 0.033024 | 267631 | 266671 |
|  |  | 265710 |  |
| 0.50\% | 0.055040 | 401946 | 401280 |
|  |  | 400614 |  |
| 0.80\% | 0.088064 | 630628 | 630667 |
|  |  | 630705 |  |
| 1.0\% | 0.110080 | 861943 | 861531 |
|  |  | 861119 |  |
| Correlation Coefficient |  |  | 0.9979 |



Figure S20. HPLC linearity curve plotted using peak area of BPO against concentration of BPO in the standard solutions

Table S14. HPLC Injection Precision for $\mathbf{0 . 1 0 \%}$ and $1.00 \%$ w/w BPO standard solutions

| $\mathbf{0 . 1 0 \%}$ Level |  |  | $\mathbf{1 . 0 0 \%}$ Level |  |
| :---: | :---: | :---: | :---: | :---: |
| Injections | Area | Injections | Area |  |
| 1 | 727390 | 1 | 7294956 |  |
| 2 | 728938 | 2 | 7308388 |  |
| 3 | 727270 | 3 | 7289689 |  |
| 4 | 728671 | 4 | 7293163 |  |
| 5 | 725630 | 5 | 7324544 |  |
| Average | $\mathbf{7 2 7 5 8 0}$ | Average | $\mathbf{7 3 0 2 1 4 8}$ |  |
| SD | $\mathbf{1 3 2 0}$ | SD | $\mathbf{1 4 3 8 9}$ |  |
| \% RSD | $\mathbf{0 . 1 8}$ | \% RSD | $\mathbf{0 . 2 0}$ |  |

Table S15. HPLC \% Recovery at $\mathbf{0 . 0 1 \%}, \mathbf{0 . 1 0 \%}$ and $\mathbf{1 . 0 0 \%}$ w/w BPO spiked in API

| Sample Wt (mg) |  | Sample Wt (mg) |  | Sample Wt (mg) |  | Sample Wt (mg) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 102.52 (As Such) |  | 102.38 (Spiked) |  | 101.44 (Spiked) |  | 100.2 (Spiked) |  |
| Area | Ave.Area | Area | Ave.Area | Area | Ave.Area | Area | Ave.Area |
| $\begin{aligned} & 163914 \\ & 165201 \end{aligned}$ | 164558 | $234037$ | 234116 | $\begin{aligned} & \hline 877626 \\ & 878472 \end{aligned}$ | 878049 | $7382585$ | 7385649 |
| \% Recovery |  | 0.01 | Level | 98.2 |  | 99.5 |  |

Table S15. HPLC Precision at LOQ level $0.01 \%$ w/w BPO standard solution

| Injection | Area |
| :---: | :---: |
| 1 | 7695 |
| 2 | 7621 |
| Average | 7623 |
| Standard Deviation | 7664 |
| \% RSD | 7739 |



Figure S21. HPLC overlay of different levels of BPO analysed for Linearity


Figure S22. HPLC Overlay of different levels $(\mathbf{0 . 0 1 \%}, \mathbf{0 . 1 0 \%}$ and $\mathbf{1 . 0 0 \%} \mathbf{w} / \mathbf{w})$ of BPO spiked in API analysed for HPLC method Recovery

## 7. Comparison of PXRD and HPLC results for 'unknown' samples

Samples with three different levels of BPO spiking in API were prepared for verification of results obtained from PXRD calibration curve and its comparison with results obtained by HPLC technique.

Table S17. Concentration of BPO in API determined using PXRD and HPLC

| PXRD |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S.No. | Sample | Area in counts at $7.38^{\circ} 2 \theta$ | Area in counts at $8.86^{\circ} 2 \theta$ | Area ratio | Average Area ratio | BPO content (\% w/w in API) |
|  |  | 610637 | 59155 | 0.0883 |  |  |
| 1 | I | 603940 | 61642 | 0.0926 | 0.093 | 0.680 |
|  |  | 615290 | 66514 | 0.0976 |  |  |
|  |  | 654480 | 32007 | 0.0466 |  |  |
| 2 | II | 657285 | 33204 | 0.0481 | 0.048 | 0.359 |
|  |  | 655223 | 33150 | 0.0482 |  |  |
|  |  | 693432 | 8302 | 0.0118 |  |  |
| 3 | III | 698202 | 7960 | 0.0113 | 0.011 | 0.096 |
|  |  | 699662 | 7543 | 0.0107 |  |  |
| HPLC |  |  |  |  |  |  |
| S.No. | $\% \mathrm{w} / \mathrm{w}$ of BPO in API | Area of Brettphos Oxide |  | Average Area |  | BPO content (\% w/w in API) |
| 1 | I | $4592712$ |  | 4600305.5 |  | 0.695 |
| 2 | II | 2485301 |  | 2483538 |  | 0.381 |
|  |  | 2481775 |  |  |  |  |
| 3 | III | 716821 |  | 716096 |  | 0.108 |



Figure S23. PXRD overlay of 'unknown' samples (I, II and III) of BPO spiked API


Figure S24. HPLC overlay of 'unknown' samples (I, II and III) of BPO spiked API

