

# Thermodynamic, kinetic, and structural parameterization of human carbonic anhydrase interactions toward enhanced inhibitor design

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# 1 Supplementary tables

## 1.1 Table 1

Table 1: Observed (pH 7.0) and intrinsic dissociation constants (nM) and observed (pH 7.0) and intrinsic Gibbs energies (kJ mol<sup>-1</sup>) of compound binding to recombinant 12 human catalytically active CAs at 37°C

No. Cpd	Structure	Thermodynamic binding parameters												
		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>Non-halogenated compounds</b>														
1 EZA		$K_{d,obs}$ (nM)	17	1.3	5200	82	26	8.6	33	0.61	1.9	71	19	10
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-46.2	-52.8	-31.4	-42.1	-45.0	-47.9	-44.4	-54.7	-51.8	-42.4	-45.8	-47.5
		$K_{d,int}$ (nM)	2.0	0.073	160	3.1	2.3	0.57	0.40	0.031	0.071	3.6	2.3	0.51
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-51.6	-60.1	-40.3	-50.5	-51.3	-54.9	-55.8	-62.4	-60.2	-50.1	-51.3	-55.2
2 AZM		$K_{d,obs}$ (nM)	2400	46	40 000	87	840	140	220	13	21	130	79	63
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.4	-43.5	-26.1	-41.9	-36.1	-40.6	-39.5	-46.8	-45.5	-40.9	-42.1	-42.8
		$K_{d,int}$ (nM)	1100	9.8	4600	12	270	34	9.8	2.4	2.9	24	35	12
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-35.5	-47.5	-31.7	-47.0	-39.0	-44.3	-47.5	-51.1	-50.6	-45.2	-44.3	-47.1
3 MZM		$K_{d,obs}$ (nM)	200	100	40 000	250	ND	67	830	50	36	500	200	110
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-39.8	-41.4	-26.1	-39.2	ND	-42.6	-36.1	-43.3	-44.2	-37.4	-39.8	-41.3
		$K_{d,int}$ (nM)	110	27	5600	41	ND	19	44	11	6.0	110	25	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.4	-44.9	-31.2	-43.8	ND	-45.8	-43.7	-47.2	-48.8	-41.2	-41.4	-45.1
4 TPM		$K_{d,obs}$ (nM)	34 000	110	≥200 000	67	≥200 000	2.5	13 000	25	34	82	240	20
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.5	-41.4	≥-22.0	-42.6	≥-22.0	-51.0	-29.1	-45.1	-44.3	-42.1	-39.2	-45.7
		$K_{d,int}$ (nM)	970	1.4	1500	0.58	20 000	0.038	35	0.30	0.30	0.97	6.8	0.24
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-35.7	-52.5	-34.6	-54.8	-27.8	-61.8	-44.3	-56.5	-56.6	-53.5	-48.5	-57.1
5 CARBS		$K_{d,obs}$ (nM)	11 000	4000	≥200 000	3300	3100	20 000	11 000	4000	1800	3300	5800	4000
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.3	-32.0	≥-22.0	-32.5	-32.7	-27.9	-29.4	-32.0	-34.1	-32.5	-31.1	-32.0
		$K_{d,int}$ (nM)	61	10	270	5.4	12	57	5.8	8.9	3.0	7.4	30	8.9
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.8	-47.4	-38.9	-49.1	-47.0	-43.0	-48.9	-47.8	-50.6	-48.3	-44.6	-47.8
6 PAMBS		$K_{d,obs}$ (nM)	83 000	17 000	≥200 000	17 000	ND	41 000	21 000	28 000	18 000	34 000	≥200 000	≥200 000
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-24.2	-28.3	≥-22.0	-28.4	ND	-26.1	-27.7	-27.0	-28.2	-26.5	≥-22.0	≥-22.0
		$K_{d,int}$ (nM)	150	14	110	9.0	ND	39	3.7	21	9.7	25	690	290
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.6	-46.5	-41.3	-47.7	ND	-44.0	-50.0	-45.6	-47.6	-45.1	-36.6	-38.8
7 BSA		$K_{d,obs}$ (nM)	7700	1900	≥200 000	17 000	6700	33 000	13 000	7200	1500	12 000	7500	5100
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-30.3	-33.9	≥-22.0	-28.4	-30.7	-26.6	-29.0	-30.5	-34.5	-29.1	-30.4	-31.4
		$K_{d,int}$ (nM)	6.5	0.78	44	4.3	4.0	15	1.1	2.5	0.40	4.4	6.2	1.8
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-48.6	-54.0	-43.7	-49.6	-49.8	-46.4	-53.2	-51.0	-55.8	-49.6	-48.7	-51.9
8 SULFA		$K_{d,obs}$ (nM)	85 000	13 000	≥200 000	13 000	36 000	≥200 000	68 000	62 000	15 000	82 000	150 000	29 000
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-24.2	-29.1	≥-22.0	-29.0	-26.4	≥-22.0	-24.7	-24.9	-28.6	-24.3	-22.7	-27.0
		$K_{d,int}$ (nM)	150	11	180	7.0	45	190	12	46	8.3	60	260	21
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.5	-47.3	-40.0	-48.4	-43.6	-39.9	-47.1	-43.5	-47.9	-42.9	-39.1	-45.6

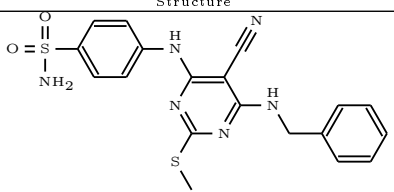
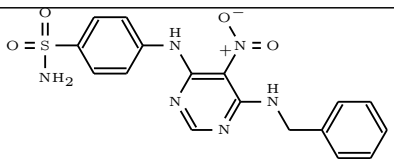
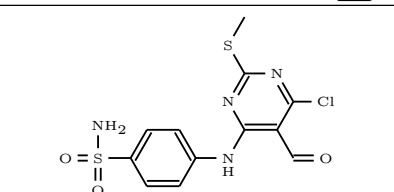
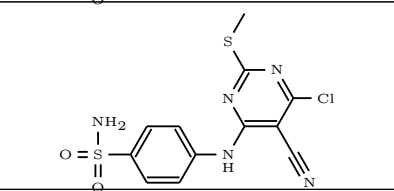
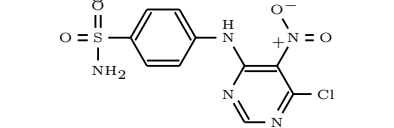
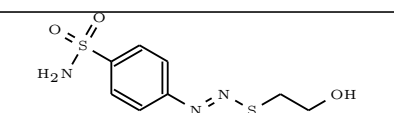
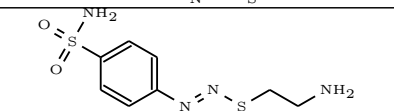
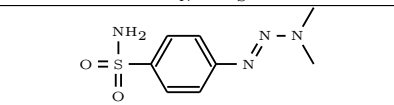
No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
9 E11-0		$K_{d,obs}$ (nM)	670	430	ND	ND	770	ND	ND	ND	250	2900	2900	ND	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-36.7	-37.8	ND	ND	-36.3	ND	ND	ND	-39.2	ND	-32.9	-32.9	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
10 VD11-31		$K_{d,obs}$ (nM)	110	140	ND	3900	5800	10 000	5000	200	850	2900	1400	250	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.3	-40.6	ND	-32.1	-31.1	-29.7	-31.5	-39.7	-36.0	-32.9	-34.7	-39.2	
		$K_{d,int}$ (nM)	0.11	0.070	ND	1.2	4.2	5.5	0.50	0.086	0.26	1.2	1.4	0.11	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.0	-60.3	ND	-52.9	-49.7	-49.0	-55.2	-59.7	-56.8	-52.9	-52.5	-59.2	
11 VD12-10		$K_{d,obs}$ (nM)	5.0	25	ND	1700	3700	67	830	40	100	330	290	26	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-49.3	-45.1	ND	-34.2	-32.3	-42.6	-36.1	-43.9	-41.5	-38.4	-38.8	-45.0	
		$K_{d,int}$ (nM)	0.0029	0.0070	ND	0.30	1.5	0.021	0.048	0.0098	0.018	0.081	0.16	0.0063	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.5	-66.2	ND	-56.5	-52.3	-63.4	-61.2	-65.3	-63.8	-59.9	-58.1	-66.5	
12 VD11-36		$K_{d,obs}$ (nM)	4.5	12	≥200 000	ND	1300	14	1100	17	77	220	50	19	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-49.5	-47.1	≥-22.0	ND	-34.9	-46.6	-35.3	-46.2	-42.2	-39.6	-43.3	-45.8	
		$K_{d,int}$ (nM)	0.0032	0.0039	36	ND	0.65	0.0054	0.077	0.0049	0.017	0.063	0.034	0.0055	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.2	-67.7	-44.1	ND	-54.5	-66.9	-60.0	-67.1	-64.0	-60.5	-62.1	-66.8	
13 E84x		$K_{d,obs}$ (nM)	100	100	ND	ND	ND	ND	ND	100	ND	1200	1400	ND	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.5	-41.5	ND	ND	ND	ND	ND	-41.5	ND	-35.0	-34.7	ND	
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	
14 JS69		$K_{d,obs}$ (nM)	490	110	≥200 000	2900	ND	200	13 000	860	33	1000	140	500	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-37.5	-41.3	≥-22.0	-32.9	ND	-39.8	-29.1	-36.0	-44.4	-35.6	-40.6	-37.4	
		$K_{d,int}$ (nM)	0.28	0.031	30	0.51	ND	0.063	0.72	0.21	0.0060	0.24	0.082	0.12	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-56.6	-62.4	-44.6	-55.1	ND	-60.5	-54.3	-57.4	-66.6	-57.0	-59.9	-58.8	
15 JS68		$K_{d,obs}$ (nM)	160 000	420	ND	ND	ND	ND	ND	100	ND	ND	100	ND	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-22.5	-37.9	ND	ND	ND	ND	ND	-41.5	ND	ND	-41.5	ND	
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	
16 JS72		$K_{d,obs}$ (nM)	67	71	≥200 000	2500	ND	1100	3300	130	180	1000	280	220	
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-42.6	-42.4	≥-22.0	-33.2	ND	-35.3	-32.5	-40.8	-40.0	-35.6	-38.9	-39.5	
		$K_{d,int}$ (nM)	0.049	0.025	38	0.57	ND	0.44	0.24	0.041	0.041	0.31	0.20	0.068	
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-61.2	-62.9	-44.0	-54.9	ND	-55.5	-57.1	-61.6	-61.6	-56.5	-57.5	-60.3	

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
17		$K_{d,obs}$ (nM)	620	16	$\geq 200\ 000$	20 000	ND	4000	25 000	710	500	ND	1700	500
JS76		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-36.8	-46.3	$\geq -22.0$	-27.9	ND	-32.0	-27.3	-36.5	-37.4	ND	-34.3	-37.4
		$K_{d,int}$ (nM)	0.46	0.0056	38	4.5	ND	1.6	1.8	0.22	0.11	ND	1.2	0.15
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-55.4	-66.8	-44.0	-49.5	ND	-52.2	-51.9	-57.3	-59.0	ND	-52.9	-58.2
18		$K_{d,obs}$ (nM)	170	170	ND	ND	ND	ND	ND	250	ND	ND	20	ND
JS80		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-40.2	-40.2	ND	ND	ND	ND	ND	-39.2	ND	ND	-45.7	ND
		$K_{d,int}$ (nM)	0.13	0.059	ND	ND	ND	ND	ND	0.077	ND	ND	0.014	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-58.8	-60.7	ND	ND	ND	ND	ND	-60.0	ND	ND	-64.3	ND
19		$K_{d,obs}$ (nM)	36	53	ND	ND	ND	ND	ND	830	ND	ND	240	ND
JS71		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-44.1	-43.2	ND	ND	ND	ND	ND	-36.1	ND	ND	-39.2	ND
		$K_{d,int}$ (nM)	0.027	0.019	ND	ND	ND	ND	ND	0.26	ND	ND	0.18	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-62.7	-63.7	ND	ND	ND	ND	ND	-56.9	ND	ND	-57.9	ND
20		$K_{d,obs}$ (nM)	25	100	$\geq 200\ 000$	5000	ND	10 000	25 000	4200	400	ND	1200	1000
JS75		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-45.1	-41.5	$\geq -22.0$	-31.5	ND	-29.7	-27.3	-31.9	-38.0	ND	-35.0	-35.6
		$K_{d,int}$ (nM)	0.018	0.035	38	1.1	ND	4.0	1.8	1.3	0.090	ND	0.90	0.31
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-63.7	-62.0	-44.0	-53.1	ND	-49.9	-51.9	-52.8	-59.6	ND	-53.7	-56.5
21		$K_{d,obs}$ (nM)	40 000	13 000	$\geq 200\ 000$	ND	ND	ND	62 000	22 000	ND	9500	33 000	ND
KR50-1		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.1	-29.1	$\geq -22.0$	ND	ND	ND	-24.9	-27.6	ND	-29.8	-26.6	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
22		$K_{d,obs}$ (nM)	36 000	9100	$\geq 200\ 000$	ND	ND	ND	71 000	36 000	ND	33 000	59 000	ND
KR50-2		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.4	-29.9	$\geq -22.0$	ND	ND	ND	-24.6	-26.4	ND	-26.6	-25.1	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
23		$K_{d,obs}$ (nM)	13 000	4500	$\geq 200\ 000$	ND	ND	ND	33 000	4500	ND	5900	26 000	ND
KR50-14		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.1	-31.7	$\geq -22.0$	ND	ND	ND	-26.6	-31.7	ND	-31.0	-27.2	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND



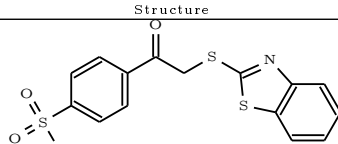
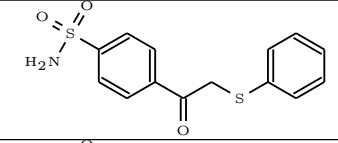
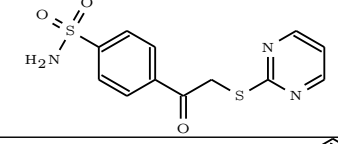
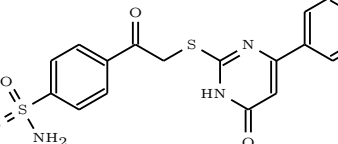
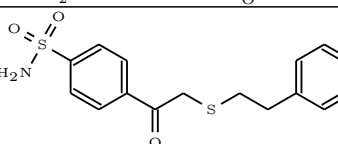
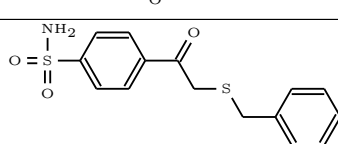
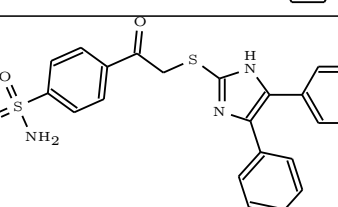


No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>32</b> KR50-5		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	15 000 -28.6 ND ND	1900 -34.0 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	25 000 -27.3 ND ND	13 000 -29.1 ND ND	ND ND ND ND	33 000 -26.6 ND ND	5600 -31.2 ND ND	ND ND ND ND
<b>33</b> KR50-10		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	13 000 -29.1 ND ND	1800 -34.1 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	7100 -30.5 ND ND	5900 -31.0 ND ND	ND ND ND ND	31 000 -26.7 ND ND	7100 -30.5 ND ND	ND ND ND ND
<b>34</b> KR50-9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	13 000 -29.1 ND ND	2000 -33.8 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	6700 -30.7 ND ND	13 000 -29.1 ND ND	ND ND ND ND	33 000 -26.6 ND ND	8300 -30.1 ND ND	ND ND ND ND
<b>35</b> KR50-11		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	37 000 -26.3 ND ND	8300 -30.1 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	50 000 -25.5 ND ND	25 000 -27.3 ND ND	ND ND ND ND	33 000 -26.6 ND ND	56 000 -25.3 ND ND	ND ND ND ND
<b>36</b> KTU17		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 ND ND	3600 -32.3 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	25 000 -27.3 ND ND	25 000 -27.3 ND ND	ND ND ND ND	67 000 -24.8 ND ND	50 000 -25.5 ND ND	ND ND ND ND
<b>37</b> KR50-6		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	11 000 -29.4 ND ND	1400 -34.7 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	25 000 -27.3 ND ND	17 000 -28.4 ND ND	ND ND ND ND	50 000 -25.5 ND ND	4300 -31.8 ND ND	ND ND ND ND
<b>38</b> KR50-16b		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	9100 -29.9 ND ND	4000 -32.0 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	8300 -30.1 ND ND	5600 -31.2 ND ND	ND ND ND ND	5600 -31.2 ND ND	9100 -29.9 ND ND	ND ND ND ND
<b>39</b> KR50-16a		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	29 000 -27.0 ND ND	4000 -32.0 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	7100 -30.5 ND ND	13 000 -29.1 ND ND	ND ND ND ND	1900 -34.0 ND ND	19 000 -28.1 ND ND	ND ND ND ND

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
40 JS46		$K_{d,obs}$ (nM) 100 000	100 000	$\geq 200\ 000$	50 000	ND	$\geq 200\ 000$	$\geq 200\ 000$	$\geq 200\ 000$	330	$\geq 200\ 000$	100 000	33 000
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -23.7	-23.7	$\geq -22.0$	-25.5	ND	$\geq -22.0$	$\geq -22.0$	$\geq -22.0$	-38.4	$\geq -22.0$	-23.7	-26.6
		$K_{d,int}$ (nM) 74	35	38	11	ND	79	14	61	0.075	310	72	10
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -42.3	-44.2	-44.0	-47.2	ND	-42.1	-46.5	-42.8	-60.1	-38.7	-42.4	-47.4
41 JS48		$K_{d,obs}$ (nM) 71	170	$\geq 200\ 000$	10 000	ND	670	17 000	10 000	50	29 000	1400	290
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -42.4	-40.2	$\geq -22.0$	-29.7	ND	-36.7	-28.4	-29.7	-43.3	-26.9	-34.7	-38.8
		$K_{d,int}$ (nM) 0.053	0.059	38	2.3	ND	0.26	1.2	3.1	0.011	9.0	1.0	0.088
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -61.0	-60.7	-44.0	-51.3	ND	-56.8	-52.9	-50.5	-65.0	-47.7	-53.3	-59.7
42 JS43		$K_{d,obs}$ (nM) 830	350	ND	ND	ND	ND	ND	1900	ND	8300	610	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -36.1	-38.3	ND	ND	ND	ND	ND	-33.9	ND	-30.1	-36.9	ND
		$K_{d,int}$ (nM) 0.61	0.12	ND	ND	ND	ND	ND	0.44	ND	2.6	0.44	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -54.7	-58.8	ND	ND	ND	ND	ND	-55.5	ND	-51.0	-55.5	ND
43 JS44		$K_{d,obs}$ (nM) 1200	130	ND	ND	ND	ND	ND	2300	ND	2500	310	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -35.1	-40.8	ND	ND	ND	ND	ND	-33.5	ND	-33.2	-38.6	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
44 JS45		$K_{d,obs}$ (nM) 560	91	10 000	5000	ND	3300	13 000	130	67	1700	2.0	250
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -37.1	-41.8	-29.7	-31.5	ND	-32.5	-29.1	-40.8	-42.6	-34.3	-51.6	-39.2
		$K_{d,int}$ (nM) 0.41	0.032	1.9	1.1	ND	1.3	0.90	0.041	0.015	0.51	0.0014	0.077
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -55.7	-62.3	-51.7	-53.1	ND	-52.7	-53.7	-61.6	-64.2	-55.1	-70.3	-60.0
45 MK8		$K_{d,obs}$ (nM) 33	67	ND	ND	ND	ND	3200	290	ND	2000	2000	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -44.4	-42.6	ND	ND	ND	ND	-32.6	-38.8	ND	-33.8	-33.8	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
46 MK9		$K_{d,obs}$ (nM) 500	280	ND	ND	ND	ND	8300	1000	ND	6300	7700	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -37.4	-38.9	ND	ND	ND	ND	-30.1	-35.6	ND	-30.9	-30.3	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
47 MK5		$K_{d,obs}$ (nM) 100	180	ND	ND	ND	ND	13 000	770	ND	4000	1700	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -41.5	-40.0	ND	ND	ND	ND	-28.9	-36.3	ND	-32.0	-34.2	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>48</b> MK6		$K_{d,obs}$ (nM) 13	71	ND	ND	ND	ND	13 000	200	ND	590	500	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -46.7	-42.4	ND	ND	ND	ND	-28.9	-39.8	ND	-37.0	-37.4	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>49</b> MK2		$K_{d,obs}$ (nM) 33	130	ND	ND	ND	ND	13 000	450	ND	1800	830	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -44.4	-40.8	ND	ND	ND	ND	-28.9	-37.6	ND	-34.1	-36.1	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>50</b> MK1		$K_{d,obs}$ (nM) 6.7	63	ND	ND	ND	ND	10 000	120	ND	770	330	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -48.5	-42.8	ND	ND	ND	ND	-29.7	-41.1	ND	-36.3	-38.4	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>51</b> MK3		$K_{d,obs}$ (nM) 3.8	43	ND	ND	ND	ND	14 000	130	ND	770	170	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -49.9	-43.7	ND	ND	ND	ND	-28.8	-41.0	ND	-36.3	-40.2	ND
		$K_{d,int}$ (nM) 0.0093	0.050	ND	ND	ND	ND	3.4	0.13	ND	0.78	0.40	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -65.5	-61.1	ND	ND	ND	ND	-50.3	-58.7	ND	-54.0	-55.8	ND
<b>52</b> MK4		$K_{d,obs}$ (nM) 40	100	ND	ND	ND	ND	12 000	400	ND	4000	1100	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -43.9	-41.5	ND	ND	ND	ND	-29.3	-38.0	ND	-32.0	-35.3	ND
		$K_{d,int}$ (nM) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>53</b> E63		$K_{d,obs}$ (nM) 25	13	ND	360	1400	4000	5000	56	ND	1000	29	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -45.2	-46.9	ND	-38.2	-34.7	-32.0	-31.5	-43.1	ND	-35.6	-44.8	ND
		$K_{d,int}$ (nM) 0.090	0.022	ND	0.41	3.8	7.9	1.8	0.085	ND	1.5	0.10	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -59.6	-63.3	ND	-55.7	-50.0	-48.1	-51.9	-59.8	ND	-52.3	-59.3	ND
<b>54</b> E66		$K_{d,obs}$ (nM) 15	83	ND	200	670	1000	1200	250	ND	91	63	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -46.5	-42.0	ND	-39.7	-36.7	-35.6	-35.0	-39.2	ND	-41.8	-42.8	ND
		$K_{d,int}$ (nM) 0.054	0.15	ND	0.23	1.8	2.0	0.45	0.38	ND	0.14	0.23	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -60.9	-58.4	ND	-57.2	-52.0	-51.6	-55.5	-55.9	ND	-58.5	-57.3	ND
<b>55</b> E67		$K_{d,obs}$ (nM) 1.7	67	ND	390	1600	2000	5000	48	32	170	4.9	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -52.0	-42.6	ND	-38.0	-34.5	-33.8	-31.5	-43.4	-44.5	-40.2	-49.3	ND
		$K_{d,int}$ (nM) 0.0063	0.12	ND	0.44	4.1	4.0	1.8	0.074	0.036	0.26	0.018	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -66.5	-58.9	ND	-55.5	-49.8	-49.9	-51.9	-60.1	-62.0	-56.9	-63.8	ND
<b>56</b> E61		$K_{d,obs}$ (nM) 22	13	ND	200	1500	6300	5000	67	ND	1400	23	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -45.5	-46.9	ND	-39.7	-34.5	-30.9	-31.5	-42.6	ND	-34.7	-45.4	ND
		$K_{d,int}$ (nM) 0.080	0.022	ND	0.23	4.1	12	1.8	0.10	ND	2.2	0.082	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -59.9	-63.3	ND	-57.2	-49.8	-46.9	-51.9	-59.3	ND	-51.4	-59.9	ND
<b>57</b> E59		$K_{d,obs}$ (nM) 67	67	ND	380	500	2500	3700	170	ND	560	360	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -42.6	-42.6	ND	-38.1	-37.4	-33.2	-32.2	-40.2	ND	-37.1	-38.3	ND
		$K_{d,int}$ (nM) 0.24	0.12	ND	0.43	1.3	5.0	1.3	0.26	ND	0.85	1.3	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -57.0	-58.9	ND	-55.6	-52.7	-49.3	-52.7	-56.9	ND	-53.8	-52.8	ND



No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>66</b> E73		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	13 -46.9 ND ND	5.0 -49.3 ND ND	ND ND ND ND	50 -43.3 ND ND	330 -38.4 ND ND	330 -38.4 ND ND	ND ND ND ND	29 -44.8 ND ND	ND ND ND ND	500 -37.4 ND ND	15 -46.4 ND ND	ND ND ND ND
<b>67</b> E88		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3.7 -50.1 ND ND	6.0 -48.8 ND ND	ND ND ND ND	380 -38.1 ND ND	1000 -35.6 ND ND	ND ND ND ND	ND ND ND ND	50 -43.3 ND ND	ND ND ND ND	290 -38.8 ND ND	33 -44.4 ND ND	ND ND ND ND
<b>68</b> E90		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	41 -43.9 0.15 -58.3	17 -46.2 0.029 -62.5	ND ND ND ND	1100 -35.4 1.2 -52.9	2500 -33.2 6.6 -48.5	ND ND ND ND	910 -35.9 0.33 -56.3	67 -42.6 0.10 -59.3	220 -39.5 0.25 -57.0	560 -37.1 0.85 -53.8	290 -38.8 1.0 -53.3	ND ND ND ND
<b>69</b> E95		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	200 -39.8 ND ND	50 -43.3 ND ND	ND ND ND ND	ND ND ND ND	3300 -32.5 ND ND	ND ND ND ND	ND ND ND ND	14 -46.6 ND ND	ND ND ND ND	38 -44.0 ND ND	50 -43.3 ND ND	ND ND ND ND
<b>70</b> E97		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2.3 -51.2 ND ND	5.0 -49.3 ND ND	ND ND ND ND	220 -39.5 ND ND	220 -39.5 ND ND	670 -36.7 ND ND	ND ND ND ND	6.7 -48.5 ND ND	ND ND ND ND	200 -39.8 ND ND	10 -47.5 ND ND	ND ND ND ND
<b>71</b> E99		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2.0 -51.6 ND ND	10 -47.5 ND ND	ND ND ND ND	40 -43.9 ND ND	400 -38.0 ND ND	500 -37.4 ND ND	ND ND ND ND	7.1 -48.3 ND ND	ND ND ND ND	100 -41.5 ND ND	38 -44.0 ND ND	ND ND ND ND
<b>72</b> AR6		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	330 -38.4 ND ND	170 -40.2 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	120 -41.1 ND ND	ND ND ND ND	4000 -32.0 ND ND	77 -42.2 ND ND	ND ND ND ND



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>80</b>		$K_{d,obs}$ (nM)	7.1	5.6	56 000	1700	1000	290	4000	17	24	670	29	7.9
E85		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-48.3	-49.0	-25.3	-34.2	-35.6	-38.8	-32.0	-46.1	-45.3	-36.7	-44.8	-48.1
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>81</b>		$K_{d,obs}$ (nM)	11	4.2	≥200 000	1800	1200	710	2500	20	25	1000	50	7.1
E93		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-47.2	-49.7	≥-22.0	-34.2	-35.0	-36.5	-33.2	-45.7	-45.1	-35.6	-43.3	-48.3
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>82</b>		$K_{d,obs}$ (nM)	8.3	4.2	21 000	1700	770	110	2900	20	36	1100	63	7.7
E86		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-47.9	-49.7	-27.8	-34.2	-36.3	-41.2	-32.9	-45.7	-44.2	-35.5	-42.8	-48.2
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>83</b>		$K_{d,obs}$ (nM)	140	100	≥200 000	1400	14 000	1000	6700	20	360	8300	290	150
E87		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-40.6	-41.5	≥-22.0	-34.7	-28.8	-35.6	-30.7	-45.7	-38.2	-30.1	-38.8	-40.4
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>84</b>		$K_{d,obs}$ (nM)	2500	250	ND	2600	3300	10 000	ND	500	ND	4000	4500	ND
E10-4		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.2	-39.2	ND	-33.2	-32.5	-29.7	ND	-37.4	ND	-32.1	-31.7	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>85</b>		$K_{d,obs}$ (nM)	130	180	≥200 000	5000	2000	5000	10 000	830	67	2500	2200	130
E74		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.0	-40.0	≥-22.0	-31.5	-33.8	-31.5	-29.7	-36.1	-42.6	-33.2	-33.5	-41.0
		$K_{d,int}$ (nM)	0.15	0.11	63	1.9	1.8	3.3	1.2	0.42	0.025	1.3	2.7	0.064
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-58.3	-59.2	-42.7	-51.8	-52.0	-50.3	-52.9	-55.6	-62.9	-52.8	-50.9	-60.5
<b>86</b>		$K_{d,obs}$ (nM)	50	200	≥200 000	10 000	3300	2500	100 000	1400	67	8300	330	290
E75		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-43.3	-39.8	≥-22.0	-29.7	-32.5	-33.2	-23.7	-34.7	-42.6	-30.1	-38.4	-38.8
		$K_{d,int}$ (nM)	0.061	0.12	63	3.7	2.9	1.6	12	0.73	0.025	4.2	0.40	0.15
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.6	-59.0	-42.7	-50.0	-50.6	-52.1	-47.0	-54.2	-62.9	-49.7	-55.8	-58.3



No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV		
<b>87</b> E76		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	25 -45.1 0.030 -62.4	71 -42.4 0.042 -61.6	$\geq 200\,000$ $\geq -22.0$ 63 -42.7	1100 -35.3 0.42 -55.7	1100 -35.3 0.97 -53.5	2900 -32.9 1.9 -51.8	5300 -31.3 0.63 -54.6	560 -37.1 0.28 -56.7	83 -42.0 0.031 -62.3	1100 -35.3 0.57 -54.9	620 -36.8 0.75 -54.2	40 -43.9 0.020 -63.4	
<b>88</b> KR50-18a		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3800 -32.1 ND ND	830 -36.1 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	13 000 -29.1 ND ND	1500 -34.5 ND ND	ND -31.2 ND ND	5600 -30.1 ND ND	8300 -31.2 ND ND	ND ND ND ND	
<b>89</b> KR50-18b		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1100 -35.3 ND ND	670 -36.7 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	8300 -30.1 ND ND	1600 -34.4 ND ND	ND -31.2 ND ND	5600 -32.9 ND ND	2900 -32.9 ND ND	ND ND ND ND	
<b>90</b> E11-63		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	33 000 -26.6 38 -44.0	5000 -31.5 2.7 -50.8	$\geq 200\,000$ $\geq -22.0$ 59 -42.9	5600 -31.2 1.9 -51.7	17 000 -28.4 14 -46.7	25 000 -27.3 15 -46.4	7900 -30.3 0.88 -53.7	8300 -30.1 4.0 -49.9	830 -36.1 0.29 -56.6	10 000 -29.7 4.8 -49.4	6700 -30.7 7.4 -48.2	2500 -33.2 1.2 -53.0	
<b>91</b> E11-65		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5900 -31.0 6.7 -48.5	1800 -34.1 0.99 -53.4	$\geq 200\,000$ $\geq -22.0$ 59 -42.9	9600 -29.8 3.4 -50.3	17 000 -28.4 14 -46.7	8300 -30.1 5.1 -49.2	20 000 -27.9 2.2 -51.3	6700 -30.7 3.2 -50.4	220 -39.5 0.078 -60.0	10 000 -29.7 4.8 -49.4	670 -36.7 0.74 -54.2	1000 -35.6 0.48 -55.3	
<b>92</b> E11-67		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.0 1.4 -52.5	670 -36.7 0.36 -56.0	$\geq 200\,000$ $\geq -22.0$ 59 -42.9	420 -37.9 0.15 -58.4	17 000 -28.4 14 -46.7	6700 -30.7 4.1 -49.8	7100 -30.5 0.80 -54.0	5000 -31.5 2.4 -51.2	140 -40.6 0.050 -61.1	17 000 -28.4 7.9 -48.1	670 -36.7 0.74 -54.2	1100 -35.5 0.50 -55.2	
<b>93</b> E11-7		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 -41.5 ND ND	560 -37.1 ND ND	ND ND ND ND	4500 -31.7 ND ND	1700 -34.3 ND ND	ND ND ND ND	ND ND ND ND	ND -34.7 ND ND	1400 -34.7 ND ND	ND -35.0 ND ND	1200 -38.8 ND ND	290 -38.8 ND ND	ND ND ND ND
<b>94</b> E11-71		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	260 -39.0 ND ND	560 -37.1 ND ND	ND ND ND ND	1800 -34.1 ND ND	6700 -30.7 ND ND	5000 -31.5 ND ND	ND ND ND ND	ND -34.5 ND ND	1500 -34.5 ND ND	ND -37.8 ND ND	430 -39.8 ND ND	200 -39.8 ND ND	ND ND ND ND
<b>95</b> E11-69		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	230 -39.4 ND ND	710 -36.5 ND ND	ND ND ND ND	5000 -31.5 ND ND	5900 -31.0 ND ND	3300 -32.5 ND ND	ND ND ND ND	ND -32.0 ND ND	4000 -32.0 ND ND	ND -34.7 ND ND	1400 -40.1 ND ND	170 -40.1 ND ND	ND ND ND ND
<b>96</b> E11-9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	770 -36.3 2.8 -50.7	1100 -35.3 2.0 -51.7	ND ND ND ND	3400 -32.4 3.9 -49.9	420 -37.9 1.1 -53.2	15 000 -28.6 31 -44.6	1900 -33.9 0.69 -54.4	4000 -32.0 6.1 -48.7	690 -36.6 0.78 -54.1	3300 -32.5 5.1 -49.2	1300 -34.9 4.8 -49.4	ND ND ND ND	



No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>105</b> E11-21		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2200 -33.5 8.2 -48.0	1100 -35.3 2.0 -51.7	ND ND ND ND	6700 -30.7 7.5 -48.2	1000 -35.6 2.6 -50.9	1700 -34.3 3.3 -50.3	3300 -32.5 1.2 -52.9	13 000 -29.1 19 -45.8	ND ND ND ND	6700 -30.7 10 -47.4	1400 -34.7 5.1 -49.2	ND ND ND ND
<b>106</b> E11-23		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.0 4.6 -49.5	670 -36.7 1.2 -53.0	ND ND ND ND	1400 -34.7 1.6 -52.2	1400 -34.7 3.8 -50.0	ND ND ND ND	2100 -33.7 0.75 -54.1	1000 -35.6 1.5 -52.3	ND ND ND ND	1000 -35.6 1.5 -52.3	2200 -33.5 8.0 -48.0	ND ND ND ND
<b>107</b> E11-75		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6700 -30.7 ND ND	1700 -34.3 ND ND	ND ND ND ND	5000 -31.5 ND ND	1100 -35.3 ND ND	6700 -30.7 ND ND	ND ND ND ND	4000 -32.0 ND ND	ND ND ND ND	3300 -32.5 ND ND	1400 -34.7 ND ND	ND ND ND ND
<b>108</b> E11-73		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5000 -31.5 ND ND	1000 -35.6 ND ND	ND ND ND ND	6700 -30.7 ND ND	2500 -33.2 ND ND	6700 -30.7 ND ND	ND ND ND ND	1700 -34.3 ND ND	ND ND ND ND	5900 -31.0 ND ND	770 -36.3 ND ND	ND ND ND ND
<b>109</b> E11-57		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	71 -42.4 ND ND	140 -40.6 ND ND	ND ND ND ND	2500 -33.2 ND ND	670 -36.7 ND ND	4000 -32.0 ND ND	3300 -32.5 ND ND	560 -37.1 ND ND	ND ND ND ND	710 -36.5 ND ND	190 -40.0 ND ND	ND ND ND ND
<b>110</b> E11-31		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	590 -37.0 ND ND	910 -35.9 ND ND	ND ND ND ND	830 -36.1 ND ND	400 -38.0 ND ND	5000 -31.5 ND ND	ND ND ND ND	3300 -32.5 ND ND	ND ND ND ND	910 -35.9 ND ND	2000 -33.8 ND ND	ND ND ND ND
<b>111</b> E11-33		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3300 -32.5 ND ND	1100 -35.3 ND ND	ND ND ND ND	1700 -34.3 ND ND	170 -40.2 ND ND	5000 -31.5 ND ND	ND ND ND ND	1400 -34.7 ND ND	ND ND ND ND	3300 -32.5 ND ND	2900 -32.9 ND ND	ND ND ND ND







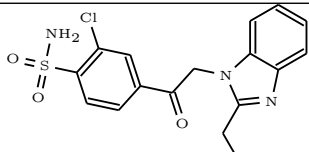
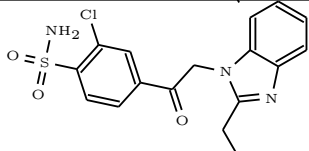
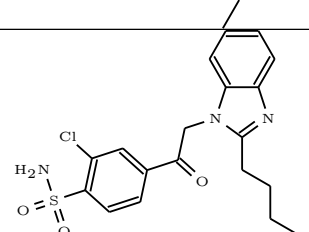
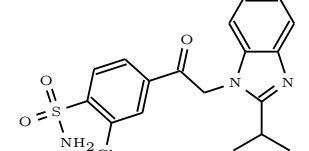
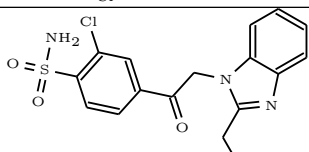
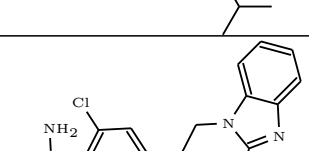
No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>131</b> VD81		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	8800 -30.0 ND ND	8200 -30.2 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	$\geq 200\,000$ $\geq -22.0$ ND ND	ND ND ND ND	25 000 -27.3 ND ND	110 000 -23.5 ND ND	ND ND ND ND
<b>132</b> VD9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 -41.5 ND ND	50 -43.3 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	410 -37.9 ND ND	ND ND ND ND	2000 -33.8 ND ND	360 -38.3 ND ND	ND ND ND ND
<b>Chlorinated compounds</b>														
<b>133</b> VD13-03		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	33 -44.4 ND ND	100 -41.5 ND ND	ND ND ND ND	ND ND ND ND	200 -39.8 ND ND	ND ND ND ND	1000 -35.6 ND ND	22 -45.4 ND ND	130 -40.9 ND ND	560 -37.1 ND ND	17 -46.2 ND ND	29 -44.7 ND ND
<b>134</b> E11-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 -41.5 ND ND	170 -40.2 ND ND	ND ND ND ND	1900 -34.0 ND ND	1100 -35.3 ND ND	ND ND ND ND	ND ND ND ND	170 -40.2 ND ND	ND ND ND ND	1700 -34.3 ND ND	200 -39.8 ND ND	ND ND ND ND
<b>135</b> E11-62		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 -41.5 0.34 -56.2	290 -38.8 0.46 -55.4	$\geq 200\,000$ $\geq -22.0$ 170 -40.1	1200 -35.0 1.3 -52.8	3300 -32.5 8.0 -48.0	4200 -31.9 7.5 -48.2	11 000 -29.4 3.7 -50.1	670 -36.7 0.93 -53.6	560 -37.1 0.57 -54.8	2000 -33.8 2.8 -50.8	530 -37.3 1.7 -52.0	180 -40.0 0.25 -56.9
<b>136</b> E11-64		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	17 -46.2 0.056 -60.8	100 -41.5 0.16 -58.1	$\geq 200\,000$ $\geq -22.0$ 170 -40.1	1400 -34.7 1.5 -52.4	1200 -35.0 3.0 -50.6	1400 -34.7 2.6 -51.0	17 000 -28.4 5.5 -49.0	150 -40.4 0.22 -57.4	250 -39.2 0.26 -56.9	500 -37.4 0.70 -54.3	77 -42.2 0.25 -57.0	91 -41.8 0.13 -58.7
<b>137</b> E11-66		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	50 -43.3 0.17 -58.0	250 -39.2 0.40 -55.8	170 000 -22.4 140 -40.6	1100 -35.3 1.1 -53.1	3300 -32.5 8.0 -48.0	1200 -35.0 2.3 -51.3	50 000 -25.5 16 -46.2	250 -39.2 0.35 -56.1	140 -40.6 0.15 -58.3	2000 -33.8 2.8 -50.8	33 -44.4 0.11 -59.1	130 -41.0 0.17 -57.9
<b>138</b> E11-68		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1.8 -51.9 ND ND	8.3 -47.9 ND ND	ND ND ND ND	420 -37.9 ND ND	130 -40.8 ND ND	2000 -33.8 ND ND	ND ND ND ND	7.7 -48.2 ND ND	ND ND ND ND	230 -39.4 ND ND	1.9 -51.8 ND ND	ND ND ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>139</b>		$K_{d,obs}$ (nM)	33	13	ND	670	770	1000	ND	11	ND	250	6.7	ND
E11-74		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-44.4	-46.9	ND	-36.7	-36.3	-35.6	ND	-47.2	ND	-39.2	-48.5	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>140</b>		$K_{d,obs}$ (nM)	67	33	ND	1700	290	2500	ND	25	ND	3300	10	ND
E11-72		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-42.6	-44.4	ND	-34.2	-38.8	-33.2	ND	-45.1	ND	-32.5	-47.5	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>141</b>		$K_{d,obs}$ (nM)	10	11	ND	910	360	ND	2500	5.0	200	830	17	ND
E11-8		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-47.5	-47.2	ND	-35.8	-38.3	ND	-33.2	-49.3	-39.8	-36.1	-46.2	ND
		$K_{d,int}$ (nM)	0.12	0.061	ND	3.2	3.0	ND	2.8	0.024	0.70	4.0	0.19	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.0	-60.6	ND	-50.4	-50.6	ND	-50.7	-63.0	-54.3	-49.8	-57.7	ND
<b>142</b>		$K_{d,obs}$ (nM)	1.0	5.6	ND	38	130	ND	1100	2.9	ND	71	5.0	ND
E11-6		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-53.4	-49.0	ND	-44.0	-41.0	ND	-35.3	-50.7	ND	-42.4	-49.3	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>143</b>		$K_{d,obs}$ (nM)	1.4	10	ND	130	250	500	ND	7.7	ND	130	7.7	ND
E11-70		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-52.5	-47.5	ND	-41.0	-39.2	-37.4	ND	-48.2	ND	-40.8	-48.2	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>144</b>		$K_{d,obs}$ (nM)	6.7	8.5	ND	620	400	1500	5000	10	ND	440	2.1	ND
E11-12		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-48.5	-47.9	ND	-36.8	-38.0	-34.5	-31.5	-47.5	ND	-37.7	-51.5	ND
		$K_{d,int}$ (nM)	0.077	0.047	ND	2.2	3.3	9.6	5.7	0.048	ND	2.1	0.024	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.0	-61.3	ND	-51.4	-50.3	-47.6	-48.9	-61.2	ND	-51.5	-63.1	ND
<b>145</b>		$K_{d,obs}$ (nM)	5.3	7.1	ND	480	330	1800	3300	17	ND	590	1.2	ND
E11-14		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-49.1	-48.3	ND	-37.5	-38.4	-34.1	-32.5	-46.2	ND	-37.0	-52.8	ND
		$K_{d,int}$ (nM)	0.061	0.039	ND	1.7	2.8	11	3.8	0.080	ND	2.8	0.014	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.6	-61.8	ND	-52.1	-50.8	-47.2	-50.0	-59.9	ND	-50.7	-64.4	ND



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>146</b> E11-16		$K_{d,obs}$ (nM)	6.2	7.7	ND	400	330	1700	3300	11	ND	360	1.8	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-48.7	-48.2	ND	-38.0	-38.4	-34.3	-32.5	-47.2	ND	-38.3	-51.9	ND
		$K_{d,int}$ (nM)	0.072	0.042	ND	1.4	2.8	10	3.8	0.053	ND	1.7	0.021	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.2	-61.6	ND	-52.5	-50.8	-47.4	-50.0	-61.0	ND	-52.0	-63.4	ND
<b>147</b> E11-10		$K_{d,obs}$ (nM)	5.0	17	ND	1300	770	ND	2900	13	ND	910	10	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-49.3	-46.2	ND	-34.9	-36.3	ND	-32.9	-46.9	ND	-35.9	-47.5	ND
		$K_{d,int}$ (nM)	0.058	0.092	ND	4.7	6.4	ND	3.2	0.060	ND	4.4	0.11	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.8	-59.6	ND	-49.4	-48.6	ND	-50.4	-60.7	ND	-49.6	-59.0	ND
<b>148</b> E11-18		$K_{d,obs}$ (nM)	6.7	28	ND	560	200	3300	2500	36	ND	330	33	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-48.5	-44.9	ND	-37.1	-39.8	-32.5	-33.2	-44.2	ND	-38.4	-44.4	ND
		$K_{d,int}$ (nM)	0.077	0.15	ND	2.0	1.7	21	2.8	0.17	ND	1.6	0.38	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.0	-58.3	ND	-51.7	-52.1	-45.6	-50.7	-58.0	ND	-52.2	-55.9	ND
<b>149</b> E11-24		$K_{d,obs}$ (nM)	10	110	ND	1200	290	5000	4500	50	ND	200	83	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-47.5	-41.3	ND	-35.0	-38.8	-31.5	-31.7	-43.3	ND	-39.8	-42.0	ND
		$K_{d,int}$ (nM)	0.12	0.61	ND	4.4	2.4	31	5.1	0.24	ND	0.96	0.94	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.0	-54.7	ND	-49.6	-51.2	-44.6	-49.2	-57.1	ND	-53.5	-53.6	ND
<b>150</b> E11-26		$K_{d,obs}$ (nM)	0.35	26	ND	1200	50	250	9100	7.5	ND	250	1.2	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-56.1	-45.0	ND	-35.0	-43.3	-39.2	-29.9	-48.2	ND	-39.2	-53.0	ND
		$K_{d,int}$ (nM)	0.0041	0.15	ND	4.4	0.41	1.6	10	0.036	ND	1.2	0.013	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-67.6	-58.4	ND	-49.6	-55.7	-52.3	-47.4	-62.0	ND	-52.9	-64.5	ND
<b>151</b> E11-28		$K_{d,obs}$ (nM)	98	110	ND	18 000	7700	100 000	ND	22	ND	320	15	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.6	-41.3	ND	-28.2	-30.3	-23.7	ND	-45.4	ND	-38.6	-46.4	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>152</b> E11-22		$K_{d,obs}$ (nM)	14	20	ND	590	170	ND	2900	25	ND	250	77	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-46.6	-45.7	ND	-37.0	-40.2	ND	-32.9	-45.1	ND	-39.2	-42.2	ND
		$K_{d,int}$ (nM)	0.16	0.11	ND	2.1	1.4	ND	3.2	0.12	ND	1.2	0.87	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-58.1	-59.1	ND	-51.5	-52.6	ND	-50.4	-58.9	ND	-52.9	-53.8	ND



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>160</b> E11-40		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	4.8 -49.4 ND ND	6.2 -48.7 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	930 -35.8 ND ND	500 -37.4 ND ND	1000 -35.6 ND ND	2300 -33.5 ND ND	7.7 -48.2 ND ND	8.3 -47.9 ND ND	67 -42.6 ND ND	11 -47.1 ND ND	7.7 -48.2 ND ND
<b>161</b> E11-42		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2.9 -50.7 ND ND	3.6 -50.1 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	1400 -34.7 ND ND	1700 -34.3 ND ND	1200 -35.0 ND ND	22 000 -27.6 ND ND	4.2 -49.7 ND ND	14 -46.6 ND ND	63 -42.8 ND ND	5.6 -49.0 ND ND	5.6 -49.0 ND ND
<b>162</b> E11-44		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3.3 -50.3 ND ND	2.7 -50.8 ND ND	130 000 $\geq -22.0$ ND ND	1100 -35.3 ND ND	830 -36.1 ND ND	670 -36.7 ND ND	5000 -31.5 ND ND	3.3 -50.3 ND ND	10 -47.4 ND ND	110 -41.2 ND ND	2.5 -51.0 ND ND	5.0 -49.3 ND ND
<b>163</b> E11-46		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5.0 -49.3 ND ND	14 -46.6 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	960 -35.7 ND ND	670 -36.7 ND ND	1100 -35.3 ND ND	5600 -31.2 ND ND	5.0 -49.3 ND ND	9.1 -47.7 ND ND	330 -38.4 ND ND	40 -43.9 ND ND	5.0 -49.3 ND ND
<b>164</b> E11-48		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6.7 -48.5 ND ND	14 -46.6 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	1000 -35.5 ND ND	1000 -35.6 ND ND	710 -36.5 ND ND	4000 -32.0 ND ND	5.0 -49.3 ND ND	3.9 -49.9 ND ND	500 -37.4 ND ND	40 -43.9 ND ND	2.4 -51.2 ND ND
<b>165</b> E11-54		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1.7 -52.1 ND ND	3.3 -50.3 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	950 -35.7 ND ND	500 -37.4 ND ND	500 -37.4 ND ND	23 000 -27.6 ND ND	4.5 -49.5 ND ND	13 -46.9 ND ND	67 -42.6 ND ND	9.1 -47.7 ND ND	12 -47.1 ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>166</b> E11-50		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 -47.5 ND ND	14 -46.6 ND ND	33 000 -26.6 ND ND	1300 -34.9 ND ND	250 -39.2 ND ND	670 -36.7 ND ND	3100 -32.7 ND ND	5.0 -49.3 ND ND	25 -45.1 ND ND	1000 -35.6 ND ND	67 -42.6 ND ND	22 -45.4 ND ND
<b>167</b> E11-52		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	8.3 -47.9 ND ND	2.9 -50.7 ND ND	≥200 000 ≥-22.0 ND ND	980 -35.7 ND ND	1000 -35.6 ND ND	5000 -31.5 ND ND	1400 -34.7 ND ND	8.3 -47.9 ND ND	71 -42.4 ND ND	170 -40.2 ND ND	6.7 -48.5 ND ND	10 -47.4 ND ND
<b>168</b> E11-60		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	67 -42.6 ND ND	250 -39.2 ND ND	ND ND ND ND	180 -40.0 ND ND	1000 -35.6 ND ND	13 000 -29.1 ND ND	3300 -32.5 ND ND	650 -36.7 ND ND	ND ND ND ND	3000 -32.7 ND ND	500 -37.4 ND ND	ND ND ND ND
<b>169</b> E16		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	17 000 -28.4 ND ND	710 -36.5 ND ND	ND ND ND ND	360 -38.3 ND ND	770 -36.3 ND ND	100 -41.5 ND ND	ND ND ND ND	830 -36.1 ND ND	ND ND ND ND	ND ND ND ND	200 -39.8 ND ND	ND ND ND ND
<b>170</b> E17		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 ND ND	1200 -35.0 ND ND	ND ND ND ND	1000 -35.6 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	1000 -35.6 ND ND	ND ND ND ND	1200 -35.0 ND ND	280 -38.9 ND ND	ND ND ND ND
<b>171</b> E39		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 ND ND	500 -37.4 ND ND	ND ND ND ND	670 -36.7 ND ND	140 -40.6 ND ND	3300 -32.5 ND ND	67 000 -24.8 ND ND	330 -38.4 ND ND	ND ND ND ND	ND ND ND ND	220 -39.5 ND ND	ND ND ND ND
<b>172</b> E35		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	17 000 -28.4 72 -42.4	670 -36.7 1.4 -52.6	≥200 000 ≥-22.0 220 -39.5	670 -36.7 0.88 -53.7	5000 -31.5 16 -46.3	2000 -33.8 4.7 -49.4	1400 -34.7 0.60 -54.7	200 -39.8 0.36 -56.0	710 -36.5 0.95 -53.6	1100 -35.3 2.0 -51.6	560 -37.1 2.4 -51.2	220 -39.5 0.40 -55.8



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>181</b> AR1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6700 -30.7 ND ND	67 -42.6 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	91 -41.8 ND ND	ND ND ND ND	1800 -34.1 ND ND	140 -40.6 ND ND	ND ND ND ND
<b>182</b> E31		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.1 ND ND	290 -38.8 ND ND	ND ND ND ND	2900 -32.9 ND ND	42 -43.8 ND ND	13 000 -29.1 ND ND	ND ND ND ND	4100 -32.0 ND ND	ND ND ND ND	1400 -34.7 ND ND	10 000 -29.7 ND ND	ND ND ND ND
<b>183</b> E21		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 ND ND	130 -40.8 ND ND	ND ND ND ND	560 -37.1 ND ND	13 -46.9 ND ND	400 -38.0 ND ND	ND ND ND ND	53 -43.2 ND ND	ND ND ND ND	500 -37.4 ND ND	170 -40.2 ND ND	ND ND ND ND
<b>184</b> E38		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.0 14 -46.5	63 -42.8 0.34 -56.2	ND ND ND ND	ND ND ND ND	6.7 -48.5 0.055 -60.9	ND ND ND ND	2800 -33.0 3.1 -50.5	130 -41.0 0.60 -54.7	ND ND ND ND	580 -37.0 2.8 -50.8	56 -43.0 0.63 -54.6	ND ND ND ND
<b>185</b> E27		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.0 14 -46.5	33 -44.4 0.18 -57.8	ND ND ND ND	910 -35.8 3.2 -50.4	170 -40.2 1.4 -52.6	ND ND ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	1000 -35.6 4.8 -49.4	33 -44.4 0.38 -55.9	ND ND ND ND
<b>186</b> E54		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	830 -36.1 ND ND	250 -39.2 ND ND	ND ND ND ND	670 -36.7 ND ND	330 -38.4 ND ND	1400 -34.7 ND ND	23 000 -27.6 ND ND	710 -36.5 ND ND	ND ND ND ND	400 -38.0 ND ND	250 -39.2 ND ND	ND ND ND ND
<b>187</b> E89		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	4300 -31.9 55 -43.1	330 -38.4 2.1 -51.6	ND ND ND ND	590 -37.0 2.3 -51.2	67 -42.6 0.62 -54.6	ND ND ND ND	560 -37.1 0.70 -54.3	710 -36.5 3.8 -49.9	ND ND ND ND	1400 -34.7 7.8 -48.1	330 -38.4 4.2 -49.7	ND ND ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>188</b> E50		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1800 -34.1 21 -45.6	140 -40.6 0.79 -54.0	ND ND ND ND	400 -38.0 1.4 -52.5	6.2 -48.7 0.052 -61.0	ND ND ND ND	670 -36.7 0.75 -54.1	330 -38.4 1.6 -52.2	ND ND ND ND	1200 -35.0 6.0 -48.8	110 -41.3 1.3 -52.8	ND ND ND ND
<b>189</b> E45		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1300 -34.9 15 -46.5	120 -41.1 0.66 -54.5	ND ND ND ND	290 -38.8 1.0 -53.4	5.0 -49.3 0.041 -61.6	560 -37.1 3.5 -50.2	1100 -35.3 1.3 -52.8	220 -39.5 1.1 -53.2	ND ND ND ND	1100 -35.5 5.1 -49.2	37 -44.1 0.41 -55.7	ND ND ND ND
<b>190</b> E53		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1400 -34.7 16 -46.2	67 -42.6 0.37 -56.0	ND ND ND ND	250 -39.2 0.89 -53.7	4.0 -49.8 0.033 -62.2	ND ND ND ND	500 -37.4 0.57 -54.9	200 -39.8 0.96 -53.5	ND ND ND ND	1100 -35.3 5.3 -49.1	67 -42.6 0.75 -54.1	ND ND ND ND
<b>191</b> E49		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 12 -47.1	220 -39.5 1.2 -52.9	ND ND ND ND	1200 -35.0 4.4 -49.6	130 -41.0 1.0 -53.3	1700 -34.3 10 -47.4	1000 -35.6 1.1 -53.1	330 -38.4 1.6 -52.2	ND ND ND ND	1400 -34.7 6.9 -48.4	330 -38.4 3.8 -50.0	ND ND ND ND
<b>192</b> E32		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	830 -36.1 9.6 -47.6	200 -39.8 1.1 -53.2	ND ND ND ND	600 -36.9 2.1 -51.5	400 -38.0 3.3 -50.3	2500 -33.2 16 -46.3	1000 -35.6 1.1 -53.1	180 -40.1 0.86 -53.8	ND ND ND ND	320 -38.6 1.5 -52.3	200 -39.8 2.3 -51.3	ND ND ND ND
<b>193</b> E57		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	670 -36.7 7.7 -48.2	67 -42.6 0.37 -56.0	ND ND ND ND	170 -40.2 0.59 -54.8	250 -39.2 2.1 -51.5	670 -36.7 4.1 -49.7	830 -36.1 0.94 -53.6	56 -43.1 0.27 -56.8	ND ND ND ND	100 -41.5 0.48 -55.3	56 -43.1 0.63 -54.6	ND ND ND ND
<b>194</b> E52		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 -41.5 1.2 -53.0	50 -43.3 0.28 -56.7	ND ND ND ND	330 -38.4 1.2 -53.0	290 -38.8 2.4 -51.1	1800 -34.1 11 -47.2	2000 -33.8 2.3 -51.3	28 -44.8 0.14 -58.6	ND ND ND ND	43 -43.7 0.21 -57.4	25 -45.1 0.28 -56.7	ND ND ND ND
<b>195</b> E46		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1200 -35.0 14 -46.5	50 -43.3 0.28 -56.7	ND ND ND ND	ND ND ND ND	100 -41.5 0.83 -53.9	1200 -35.0 7.8 -48.1	200 -39.8 0.23 -57.2	38 -44.0 0.18 -57.8	ND ND ND ND	200 -39.8 0.96 -53.5	130 -41.0 1.4 -52.5	ND ND ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
196 E33		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	450 -37.6 5.2 -49.1	26 -45.0 0.15 -58.4	ND ND ND ND	140 -40.6 0.50 -55.2	110 -41.3 0.92 -53.6	330 -38.4 2.1 -51.5	290 -38.8 0.32 -56.3	130 -40.8 0.64 -54.6	ND ND ND ND	230 -39.4 1.1 -53.2	42 -43.8 0.47 -55.4	ND ND ND ND
197 E44		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2000 -33.8 ND ND	200 -39.8 ND ND	ND ND ND ND	120 -41.1 ND ND	250 -39.2 ND ND	3300 -32.5 ND ND	5000 -31.5 ND ND	500 -37.4 ND ND	ND ND ND ND	1000 -35.6 ND ND	330 -38.4 ND ND	ND ND ND ND
198 E56		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2700 -33.1 ND ND	1200 -35.2 ND ND	ND ND ND ND	400 -38.0 ND ND	2.5 -51.0 ND ND	1200 -35.0 ND ND	ND ND ND ND	580 -37.0 ND ND	ND ND ND ND	1400 -34.8 ND ND	630 -36.8 ND ND	ND ND ND ND
199 E36		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3100 -32.7 36 -44.2	170 -40.2 0.92 -53.6	ND ND ND ND	ND ND ND ND	6.7 -48.5 0.055 -60.9	ND ND ND ND	ND ND ND ND	110 -41.3 0.54 -55.0	ND ND ND ND	910 -35.8 4.4 -49.6	41 -43.9 0.46 -55.4	ND ND ND ND
200 E94		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5000 -31.5 ND ND	26 -45.0 ND ND	ND ND ND ND	3300 -32.5 ND ND	33 000 -26.6 ND ND	ND ND ND ND	ND ND ND ND	170 -40.2 ND ND	ND ND ND ND	290 -38.8 ND ND	100 -41.5 ND ND	ND ND ND ND
201 E14-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	110 000 -23.5 ND ND	1500 -34.5 ND ND	$\geq 200 000$ $\geq -22.0$ ND ND	83 -42.0 ND ND	13 -46.7 ND ND	10 000 -29.7 ND ND	1200 -35.0 ND ND	1200 -35.2 ND ND	2000 -33.8 ND ND	3000 -32.7 ND ND	1300 -35.0 ND ND	590 -37.0 ND ND
202 VR15-3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	26 000 -27.2 ND ND	1700 -34.2 ND ND	$\geq 200 000$ $\geq -22.0$ ND ND	11 000 -29.4 ND ND	450 -37.6 ND ND	3700 -32.2 ND ND	4300 -31.8 ND ND	2600 -33.1 ND ND	1200 -35.0 ND ND	2900 -32.9 ND ND	620 -36.8 ND ND	530 -37.3 ND ND



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>203</b> VR15-5		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND ND ND ND	ND ND ND ND	50 000 -25.5 ND ND	ND ND ND ND	ND ND ND ND	310 -38.6 ND ND	ND ND ND ND	ND ND ND ND	670 -36.7 ND ND	ND ND ND ND	ND ND ND ND	150 -40.4 ND ND
<b>204</b> VR15-4		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	31 000 -26.7 ND ND	1100 -35.3 ND ND	170 000 -22.4 ND ND	1400 -34.7 ND ND	33 -44.4 ND ND	1000 -35.6 ND ND	2100 -33.7 ND ND	2100 -33.7 ND ND	1600 -34.4 ND ND	2800 -33.0 ND ND	1700 -34.2 ND ND	480 -37.5 ND ND
<b>205</b> VR15-6		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\ 000$ $\geq -22.0$ ND ND	20 000 -27.9 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	15 000 -28.6 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	34 000 -26.5 ND ND	17 000 -28.4 ND ND
<b>206</b> AZ15-15		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5000 -31.5 ND ND	1000 -35.6 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	150 -40.4 ND ND	1200 -35.0 ND ND	830 -36.1 ND ND	3800 -32.1 ND ND	4200 -31.9 ND ND	1000 -35.6 ND ND	1700 -34.3 ND ND	620 -36.8 ND ND	250 -39.2 ND ND
<b>207</b> E2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	11 000 -29.4 130 -40.9	1600 -34.5 8.6 -47.9	$\geq 200\ 000$ $\geq -22.0$ 600 -36.9	640 -36.8 2.3 -51.3	0.25 -57.0 0.0021 -69.3	3300 -32.5 21 -45.6	720 -36.5 0.81 -54.0	1000 -35.6 4.8 -49.4	770 -36.3 2.7 -50.8	3100 -32.7 15 -46.4	360 -38.3 4.0 -49.8	300 -38.7 1.5 -52.4
<b>208</b> E3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 ND ND	2000 -33.8 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	1200 -35.2 ND ND	330 -38.4 ND ND	4000 -32.0 ND ND	5000 -31.5 ND ND	2500 -33.2 ND ND	1000 -35.6 ND ND	6100 -31.0 ND ND	200 -39.8 ND ND	260 -39.1 ND ND
<b>209</b> E12		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	7100 -30.5 ND ND	560 -37.1 ND ND	130 000 -23.2 ND ND	1400 -34.7 ND ND	670 -36.7 ND ND	1700 -34.3 ND ND	2500 -33.2 ND ND	1700 -34.3 ND ND	580 -37.0 ND ND	2500 -33.3 ND ND	200 -39.8 ND ND	210 -39.6 ND ND

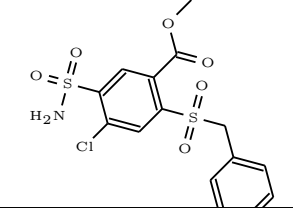
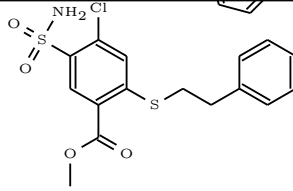
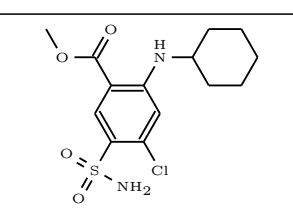
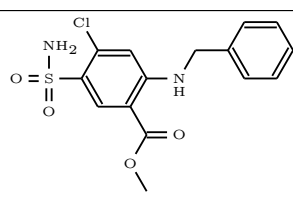
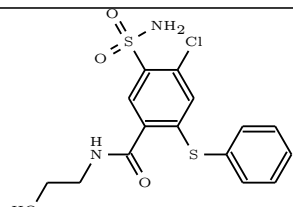


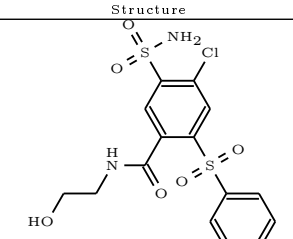
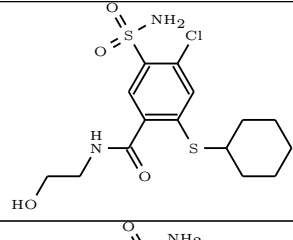
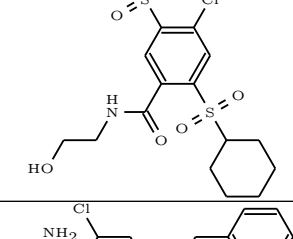
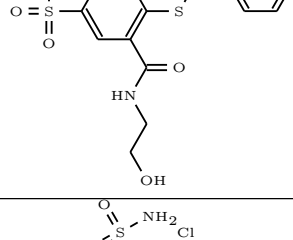
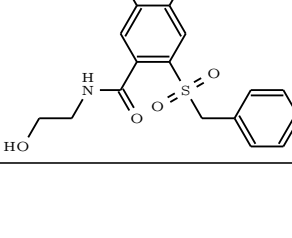
No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>215</b> E6		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND ND ND ND	1000 -35.6 ND ND	$\geq 200\,000$ $\geq -22.0$ ND ND	1400 -34.7 ND ND	19 -45.9 ND ND	1800 -34.1 ND ND	2200 -33.5 ND ND	400 -38.0 ND ND	470 -37.6 ND ND	6100 -31.0 ND ND	380 -38.1 ND ND	250 -39.2 ND ND
<b>216</b> E20		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	40 000 -26.1 ND ND	4200 -31.9 ND ND	ND ND ND ND	100 000 -23.7 ND ND	11 000 -29.4 ND ND	17 000 -28.4 ND ND	ND ND ND ND	10 000 -29.7 ND ND	ND ND ND ND	20 000 -27.9 ND ND	6300 -30.9 ND ND	ND ND ND ND
<b>217</b> E7		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	7200 -30.5 ND ND	1600 -34.5 ND ND	$\geq 200\,000$ $\geq -22.0$ ND ND	1500 -34.6 ND ND	1000 -35.6 ND ND	1200 -35.0 ND ND	1200 -35.0 ND ND	2400 -33.4 ND ND	660 -36.7 ND ND	980 -35.7 ND ND	490 -37.5 ND ND	150 -40.5 ND ND
<b>218</b> VR15-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	7100 -30.5 ND ND	590 -37.0 ND ND	80 000 -24.3 ND ND	3300 -32.5 ND ND	0.77 -54.1 ND ND	500 -37.4 ND ND	2000 -33.8 ND ND	1700 -34.3 ND ND	620 -36.8 ND ND	3100 -32.7 ND ND	770 -36.3 ND ND	190 -39.9 ND ND
<b>219</b> AZ15-16		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2700 -33.0 ND ND	1200 -35.0 ND ND	$\geq 200\,000$ $\geq -22.0$ ND ND	3300 -32.5 ND ND	400 -38.0 ND ND	220 -39.5 ND ND	10 000 -29.7 ND ND	3300 -32.5 ND ND	400 -38.0 ND ND	2500 -33.2 ND ND	530 -37.3 ND ND	330 -38.4 ND ND
<b>220</b> EA1-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	50 000 -25.5 150 -40.6	330 -38.4 0.47 -55.4	11 000 -29.4 8.4 -47.9	1500 -34.6 1.3 -52.6	20 000 -27.9 42 -43.8	2500 -33.2 3.9 -49.9	4000 -32.0 1.1 -53.1	110 -41.3 0.14 -58.6	670 -36.7 0.60 -54.7	620 -36.8 0.76 -54.1	330 -38.4 0.96 -53.5	440 -37.7 0.54 -55.0

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>221</b> EA3-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 000 -23.7 1400 -34.7	83 -42.0 0.58 -54.8	8300 -30.1 31 -44.5	400 -38.0 1.8 -51.9	5000 -31.5 52 -43.2	400 -38.0 3.1 -50.5	620 -36.8 0.89 -53.7	10 -47.5 0.060 -60.6	170 -40.2 0.74 -54.2	130 -41.0 0.75 -54.1	560 -37.1 7.9 -48.1	67 -42.6 0.40 -55.8
<b>222</b> EA4-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\ 000$ $\geq -22.0$ 2900 -32.9	10 -47.5 0.069 -60.3	25 000 -27.3 94 -41.7	7.1 -48.3 0.032 -62.3	8300 -30.1 87 -41.9	770 -36.3 6.0 -48.8	1000 -35.6 1.4 -52.5	10 -47.5 0.060 -60.6	50 -43.3 0.22 -57.3	170 -40.2 1.0 -53.4	620 -36.8 8.9 -47.8	63 -42.8 0.38 -55.9
<b>223</b> EA5-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	33 000 -26.6 540 -37.2	20 -45.7 0.15 -58.2	7100 -30.5 30 -44.6	83 -42.0 0.41 -55.7	5000 -31.5 58 -42.9	83 -42.0 0.73 -54.2	170 -40.2 0.26 -56.8	5.0 -49.3 0.034 -62.1	50 -43.3 0.25 -57.0	50 -43.3 0.34 -56.2	400 -38.0 6.3 -48.7	50 -43.3 0.34 -56.2
<b>224</b> EA8-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	50 000 -25.5 810 -36.2	63 -42.8 0.48 -55.3	12 000 -29.2 51 -43.3	10 -47.5 0.050 -61.1	3400 -32.4 40 -43.9	250 -39.2 2.2 -51.4	590 -37.0 0.93 -53.6	11 -47.2 0.075 -60.1	71 -42.4 0.36 -56.1	200 -39.8 1.4 -52.6	710 -36.5 11 -47.2	40 -43.9 0.27 -56.8
<b>225</b> EA12-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\ 000$ $\geq -22.0$ 2500 -33.3	140 -40.6 0.84 -53.9	45 000 -25.8 150 -40.6	280 -38.9 1.1 -53.3	2000 -33.8 18 -46.0	2300 -33.4 15 -46.4	1400 -34.7 1.7 -52.0	67 -42.6 0.34 -56.2	290 -38.8 1.1 -53.2	40 -43.9 0.21 -57.5	670 -36.7 8.1 -48.0	87 -41.9 0.45 -55.5
<b>226</b> EA11-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 000 -23.7 1600 -34.4	50 -43.3 0.39 -55.9	50 000 -25.5 210 -39.6	110 -41.3 0.55 -54.9	1200 -35.0 15 -46.5	67 -42.6 0.58 -54.8	1000 -35.6 1.6 -52.2	20 -45.7 0.14 -58.6	140 -40.7 0.69 -54.4	130 -41.0 0.84 -53.8	500 -37.4 7.9 -48.1	59 -42.9 0.40 -55.8
<b>227</b> EA4-1-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	100 000 -23.7 1700 -34.2	63 -42.8 0.51 -55.2	50 000 -25.5 220 -39.5	50 -43.3 0.26 -56.9	17 000 -28.4 200 -39.7	670 -36.7 6.1 -48.8	1200 -35.2 2.0 -51.7	17 -46.2 0.12 -58.9	130 -41.0 0.65 -54.5	330 -38.4 2.4 -51.2	830 -36.1 14 -46.6	100 -41.5 0.71 -54.3



No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>235</b> E13-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6300 -30.9 ND ND	6700 -30.7 ND ND	ND ND ND ND	17 000 -28.4 ND ND	25 000 -27.3 ND ND	3300 -32.5 ND ND	ND ND ND ND	4000 -32.0 ND ND	ND ND ND ND	12 000 -29.3 ND ND	2000 -33.8 ND ND	ND ND ND ND
<b>236</b> E13-4		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	290 -38.8 ND ND	5000 -31.5 ND ND	ND ND ND ND	≥200 000 ≥-22.0 ND ND	100 000 -23.7 ND ND	25 000 -27.3 ND ND	ND ND ND ND	100 000 -23.7 ND ND	ND ND ND ND	420 -37.9 ND ND	590 -37.0 ND ND	ND ND ND ND
<b>237</b> E13-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 ND ND	2200 -33.5 ND ND	ND ND ND ND	560 -37.1 ND ND	100 000 -23.7 ND ND	67 000 -24.8 ND ND	ND ND ND ND	670 -36.7 ND ND	ND ND ND ND	2500 -33.2 ND ND	1100 -35.3 ND ND	ND ND ND ND
<b>238</b> EA2-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 ND ND	36 -44.2 ND ND	25 000 -27.3 ND ND	33 -44.4 ND ND	100 000 -23.7 ND ND	290 -38.8 ND ND	200 -39.8 ND ND	50 -43.3 ND ND	2.5 -51.0 ND ND	6.7 -48.5 ND ND	17 -46.2 ND ND	11 -47.2 ND ND
<b>239</b> EA2-2 <sub>o</sub>		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	140 -40.6 ND ND	0.91 -53.7 ND ND	3300 -32.5 ND ND	25 -45.1 ND ND	770 -36.3 ND ND	13 -46.7 ND ND	56 -43.1 ND ND	0.45 -55.4 ND ND	3.3 -50.3 ND ND	22 -45.4 ND ND	5.6 -49.0 ND ND	0.86 -53.8 ND ND
<b>240</b> EA2-3 <sub>o</sub>		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	≥200 000 ≥-22.0 ND ND	50 000 -25.5 ND ND	≥200 000 ≥-22.0 ND ND	46 000 -25.8 ND ND	≥200 000 ≥-22.0 ND ND	20 000 -27.9 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	9600 -29.8 ND ND	82 000 -24.2 ND ND	69 000 -24.7 ND ND	100 000 -23.7 ND ND
<b>241</b> EA2-4		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6900 -30.6 ND ND	110 -41.3 ND ND	50 000 -25.5 ND ND	100 -41.5 ND ND	100 000 -23.7 ND ND	5000 -31.5 ND ND	360 -38.3 ND ND	150 -40.4 ND ND	2.9 -50.7 ND ND	22 -45.4 ND ND	38 -44.0 ND ND	40 -43.9 ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>242</b> EA2-4o		$K_{d,obs}$ (nM)	$\geq 200\,000$	$\geq 200\,000$	$\geq 200\,000$	9100	$\geq 200\,000$	100 000	100 000	$\geq 200\,000$	3300	10 000	110 000	6700
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	$\geq -22.0$	$\geq -22.0$	-29.9	$\geq -22.0$	-23.7	-23.7	$\geq -22.0$	-32.5	-29.7	-23.5	-30.7
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>243</b> EA2-5		$K_{d,obs}$ (nM)	13 000	170	15 000	290	100 000	1800	620	110	13	53	36	8.3
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.0	-40.2	-28.6	-38.8	-23.7	-34.1	-36.8	-41.3	-46.9	-43.2	-44.2	-47.9
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>244</b> EA2-7		$K_{d,obs}$ (nM)	14 000	910	33 000	ND	$\geq 200\,000$	ND	5600	10 000	ND	ND	ND	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-28.8	-35.9	-26.6	ND	$\geq -22.0$	ND	-31.2	-29.7	ND	ND	ND	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>245</b> EA2-8		$K_{d,obs}$ (nM)	50 000	ND	$\geq 200\,000$	ND	ND	ND	3300	2900	ND	ND	ND	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-25.5	ND	$\geq -22.0$	ND	ND	ND	-32.5	-32.9	ND	ND	ND	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>246</b> EA3-2		$K_{d,obs}$ (nM)	10 000	31	15 000	1.4	5600	330	1400	11	4.0	6.2	100	3.0
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.7	-44.5	-28.6	-52.5	-31.2	-38.4	-34.7	-47.2	-49.8	-48.7	-41.5	-50.6
		$K_{d,int}$ (nM)	96	0.14	38	0.0042	38	1.7	1.3	0.045	0.012	0.025	0.94	0.012
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.6	-58.4	-44.0	-67.5	-44.0	-52.0	-52.6	-61.4	-64.9	-62.9	-53.6	-64.8

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>247</b> EA3-2o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2000 -33.8 99 -41.6	5.0 -49.3 0.12 -58.9	8300 -30.1 110 -41.4	ND ND ND ND	1000 -35.6 35 -44.2	17 -46.2 0.44 -55.5	910 -35.9 4.4 -49.6	1.2 -52.8 0.026 -62.8	3.0 -50.6 0.046 -61.4	5.6 -49.0 0.11 -59.0	17 -46.2 0.81 -54.0	3.0 -50.6 0.062 -60.6
<b>248</b> EA3-3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 9.2 -47.7	10 -47.5 0.044 -61.5	13 000 -29.1 30 -44.7	10 -47.5 0.028 -62.6	590 -37.0 3.9 -49.9	77 -42.2 0.38 -55.9	1200 -35.0 1.1 -53.1	2.5 -51.0 0.0096 -65.4	1.2 -52.8 0.0035 -68.0	2.0 -51.6 0.0077 -66.0	29 -44.8 0.26 -56.9	1.1 -53.2 0.0042 -67.5
<b>249</b> EA3-3o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1400 -34.7 75 -42.3	3.3 -50.3 0.084 -59.8	25 000 -27.3 340 -38.4	33 -44.4 0.54 -55.0	330 -38.4 13 -46.9	10 -47.5 0.28 -56.7	1200 -35.0 6.5 -48.6	4.0 -49.8 0.088 -59.7	3.1 -50.5 0.051 -61.1	20 -45.7 0.44 -55.5	25 -45.1 1.3 -52.8	1.8 -51.9 0.040 -61.7
<b>250</b> EA3-4		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2100 -33.7 14 -46.6	13 -46.8 0.040 -61.7	50 000 -25.5 84 -42.0	33 -44.4 0.067 -60.4	500 -37.4 2.3 -51.2	150 -40.4 0.54 -55.0	1600 -34.5 1.0 -53.4	3.3 -50.3 0.0091 -65.5	15 -46.5 0.029 -62.5	10 -47.5 0.027 -62.7	91 -41.8 0.58 -54.8	13 -46.9 0.034 -62.1
<b>251</b> EA3-4o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	6300 -30.9 340 -38.4	36 -44.2 0.94 -53.6	14 000 -28.9 200 -39.8	250 -39.2 4.2 -49.7	710 -36.5 28 -44.8	77 -42.2 2.3 -51.3	2400 -33.4 13 -46.8	9.1 -47.7 0.21 -57.4	45 -43.6 0.77 -54.1	83 -42.0 1.9 -51.7	130 -41.0 6.7 -48.5	20 -45.7 0.46 -55.4

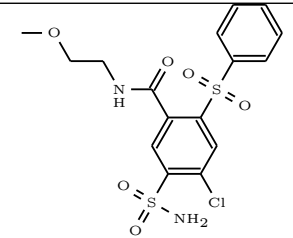
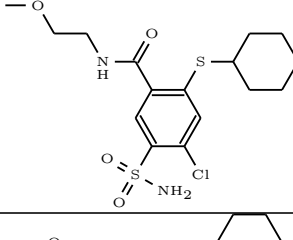
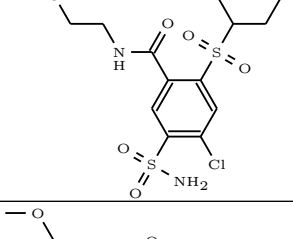
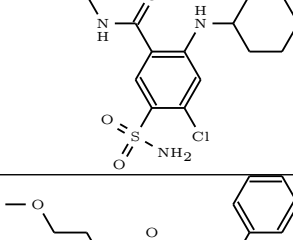
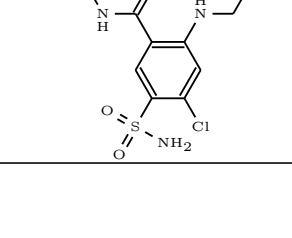


No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>252</b>		$K_{d,obs}$ (nM)	14 000	420	$\geq 200\ 000$	ND	50 000	50 000	33 000	3300	20	ND	670	ND
EA3-7		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-28.8	-37.9	$\geq -22.0$	ND	-25.5	-25.5	-26.6	-32.5	-45.7	ND	-36.7	ND
		$K_{d,int}$ (nM)	26	0.37	240	ND	66	50	6.0	2.6	0.011	ND	1.2	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.0	-56.0	-39.3	ND	-42.6	-43.3	-48.8	-51.0	-65.0	ND	-52.9	ND
<b>253</b>		$K_{d,obs}$ (nM)	6300	77	$\geq 200\ 000$	ND	ND	2000	6700	230	40	170	400	20
EA3-8		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-30.9	-42.2	$\geq -22.0$	ND	ND	-33.8	-30.7	-39.4	-43.9	-40.2	-38.0	-45.7
		$K_{d,int}$ (nM)	3.7	0.021	30	ND	ND	0.63	0.38	0.055	0.0072	0.041	0.23	0.0049
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-50.1	-63.3	-44.6	ND	ND	-54.6	-55.9	-60.9	-66.1	-61.7	-57.2	-67.1
<b>254</b>		$K_{d,obs}$ (nM)	13 000	10	13 000	ND	ND	ND	560	2.5	5.0	14	200	ND
AZ14-2		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.1	-47.5	-28.9	ND	ND	ND	-37.1	-51.0	-49.3	-46.6	-39.8	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>255</b>		$K_{d,obs}$ (nM)	670	3.3	3300	ND	4500	3.7	240	0.25	0.67	2.9	11	1.1
EA5-2o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-36.7	-50.3	-32.5	ND	-31.7	-50.0	-39.3	-57.0	-54.5	-50.7	-47.2	-53.1
		$K_{d,int}$ (nM)	33	0.079	43	ND	160	0.099	1.2	0.0051	0.010	0.059	0.54	0.023
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-44.4	-60.0	-43.7	ND	-40.3	-59.4	-53.0	-67.0	-65.3	-60.7	-55.0	-63.1
<b>256</b>		$K_{d,obs}$ (nM)	400	2.5	10 000	5.0	400	8.3	500	0.53	0.83	0.50	25	2.0
EA5-3		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-38.0	-51.0	-29.7	-49.3	-38.0	-47.9	-37.4	-55.1	-53.9	-55.2	-45.1	-51.6
		$K_{d,int}$ (nM)	3.7	0.011	24	0.014	2.6	0.041	0.45	0.0020	0.0023	0.0019	0.23	0.0077
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-50.1	-65.0	-45.2	-64.4	-50.9	-61.6	-55.5	-69.4	-69.0	-69.5	-57.3	-66.0

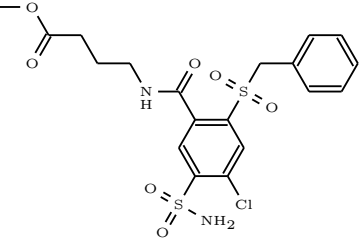
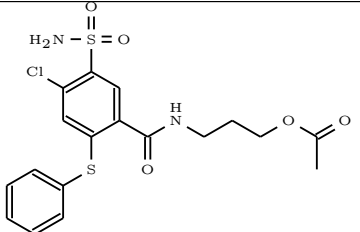
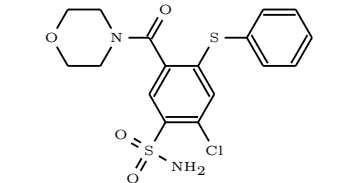
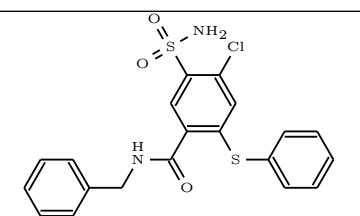
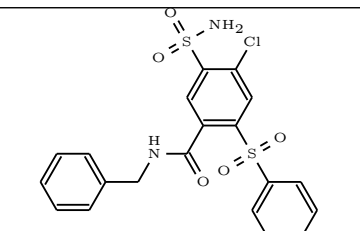
No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>257</b>		$K_{d,obs}$ (nM)	1100	1.4	8300	29	1500	1.1	310	0.63	0.43	2.5	7.1	1.1
EA5-3o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-35.3	-52.5	-30.1	-44.8	-34.5	-53.1	-38.6	-54.6	-55.6	-51.0	-48.3	-53.1
		$K_{d,int}$ (nM)	55	0.034	110	0.43	55	0.030	1.5	0.013	0.0066	0.051	0.35	0.023
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.1	-62.2	-41.4	-55.6	-43.1	-62.5	-52.4	-64.6	-66.4	-61.1	-56.1	-63.1
<b>258</b>		$K_{d,obs}$ (nM)	1800	2.9	≥200 000	ND	400	11	560	5.3	3.3	2.4	71	11
EA5-4		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-34.1	-50.7	≥-22.0	ND	-38.0	-47.2	-37.1	-49.1	-50.3	-51.2	-42.4	-47.3
		$K_{d,int}$ (nM)	11	0.0079	300	ND	1.7	0.035	0.32	0.013	0.0060	0.0058	0.41	0.026
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.3	-65.9	-38.7	ND	-52.1	-62.1	-56.4	-64.7	-66.6	-66.7	-55.7	-62.9
<b>259</b>		$K_{d,obs}$ (nM)	1500	2.0	20 000	ND	320	2.7	670	4.0	1.2	1.4	20	7.1
EA5-5		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-34.6	-51.6	-27.9	ND	-38.5	-50.8	-36.7	-49.8	-52.8	-52.5	-45.7	-48.3
		$K_{d,int}$ (nM)	7.6	0.0050	27	ND	1.2	0.0076	0.34	0.0087	0.0020	0.0031	0.10	0.015
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-48.2	-67.1	-44.9	ND	-52.9	-66.0	-56.2	-65.7	-69.4	-68.3	-59.3	-64.2
<b>260</b>		$K_{d,obs}$ (nM)	40 000	40 000	40 000	ND	40 000	ND	≥200 000	40 000	40 000	40 000	40 000	ND
EA5-5-1		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.1	-26.1	-26.1	ND	-26.1	ND	≥-22.0	-26.1	-26.1	-26.1	-26.1	ND
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>261</b>		$K_{d,obs}$ (nM)	≥200 000	910	≥200 000	ND	100 000	1200	17 000	17 000	20	ND	ND	140
EA5-7		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	≥-22.0	-35.9	≥-22.0	ND	-23.7	-35.0	-28.4	-28.4	-45.7	ND	ND	-40.6
		$K_{d,int}$ (nM)	370	0.80	96	ND	130	1.2	3.0	13	0.011	ND	ND	0.11
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-38.2	-54.0	-41.7	ND	-40.8	-52.8	-50.6	-46.8	-65.0	ND	ND	-59.1

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>262</b>		$K_{d,obs}$ (nM)	33 000	130	$\geq 200\,000$	ND	$\geq 200\,000$	7700	20 000	500	40	330	2000	140
EA5-8		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.6	-41.0	$\geq -22.0$	ND	$\geq -22.0$	-30.3	-27.9	-37.4	-43.9	-38.4	-33.8	-40.6
		$K_{d,int}$ (nM)	19	0.035	30	ND	84	2.4	1.1	0.12	0.0072	0.081	1.1	0.035
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.8	-62.1	-44.6	ND	-42.0	-51.1	-53.1	-58.8	-66.1	-59.9	-53.1	-62.1
<b>263</b>		$K_{d,obs}$ (nM)	$\geq 200\,000$	130	$\geq 200\,000$	ND	$\geq 200\,000$	6700	20 000	2000	10	670	ND	12
EA5-9		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	-41.0	$\geq -22.0$	ND	$\geq -22.0$	-30.7	-27.9	-33.8	-47.5	-36.7	ND	-47.0
		$K_{d,int}$ (nM)	370	0.11	96	ND	270	6.6	3.6	1.5	0.0057	0.51	ND	0.0094
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-38.2	-59.1	-41.7	ND	-39.0	-48.5	-50.1	-52.3	-66.7	-55.1	ND	-65.4
<b>264</b>		$K_{d,obs}$ (nM)	6700	5.0	33 000	1.7	4500	130	830	1.2	2.0	0.83	180	5.6
EA4-2		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-30.7	-49.3	-26.6	-52.1	-31.7	-41.0	-36.1	-52.8	-51.6	-53.9	-40.0	-49.0
		$K_{d,int}$ (nM)	69	0.025	89	0.0053	34	0.69	0.84	0.0054	0.0063	0.0036	1.8	0.024
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.5	-63.0	-41.8	-66.9	-44.4	-54.4	-53.9	-66.9	-66.5	-67.9	-51.8	-63.0
<b>265</b>		$K_{d,obs}$ (nM)	1400	3.3	17 000	28	5600	19	1400	0.33	1.5	3.1	67	4.0
EA4-2o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-34.7	-50.3	-28.4	-44.9	-31.2	-45.8	-34.7	-56.2	-52.3	-50.5	-42.6	-49.8
		$K_{d,int}$ (nM)	70	0.079	210	0.42	200	0.50	6.9	0.0069	0.023	0.064	3.2	0.082
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.4	-60.0	-39.6	-55.7	-39.8	-55.2	-48.4	-66.2	-63.1	-60.5	-50.4	-59.8
<b>266</b>		$K_{d,obs}$ (nM)	1200	3.7	25 000	33	430	29	1700	0.67	0.71	1.0	67	2.0
EA4-3		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-35.0	-50.0	-27.3	-44.4	-37.8	-44.8	-34.3	-54.5	-54.3	-53.4	-42.6	-51.6
		$K_{d,int}$ (nM)	16	0.023	84	0.13	4.0	0.20	2.1	0.0036	0.0028	0.0054	0.84	0.011
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-46.2	-63.2	-42.0	-58.6	-49.8	-57.6	-51.5	-67.9	-68.5	-66.9	-53.8	-65.1

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>267</b> EA4-3o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 44 -43.6	1.1 -53.3 0.022 -63.2	33 000 -26.6 380 -38.1	ND ND ND ND	1400 -34.7 45 -43.6	11 -47.2 0.27 -56.8	1200 -35.0 5.4 -49.1	1.4 -52.5 0.026 -62.8	0.67 -54.5 0.0091 -65.5	8.3 -47.9 0.15 -58.2	50 -43.3 2.2 -51.4	5.0 -49.3 0.092 -59.6
<b>268</b> EA4-7		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	33 000 -26.6 49 -43.4	190 -39.9 0.13 -58.6	160 000 -22.5 60 -42.8	ND ND ND ND	160 000 -22.5 170 -40.2	25 000 -27.3 20 -45.7	25 000 -27.3 3.6 -50.1	1400 -34.7 0.87 -53.8	8.3 -47.9 0.0038 -67.8	21 -45.6 0.013 -64.7	ND ND ND ND	77 -42.2 0.047 -61.3
<b>269</b> EA4-8		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	25 000 -27.3 15 -46.5	20 -45.7 0.0056 -66.8	50 000 -25.5 7.6 -48.2	ND ND ND ND	48 000 -25.7 20 -45.7	7700 -30.3 2.4 -51.1	13 000 -29.1 0.72 -54.3	67 -42.6 0.016 -64.0	31 -44.6 0.0056 -66.8	130 -41.0 0.030 -62.4	1100 -35.3 0.64 -54.6	48 -43.5 0.012 -64.9
<b>270</b> EA4-8b		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	25 000 -27.3 ND ND	10 000 -29.7 ND ND	50 000 -25.5 ND ND	ND ND ND ND	140 000 -22.8 ND ND	100 000 -23.7 ND ND	100 000 -23.7 ND ND	100 000 -23.7 ND ND	ND ND ND ND	20 000 -27.9 ND ND	25 000 -27.3 ND ND	6700 -30.7 ND ND
<b>271</b> EA8-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	5000 -31.5 46 -43.6	8.3 -47.9 0.037 -61.9	10 000 -29.7 24 -45.2	1.4 -52.5 0.0040 -67.6	4500 -31.7 30 -44.6	40 -43.9 0.20 -57.6	670 -36.7 0.60 -54.7	2.5 -51.0 0.0096 -65.4	1.7 -52.1 0.0047 -67.2	2.5 -51.0 0.0096 -65.4	140 -40.6 1.3 -52.8	2.5 -51.0 0.0096 -65.4

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>272</b> EA8-2o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3300 -32.5 160 -40.3	3.3 -50.3 0.079 -60.0	6700 -30.7 85 -42.0	10 -47.5 0.15 -58.3	2000 -33.8 71 -42.4	7.7 -48.2 0.20 -57.5	770 -36.3 3.7 -50.0	0.50 -55.2 0.010 -65.2	1.6 -52.3 0.024 -63.1	5.6 -49.0 0.11 -59.0	36 -44.2 1.7 -52.0	1.0 -53.4 0.021 -63.4
<b>273</b> EA8-3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	670 -36.7 6.1 -48.7	4.0 -49.8 0.018 -63.8	20 000 -27.9 48 -43.5	10 -47.5 0.028 -62.6	140 -40.6 0.94 -53.6	13 -46.7 0.066 -60.4	670 -36.7 0.60 -54.7	0.67 -54.5 0.0026 -68.8	1.4 -52.5 0.0040 -67.6	1.7 -52.1 0.0064 -66.4	33 -44.4 0.30 -56.5	1.7 -52.1 0.0064 -66.4
<b>274</b> EA8-3o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2500 -33.2 120 -41.0	2.6 -50.9 0.062 -60.6	20 000 -27.9 260 -39.1	50 -43.3 0.76 -54.1	330 -38.4 12 -47.0	22 -45.4 0.59 -54.8	670 -36.7 3.2 -50.4	2.5 -51.0 0.051 -61.1	1.0 -53.4 0.015 -64.2	20 -45.7 0.41 -55.7	50 -43.3 2.4 -51.1	2.9 -50.7 0.059 -60.7
<b>275</b> EA8-7		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 37 -44.1	330 -38.4 0.29 -56.6	100 000 -23.7 48 -43.4	ND ND ND ND	100 000 -23.7 130 -40.8	13 000 -29.1 12 -46.9	10 000 -29.7 1.8 -51.9	2900 -32.9 2.2 -51.4	ND ND ND ND	ND ND ND ND	ND ND ND ND	67 -42.6 0.051 -61.1
<b>276</b> EA8-8		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 15 -46.5	50 -43.3 0.018 -63.8	≥200 000 ≥-22.0 38 -44.0	ND ND ND ND	14 000 -28.8 7.6 -48.2	3600 -32.3 1.4 -52.5	5600 -31.2 0.40 -55.8	130 -41.0 0.038 -61.8	33 -44.4 0.0075 -66.0	250 -39.2 0.077 -60.0	1000 -35.6 0.72 -54.3	33 -44.4 0.010 -65.2

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>277</b>		$K_{d,obs}$ (nM)	3300	13	$\geq 200\ 000$	130	250	33	2200	9.1	2.2	0.40	130	1.8
EA12-3		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-32.5	-46.9	$\geq -22.0$	-40.9	-39.2	-44.4	-33.5	-47.7	-51.4	-55.8	-41.0	-51.9
		$K_{d,int}$ (nM)	31	0.055	480	0.36	1.6	0.17	2.0	0.035	0.0063	0.0015	1.1	0.0070
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-44.6	-60.9	-37.5	-56.1	-52.1	-58.1	-51.6	-62.1	-66.5	-70.1	-53.1	-66.2
<b>278</b>		$K_{d,obs}$ (nM)	34 000	100	33 000	ND	5600	400	9100	29	300	40	830	50
EA12-4o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.5	-41.5	-26.6	ND	-31.2	-38.0	-29.9	-44.7	-38.7	-43.9	-36.1	-43.3
		$K_{d,int}$ (nM)	1900	2.6	480	ND	220	12	49	0.68	5.1	0.92	45	1.1
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-34.0	-50.9	-37.5	ND	-39.5	-47.0	-43.4	-54.4	-49.2	-53.6	-43.6	-53.1
<b>279</b>		$K_{d,obs}$ (nM)	2000	10	$\geq 200\ 000$	96	250	6.7	1700	3.3	2.0	1.2	100	2.0
EA11-3		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.8	-47.5	$\geq -22.0$	-41.6	-39.2	-48.5	-34.3	-50.3	-51.6	-52.8	-41.5	-51.6
		$K_{d,int}$ (nM)	18	0.044	480	0.27	1.6	0.033	1.5	0.013	0.0056	0.0048	0.90	0.0077
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.9	-61.5	-37.5	-56.8	-52.1	-62.2	-52.4	-64.7	-66.8	-67.2	-53.7	-66.0
<b>280</b>		$K_{d,obs}$ (nM)	2000	4.3	71 000	110	1600	14	1100	20	1.0	12	50	3.0
EA11-3o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.8	-49.6	-24.6	-41.2	-34.4	-46.6	-35.3	-45.7	-53.4	-47.1	-43.3	-50.6
		$K_{d,int}$ (nM)	99	0.10	910	1.7	57	0.38	5.4	0.41	0.015	0.24	2.4	0.062
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.6	-59.3	-35.8	-52.0	-43.0	-55.9	-49.1	-55.7	-64.2	-57.1	-51.1	-60.6
<b>281</b>		$K_{d,obs}$ (nM)	3200	7.8	$\geq 200\ 000$	11	670	43	1700	4.3	46	7.3	180	5.9
EA11-4		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-32.6	-48.1	$\geq -22.0$	-47.2	-36.6	-43.7	-34.3	-49.7	-43.6	-48.3	-40.1	-48.8
		$K_{d,int}$ (nM)	19	0.022	300	0.020	2.8	0.14	0.95	0.010	0.081	0.018	1.0	0.014
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.9	-63.3	-38.7	-63.5	-50.8	-58.5	-53.5	-65.2	-59.9	-63.8	-53.4	-64.4

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>282</b> EA11-4o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	15 000 -28.7 810 -36.2	50 -43.3 1.3 -52.7	67 000 -24.8 950 -35.7	560 -37.1 9.4 -47.6	5000 -31.5 200 -39.8	140 -40.6 4.2 -49.7	3300 -32.5 18 -46.0	12 -47.1 0.27 -56.8	29 -44.8 0.48 -55.3	120 -41.1 2.7 -50.8	310 -38.6 17 -46.1	30 -44.6 0.70 -54.3
<b>283</b> EA4-2c		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 86 -41.9	25 -45.1 0.10 -59.3	77 000 -24.4 170 -40.2	2.9 -50.7 0.0076 -66.0	2200 -33.5 14 -46.7	100 -41.5 0.46 -55.4	1400 -34.7 1.2 -52.9	7.7 -48.2 0.028 -62.7	5.0 -49.3 0.013 -64.6	10 -47.5 0.036 -62.0	330 -38.4 2.8 -50.8	6.2 -48.7 0.022 -63.2
<b>284</b> EA7-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\ 000$ $\geq -22.0$ 1800 -34.0	1000 -35.6 4.4 -49.6	$\geq 200\ 000$ $\geq -22.0$ 480 -37.5	2900 -32.9 8.1 -48.0	$\geq 200\ 000$ $\geq -22.0$ 1300 -34.9	12 000 -29.3 58 -42.9	14 000 -28.8 13 -46.8	670 -36.7 2.6 -51.0	ND ND ND ND	3300 -32.5 13 -46.8	7700 -30.3 69 -42.5	670 -36.7 2.6 -51.0
<b>285</b> EA10-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	330 -38.4 3.1 -50.5	4.5 -49.5 0.020 -63.5	2800 -33.0 6.6 -48.5	9.1 -47.7 0.026 -62.9	1800 -34.1 12 -47.1	10 -47.4 0.051 -61.1	190 -39.9 0.17 -58.0	9.1 -47.7 0.035 -62.1	7.7 -48.2 0.022 -63.3	1.7 -52.1 0.0064 -66.4	150 -40.4 1.4 -52.6	2.9 -50.7 0.011 -65.0
<b>286</b> EA10-2o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	91 -41.8 4.5 -49.5	1.2 -52.9 0.029 -62.6	1600 -34.4 20 -45.7	32 -44.5 0.49 -55.3	11 000 -29.5 370 -38.1	9.1 -47.7 0.24 -57.1	91 -41.8 0.44 -55.5	0.22 -57.3 0.0046 -67.3	1.2 -53.0 0.018 -63.8	5.6 -49.0 0.11 -59.0	16 -46.2 0.79 -54.0	1.4 -52.5 0.029 -62.5

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>287</b> EA10-3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	83 -42.0 0.76 -54.1	1.4 -52.5 0.0063 -66.5	4300 -31.8 10 -47.4	86 -41.9 0.24 -57.1	170 -40.1 1.1 -53.1	1.4 -52.5 0.0071 -66.2	220 -39.5 0.20 -57.6	2.6 -50.9 0.010 -65.3	1.1 -53.1 0.0031 -68.3	1.0 -53.4 0.0038 -67.8	50 -43.3 0.45 -55.5	1.2 -52.8 0.0048 -67.2
<b>288</b> EA10-3o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	200 -39.8 9.9 -47.5	1.0 -53.4 0.024 -63.1	4000 -32.0 51 -43.3	220 -39.5 3.3 -50.3	500 -37.4 1.8 -46.0	1.9 -51.8 0.050 -61.1	110 -41.4 0.51 -55.1	1.1 -53.1 0.023 -63.1	0.83 -53.9 0.013 -64.7	7.7 -48.2 0.16 -58.2	14 -46.6 0.69 -54.4	2.3 -51.3 0.047 -61.3
<b>289</b> EA10-8		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	4000 -32.0 2.3 -51.2	40 -43.9 0.011 -65.0	≥200 000 ≥-22.0 30 -44.6	ND ND ND ND	100 000 -23.7 42 -43.8	1200 -35.2 0.37 -56.0	3300 -32.5 0.19 -57.7	130 -41.0 0.030 -62.4	25 -45.1 0.0045 -67.3	330 -38.4 0.081 -59.9	2000 -33.8 1.1 -53.1	15 -46.4 0.0038 -67.8
<b>290</b> EA9-11		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	45 000 -25.8 260 -39.0	420 -37.9 1.2 -53.0	≥200 000 ≥-22.0 300 -38.7	330 -38.4 0.60 -54.7	5600 -31.2 23 -45.3	360 -38.3 1.1 -53.1	5000 -31.5 2.9 -50.7	110 -41.3 0.27 -56.8	91 -41.8 0.16 -58.1	180 -40.0 0.44 -55.5	710 -36.5 4.1 -49.8	110 -41.3 0.27 -56.8
<b>291</b> EA9-11o		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	50 000 -25.5 1600 -34.4	330 -38.4 5.1 -49.2	≥200 000 ≥-22.0 1600 -34.3	1100 -35.4 11 -47.3	4800 -31.6 110 -41.3	140 -40.6 2.4 -51.1	4800 -31.6 15 -46.5	140 -40.6 1.9 -51.8	130 -41.0 1.2 -52.9	360 -38.3 4.7 -49.4	910 -35.9 28 -44.8	130 -41.0 1.7 -52.1

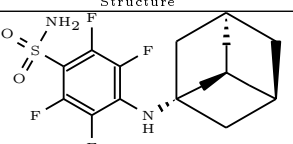
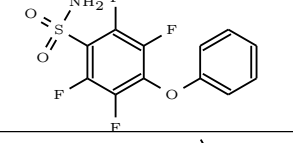
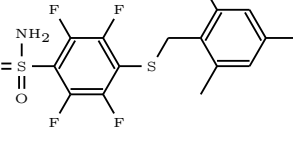
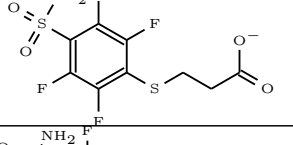
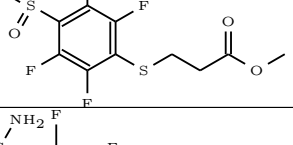
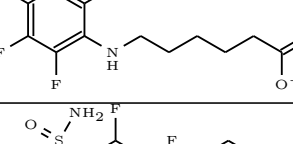
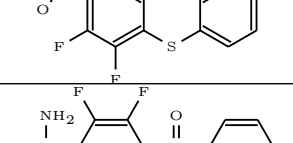
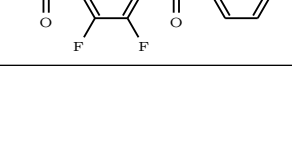


No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>292</b>		$K_{d,obs}$ (nM)	2000	130	$\geq 200\,000$	56	6700	110	5000	63	77	130	360	130
EA9-2		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.8	-41.0	$\geq -22.0$	-43.1	-30.7	-41.3	-31.5	-42.8	-42.2	-41.0	-38.3	-41.0
		$K_{d,int}$ (nM)	18	0.55	480	0.16	44	0.55	4.5	0.24	0.22	0.48	3.2	0.48
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.9	-55.0	-37.5	-58.2	-43.7	-55.0	-49.5	-57.1	-57.4	-55.3	-50.4	-55.3
<b>293</b>		$K_{d,obs}$ (nM)	1200	20	$\geq 200\,000$	ND	10\,000	ND	1700	11	ND	91	67	5.0
EA9-2o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-35.0	-45.7	$\geq -22.0$	ND	-29.7	ND	-34.3	-47.2	ND	-41.8	-42.6	-49.3
		$K_{d,int}$ (nM)	62	0.47	2600	ND	350	ND	8.1	0.23	ND	1.9	3.2	0.10
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.8	-55.3	-33.2	ND	-38.3	ND	-48.0	-57.2	ND	-51.8	-50.4	-59.3
<b>294</b>		$K_{d,obs}$ (nM)	560	50	$\geq 200\,000$	100	2000	4.0	5600	20	3.3	33	130	8.3
EA9-3		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-37.1	-43.3	$\geq -22.0$	-41.5	-33.8	-49.8	-31.2	-45.7	-50.3	-44.4	-41.0	-47.9
		$K_{d,int}$ (nM)	5.1	0.22	480	0.28	13	0.020	5.0	0.077	0.0094	0.13	1.1	0.032
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-49.2	-57.3	-37.5	-56.7	-46.8	-63.5	-49.3	-60.0	-65.4	-58.7	-53.1	-62.3
<b>295</b>		$K_{d,obs}$ (nM)	2000	22	$\geq 200\,000$	400	13\,000	7.7	3300	17	2.0	33	56	4.0
EA9-3o		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.8	-45.4	$\geq -22.0$	-38.0	-29.1	-48.2	-32.5	-46.2	-51.6	-44.4	-43.1	-49.8
		$K_{d,int}$ (nM)	99	0.52	2600	6.1	440	0.20	16	0.34	0.030	0.69	2.7	0.082
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.6	-55.1	-33.2	-48.8	-37.7	-57.5	-46.2	-56.2	-62.4	-54.4	-50.9	-59.8
<b>296</b>		$K_{d,obs}$ (nM)	1900	59	$\geq 200\,000$	180	180	ND	2500	11	29	83	110	13
EA9-4		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.9	-42.9	$\geq -22.0$	-40.0	-40.0	ND	-33.2	-47.2	-44.8	-42.0	-41.3	-46.7
		$K_{d,int}$ (nM)	11	0.16	300	0.32	0.76	ND	1.4	0.027	0.051	0.20	0.63	0.032
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.2	-58.1	-38.7	-56.3	-54.1	ND	-52.5	-62.7	-61.1	-57.5	-54.6	-62.3



No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>302</b> VR14-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	56 000 -25.3 ND ND	5300 -31.3 ND ND	100 000 -23.7 ND ND	4500 -31.7 ND ND	4000 -32.0 ND ND	13 000 -29.0 ND ND	5900 -31.0 ND ND	13 000 -29.1 ND ND	5000 -31.5 ND ND	2200 -33.5 ND ND	2600 -33.2 ND ND	1700 -34.3 ND ND
<b>Fluorinated compounds</b>														
<b>303</b> TFMSA		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	61 -42.8 51 -43.3	21 -45.6 8.4 -47.9	1000 -35.6 220 -39.5	65 -42.7 17 -46.2	39 -44.0 24 -45.3	ND ND ND ND	14 -46.6 1.2 -53.0	8.3 -47.9 2.9 -50.7	43 -43.7 11 -47.2	110 -41.3 38 -44.0	40 -43.9 33 -44.4	43 -43.7 15 -46.4
<b>304</b> VD12-22		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	4.1 -49.8 0.22 -57.3	29 -44.8 0.73 -54.2	29 000 -26.9 400 -38.0	560 -37.1 9.2 -47.7	290 -38.8 11 -47.2	1.8 -51.9 0.053 -61.0	670 -36.7 3.5 -50.2	11 -47.2 2.5 -57.0	150 -40.5 7.5 -51.1	330 -38.4 2.5 -48.2	20 -45.7 1.1 -53.3	56 -43.1 1.2 -52.8
<b>305</b> VD10-9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3.3 -50.3 0.22 -57.3	46 -43.6 1.4 -52.5	ND ND ND ND	740 -36.4 15 -46.4	450 -37.7 21 -45.6	38 -44.0 1.3 -52.7	430 -37.8 2.7 -50.8	56 -43.0 1.5 -52.3	150 -40.5 3.0 -50.6	780 -36.3 21 -45.5	76 -42.2 4.9 -49.3	35 -44.2 0.96 -53.5
<b>306</b> VD12-05		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.058 -60.8 0.0035 -68.0	2.2 -51.3 0.065 -60.4	3800 -32.2 60 -42.9	100 -41.4 2.0 -51.7	200 -39.8 8.8 -47.8	0.050 -61.1 0.0017 -69.9	140 -40.6 0.86 -53.8	1.1 -53.1 0.028 -62.6	5.4 -49.1 0.10 -59.3	37 -44.1 0.93 -53.6	2.4 -51.2 0.14 -58.4	3.6 -50.1 0.093 -59.5
<b>307</b> VD10-13		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.15 -58.3 0.0094 -65.4	11 -47.3 0.32 -56.4	29 000 -26.9 480 -37.5	440 -37.7 8.5 -47.9	400 -38.0 18 -46.0	1.7 -52.1 0.056 -60.8	200 -39.8 1.2 -52.9	13 -46.8 0.34 -56.2	32 -44.5 0.61 -54.7	220 -39.5 5.8 -48.9	11 -47.2 0.68 -54.4	5.0 -49.3 0.13 -58.7
<b>308</b> AZ13-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.88 -53.7 0.22 -57.3	20 -45.7 2.4 -51.2	33 000 -26.6 2200 -33.6	2000 -33.8 150 -40.4	200 -39.8 36 -44.2	40 -43.9 5.4 -49.1	500 -37.4 12 -46.9	14 -46.6 1.5 -52.4	29 -44.7 2.3 -51.3	250 -39.2 26 -45.0	50 -43.3 12 -46.9	29 -44.8 3.0 -50.6
<b>309</b> VD12-01		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.32 -56.4 0.020 -63.5	15 -46.4 0.45 -55.5	ND ND ND ND	290 -38.8 5.5 -49.0	330 -38.4 15 -46.4	17 -46.2 0.56 -54.9	1000 -35.6 6.1 -48.7	5.0 -49.3 0.13 -58.7	67 -42.6 1.3 -52.8	50 -43.3 1.3 -52.7	6.7 -48.5 0.41 -55.7	83 -42.0 2.2 -51.4
<b>310</b> VD10-35		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.20 -57.6 0.064 -60.5	17 -46.2 2.5 -51.0	20 000 -27.9 1700 -34.3	510 -37.3 50 -43.3	310 -38.6 71 -42.4	22 -45.4 3.8 -50.0	67 -42.6 2.1 -51.5	7.1 -48.3 0.95 -53.5	41 -43.9 4.0 -49.8	250 -39.2 33 -44.4	29 -44.8 8.9 -47.8	33 -44.4 4.4 -49.6

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
311 VD10-49		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1.1 -53.3 0.13 -58.8	0.65 -54.5 0.037 -61.9	ND ND ND ND	730 -36.4 27 -44.9	200 -39.8 17 -46.1	2.0 -51.6 0.13 -58.7	200 -39.8 2.3 -51.2	0.22 -57.3 0.011 -65.0	5.1 -49.2 0.19 -57.7	120 -41.1 5.9 -48.8	0.32 -55.2 0.037 -61.9	0.50 -55.2 0.025 -62.9
312 VD10-28		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.40 -55.8 0.063 -60.5	6.7 -48.5 0.50 -55.2	ND ND ND ND	87 -41.9 4.2 -49.7	25 -45.1 2.8 -50.7	5.0 -49.3 0.42 -55.6	220 -39.5 3.4 -50.2	13 -46.9 0.82 -53.9	8.3 -47.9 0.40 -55.8	110 -41.3 7.3 -48.3	2.5 -51.0 0.39 -55.9	5.0 -49.3 0.33 -56.3
313 VD10-14		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	13 -46.7 0.18 -57.9	91 -41.8 0.57 -54.8	ND ND ND ND	1200 -35.2 4.8 -49.4	1100 -35.4 10 -47.4	1000 -35.6 7.1 -48.4	1000 -35.6 1.3 -52.7	300 -38.7 1.7 -52.1	710 -36.5 2.9 -50.7	1100 -35.3 6.2 -48.7	140 -40.6 1.9 -51.8	170 -40.2 0.92 -53.6
314 VD10-16		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.20 -57.6 0.0061 -66.6	9.1 -47.7 0.13 -58.6	ND ND ND ND	800 -36.2 7.5 -48.2	1000 -35.6 22 -45.5	8.3 -47.9 0.14 -58.5	1200 -35.0 3.7 -50.0	44 -43.7 0.55 -54.9	25 -45.1 0.23 -57.2	330 -38.4 4.2 -49.7	5.0 -49.3 0.15 -58.3	3.8 -50.0 0.048 -61.2
315 VD12-70		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.17 -58.0 0.0048 -67.2	10 -47.5 0.14 -58.6	ND ND ND ND	67000 -24.8 580 -37.0	500 -37.4 10 -47.4	ND ND ND ND	1800 -34.1 5.1 -49.2	20 -45.7 0.24 -57.1	18 -45.9 0.16 -58.1	330 -38.4 4.0 -49.9	2.5 -51.0 0.070 -60.3	6.7 -48.5 0.079 -60.0
316 VD12-13		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.50 -55.2 0.011 -65.0	1.7 -52.1 0.018 -63.8	ND ND ND ND	360 -38.3 2.4 -51.1	330 -38.4 5.3 -49.1	1.9 -51.7 0.023 -63.1	ND ND ND ND	0.50 -55.2 0.0046 -67.3	11 -47.2 0.076 -60.1	150 -40.4 1.4 -52.5	0.40 -55.8 0.0087 -65.6	6.7 -48.5 0.062 -60.6
317 VD10-20		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2.0 -51.6 0.028 -62.7	3.5 -50.2 0.023 -63.1	ND ND ND ND	300 -38.7 1.3 -52.8	2000 -33.8 20 -45.7	5.0 -49.3 0.037 -61.9	25000 -27.3 34 -44.3	43 -43.7 0.25 -57.0	50 -43.3 0.21 -57.4	5000 -31.5 29 -44.7	2.2 -51.4 0.030 -62.4	50 -43.3 0.29 -56.6
318 VD12-63		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.053 -61.0 0.0026 -68.8	13 -46.9 0.29 -56.6	ND ND ND ND	3600 -32.3 53 -43.2	520 -37.3 18 -46.0	25 -45.1 0.65 -54.5	1700 -34.3 7.9 -48.1	14 -46.6 0.29 -56.6	15 -46.4 0.22 -57.3	100 -41.5 2.0 -51.6	13 -46.9 0.59 -54.8	8.3 -47.9 0.17 -58.0
319 VD10-12		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.098 -59.4 0.0022 -69.2	18 -45.9 0.19 -57.7	ND ND ND ND	1600 -34.3 11 -47.2	1200 -35.0 20 -45.7	1000 -35.6 12 -47.0	1100 -35.3 2.4 -51.1	46 -43.6 0.42 -55.6	50 -43.3 0.34 -56.2	500 -37.4 4.6 -49.5	28 -44.9 0.60 -54.7	14 -46.6 0.13 -58.6

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>320</b> VD10-51		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.050 -61.1 0.0012 -70.8	5.0 -49.3 0.057 -60.8	ND ND ND ND	450 -37.7 3.3 -50.4	250 -39.2 4.3 -49.7	5.0 -49.3 0.064 -60.5	500 -37.4 1.2 -53.0	1.0 -53.4 0.0099 -65.3	3.3 -50.3 0.024 -63.0	17 -46.2 0.17 -58.1	CA XIII 0.50 -55.2 0.012 -64.9	CA XIV 0.67 -54.5 0.0066 -66.3
<b>321</b> VD12-47		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.10 -59.3 0.011 -65.0	1.6 -52.2 0.085 -59.8	ND ND ND ND	830 -36.1 29 -44.8	130 -40.8 11 -47.3	1.0 -53.4 0.061 -60.6	400 -38.0 4.4 -49.6	1.0 -53.4 0.047 -61.3	17 -46.2 0.58 -54.8	50 -43.3 2.3 -51.2	CA XIII 1.0 -53.4 0.11 -59.1	CA XIV 3.3 -50.3 0.16 -58.2
<b>322</b> VD11-49		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.067 -60.4 0.0044 -67.4	3.3 -50.3 0.10 -59.2	ND ND ND ND	20 000 -27.9 400 -38.0	3300 -32.5 160 -40.4	3.3 -50.3 0.12 -58.9	20 000 -27.9 130 -40.9	2.5 -51.0 0.068 -60.3	7.7 -48.2 0.15 -58.2	100 -41.5 2.7 -50.8	CA XIII 3.3 -50.3 0.21 -57.4	CA XIV 1.7 -52.1 0.045 -61.4
<b>323</b> VD11-56		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.40 -55.8 0.036 -62.0	20 -45.7 0.86 -53.8	ND ND ND ND	400 -38.0 11 -47.2	290 -38.8 18 -45.9	67 -42.6 3.2 -50.4	500 -37.4 4.4 -49.6	10 -47.5 0.37 -55.9	50 -43.3 1.4 -52.6	91 -41.8 3.4 -50.3	CA XIII 20 -45.7 1.8 -52.0	CA XIV 33 -44.4 1.2 -52.8
<b>324</b> AZ14-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.33 -56.2 ND ND	5.0 -49.3 ND ND	20 000 -27.9 ND ND	ND ND ND ND	ND ND ND ND	ND ND ND ND	500 -37.4 ND ND	1.7 -52.1 ND ND	20 -45.7 ND ND	150 -40.4 ND ND	CA XIII 3.3 -50.3 ND ND	CA XIV ND -23.7 ND ND
<b>325</b> VD10-21a		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.14 -58.5 0.0040 -67.6	67 -42.6 0.93 -53.6	ND ND ND ND	570 -37.1 5.1 -49.2	400 -38.0 8.4 -47.9	200 -39.8 3.1 -50.5	2900 -32.8 8.4 -47.9	150 -40.5 1.8 -51.9	77 -42.2 0.69 -54.4	170 -40.2 2.0 -51.6	CA XIII 14 -46.6 0.41 -55.7	CA XIV 10 -47.5 0.12 -58.8
<b>326</b> VD10-18		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.094 -59.5 0.012 -64.8	3.4 -50.3 0.20 -57.5	ND ND ND ND	240 -39.3 9.5 -47.6	500 -37.4 46 -43.6	1.0 -53.4 0.068 -60.3	200 -39.8 2.5 -51.1	6.3 -48.7 0.33 -56.3	11 -47.3 0.41 -55.7	18 -45.9 0.97 -53.5	CA XIII 1.3 -52.6 0.17 -58.0	CA XIV 100 000 -23.7 5300 -31.3
<b>327</b> VD11-51		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.050 -61.1 0.021 -63.3	3.3 -50.3 0.68 -54.4	ND ND ND ND	290 -38.8 38 -44.0	ND ND ND ND	5.0 -49.3 1.1 -53.1	160 -40.4 6.6 -48.5	0.67 -54.5 0.12 -58.9	0.77 -54.1 0.10 -59.3	17 -46.2 3.0 -50.6	CA XIII 2.5 -51.0 1.0 -53.3	CA XIV 0.67 -54.5 0.12 -58.9

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>328</b> VD11-61		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.025 -62.9 0.00066 -72.3	3.3 -50.3 0.042 -61.6	ND ND ND ND	1200 -35.0 10 -47.4	430 -37.8 8.3 -48.0	5.0 -49.3 0.072 -60.2	330 -38.4 0.87 -53.8	2.5 -51.0 0.028 -62.7	5.0 -49.3 0.041 -61.7	140 -40.6 1.6 -52.2	2.0 -51.6 0.052 -61.0	6.7 -48.5 0.074 -60.1
<b>329</b> VD11-9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.32 -56.4 0.024 -63.0	1.7 -52.1 0.061 -60.6	ND ND ND ND	810 -36.1 19 -45.8	200 -39.8 11 -47.3	0.56 -54.9 0.023 -63.1	400 -38.0 3.0 -50.6	0.83 -53.9 0.026 -62.8	5.8 -48.9 0.13 -58.6	76 -42.2 2.4 -51.1	0.27 -56.8 0.020 -63.5	1.4 -52.5 0.045 -61.4
<b>330</b> VD11-10		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	0.25 -57.0 0.087 -59.7	1.2 -52.8 0.21 -57.5	ND ND ND ND	2500 -33.2 270 -39.0	140 -40.6 36 -44.2	ND ND ND ND	140 -40.6 4.8 -49.3	1.2 -52.8 0.18 -57.8	22 -45.4 2.4 -51.2	77 -42.2 11 -47.2	0.40 -55.8 0.14 -58.5	13 -46.9 1.8 -51.9
<b>331</b> VD10-45		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	14 -46.6 2.2 -51.3	5.8 -48.9 0.43 -55.6	ND ND ND ND	83 -42.0 4.0 -49.8	330 -38.4 38 -44.1	6.7 -48.5 0.57 -54.9	140 -40.6 2.2 -51.4	1.7 -52.1 0.11 -59.1	1.0 -53.4 0.048 -61.2	540 -37.2 35 -44.2	2.0 -51.6 0.31 -56.4	40 -43.9 2.6 -50.9
<b>332</b> VD10-50		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2.9 -50.7 0.23 -57.2	9.6 -47.6 0.37 -56.0	ND ND ND ND	1800 -34.1 44 -43.7	2000 -33.8 120 -41.2	1.4 -52.5 0.062 -60.6	1000 -35.6 7.9 -48.1	10 -47.5 0.34 -56.2	18 -46.0 0.44 -55.5	280 -38.8 9.6 -47.6	2.9 -50.7 0.23 -57.2	1.7 -52.1 0.056 -60.8
<b>333</b> VD12-31		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 19 -45.8	4000 -32.0 37 -44.1	ND ND ND ND	ND ND ND ND	20 000 -27.9 280 -38.9	ND ND ND ND	11 000 -29.4 21 -45.5	33 000 -26.6 270 -39.0	670 -36.7 4.0 -49.9	20 000 -27.9 160 -40.3	5000 -31.5 95 -41.7	2900 -32.9 23 -45.3
<b>334</b> VD12-37		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	560 -37.1 12 -47.0	670 -36.7 6.9 -48.4	ND ND ND ND	13 000 -29.1 83 -42.0	5000 -31.5 78 -42.2	610 -36.9 7.1 -48.3	13 000 -29.1 27 -45.0	6700 -30.7 60 -42.8	250 -39.2 1.7 -52.1	5000 -31.5 45 -43.6	140 -40.6 3.0 -50.5	500 -37.4 4.5 -49.5

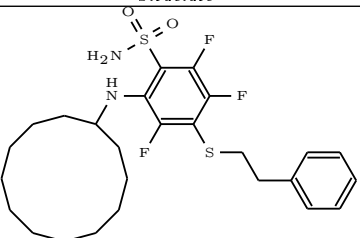
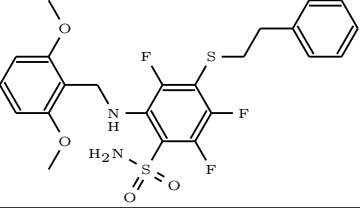
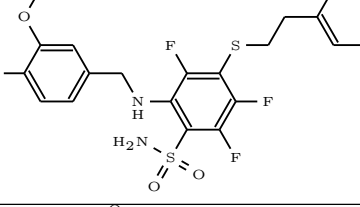
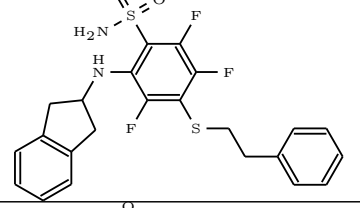
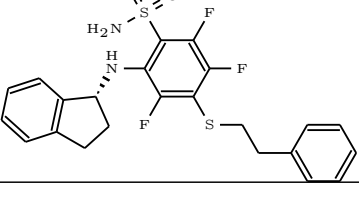
No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
335 VD12-36		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	610 -36.9 9.3 -47.7	230 -39.4 1.7 -52.1	ND ND ND ND	1500 -34.6 6.8 -48.5	1200 -35.2 13 -46.9	20 -45.7 0.16 -58.1	4000 -32.0 5.9 -48.8	290 -38.8 1.8 -51.9	10 -47.5 0.047 -61.3	720 -36.4 4.6 -49.5	140 -40.7 2.1 -51.5	83 -42.0 0.53 -55.1
336 VD12-35		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2200 -33.6 42 -43.8	5200 -31.4 48 -43.4	≥200 000 ≥-22.0 1000 -35.6	1200 -35.0 7.5 -48.2	14 000 -28.8 200 -39.8	2500 -33.2 26 -45.0	≥200 000 ≥-22.0 460 -33.9	56 000 -25.2 460 -37.6	7.1 -48.4 0.042 -61.6	8200 -30.2 66 -42.6	1000 -35.5 20 -45.7	500 -37.4 4.0 -49.8
337 VD12-38		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	12 000 -29.2 260 -39.1	3000 -32.7 32 -44.5	ND ND ND ND	40 000 -26.1 270 -39.0	10 000 -29.7 160 -40.4	67 -42.6 0.78 -54.0	3600 -32.3 7.6 -48.2	15 000 -28.7 130 -40.8	59 -42.9 0.39 -55.8	2500 -33.2 23 -45.4	380 -38.1 8.2 -48.0	330 -38.4 3.0 -50.6
338 VD12-29-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	10 000 -29.7 160 -40.3	2200 -33.5 17 -46.1	ND ND ND ND	100 000 -23.7 500 -37.4	20 000 -27.9 230 -39.4	3300 -32.5 29 -44.7	7700 -30.3 12 -47.0	21 000 -27.7 140 -40.6	65 -42.7 0.32 -56.3	10 000 -29.7 68 -42.6	450 -37.6 7.2 -48.3	330 -38.4 2.3 -51.3
339 VD12-67-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	130 000 -23.0 680 -36.6	29 000 -26.9 71 -42.4	ND ND ND ND	50 000 -25.5 78 -42.2	14 000 -28.8 52 -43.2	ND ND ND ND	≥200 000 ≥-22.0 500 -37.4	≥200 000 ≥-22.0 2100 -33.7	3500 -32.4 5.4 -49.1	≥200 000 ≥-22.0 2100 -33.7	14 000 -28.8 71 -42.4	10 000 -29.7 21 -45.5
340 VD12-69-1		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	67 -42.6 1.6 -52.2	200 -39.8 2.3 -51.2	ND ND ND ND	ND ND ND ND	4000 -32.0 70 -42.5	4.3 -49.6 0.057 -60.8	710 -36.5 1.7 -52.0	560 -37.1 5.6 -49.0	50 -43.3 0.37 -56.0	1000 -35.6 10 -47.4	140 -40.6 3.4 -50.3	63 -42.8 0.63 -54.6
341 VD12-09		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	24 000 -27.4 460 -37.6	1000 -35.6 9.1 -47.7	≥200 000 ≥-22.0 980 -35.7	1500 -34.5 8.9 -47.8	3300 -32.5 45 -43.6	100 -41.5 1.0 -53.4	5000 -31.5 9.3 -47.7	200 -39.7 1.6 -52.2	0.77 -54.1 0.0045 -67.4	240 -39.3 1.9 -51.8	98 -41.6 1.8 -51.9	140 -40.6 1.1 -53.1

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>342</b> VD12-19		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 390 -38.0	1700 -34.3 15 -46.4	ND ND ND ND	100 000 -23.7 600 -36.9	ND ND ND ND	50 -43.3 0.52 -55.1	33 000 -26.6 63 -42.7	3300 -32.5 27 -44.9	0.25 -57.0 0.0015 -70.2	330 -38.4 2.7 -50.9	11 -47.2 0.21 -57.4	50 -43.3 0.40 -55.7
<b>343</b> VD12-16		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 430 -37.8	20 000 -27.9 210 -39.7	ND ND ND ND	ND -26.6 ND -37.3	33 000 -35.0 520 -46.5	1200 -25.2 15 -41.0	58 000 -27.9 120 -40.0	20 000 -39.2 180 -52.1	250 -27.9 1.7 -40.0	20 000 -27.9 180 -40.0	20 000 -27.9 430 -37.8	100 -41.5 0.91 -53.7
<b>344</b> VD12-17		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	13 000 -28.9 260 -39.1	1300 -35.0 12 -47.1	ND ND ND ND	8300 -30.1 50 -43.3	670 -36.7 9.3 -47.7	50 -43.3 0.52 -55.1	11 000 -29.4 21 -45.5	750 -36.4 6.0 -48.8	110 -41.3 0.66 -54.5	4700 -31.6 38 -44.0	47 -43.5 0.89 -53.7	200 -39.8 1.6 -52.2
<b>345</b> VD12-15		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	8300 -30.1 180 -40.0	2800 -33.0 29 -44.7	ND ND ND ND	6700 -30.7 45 -43.6	10 000 -29.7 160 -40.3	330 -38.4 4.0 -49.8	3300 -32.5 7.3 -48.3	1700 -34.3 15 -46.4	7.4 -48.2 0.051 -61.1	1200 -35.0 12 -47.1	33 -44.4 0.73 -54.2	170 -40.2 1.5 -52.3
<b>346</b> VD12-18		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 390 -38.0	10 000 -29.7 93 -41.7	ND ND ND ND	33 000 -26.6 200 -39.8	13 000 -29.0 180 -40.0	2500 -33.2 26 -45.0	25 000 -27.3 48 -43.5	12 000 -29.3 95 -41.7	10 -47.5 0.060 -60.7	2000 -33.8 16 -46.2	100 -41.5 1.9 -51.8	200 -39.8 1.6 -52.2

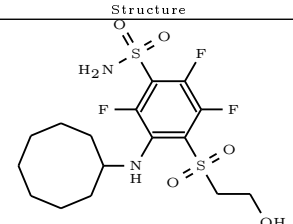
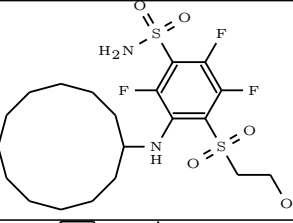
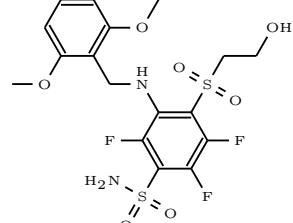
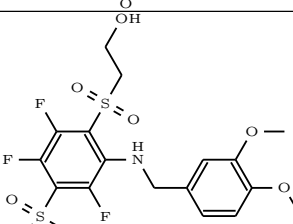
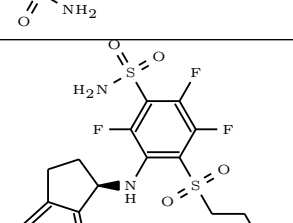


No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>347</b> VD12-11		$K_{d,obs}$ (nM)	$\geq 200\,000$	$\geq 200\,000$	ND	100 000	ND	$\geq 200\,000$	33 000	$\geq 200\,000$	50	6700	5600	670
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	$\geq -22.0$	ND	-23.7	ND	$\geq -22.0$	-26.6	$\geq -22.0$	-43.3	-30.7	-31.2	-36.7
		$K_{d,int}$ (nM)	19 000	8900	ND	570	ND	10 000	61	7700	0.28	52	100	5.2
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-28.1	-30.0	ND	-37.1	ND	-29.7	-42.8	-30.3	-56.6	-43.2	-41.5	-49.2
<b>348</b> VD12-08		$K_{d,obs}$ (nM)	$\geq 200\,000$	3300	ND	17 000	25 000	1400	20 000	1400	1.7	1000	670	350
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	-32.5	ND	-28.4	-27.3	-34.7	-27.9	-34.7	-52.1	-35.6	-36.7	-38.3
		$K_{d,int}$ (nM)	19 000	31	ND	99	350	15	38	12	0.010	8.1	13	2.9
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-28.0	-44.6	ND	-41.6	-38.3	-46.4	-44.0	-47.1	-65.3	-48.0	-46.9	-50.7
<b>349</b> VD12-14		$K_{d,obs}$ (nM)	100 000	10 000	ND	2200	ND	$\geq 200\,000$	100 000	1700	14	1400	770	170
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-23.7	-29.7	ND	-33.5	ND	$\geq -22.0$	-23.7	-34.3	-46.6	-34.7	-36.3	-40.2
		$K_{d,int}$ (nM)	61	2.9	ND	0.42	ND	330	6.0	0.43	0.0027	0.36	0.46	0.043
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.8	-50.6	ND	-55.7	ND	-38.5	-48.8	-55.6	-68.7	-56.0	-55.4	-61.5
<b>350</b> VD10-27		$K_{d,obs}$ (nM)	41 000	2000	ND	100 000	33 000	40	560	56	0.35	1000	20	620
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-26.0	-33.8	ND	-23.7	-26.6	-43.9	-37.1	-43.1	-56.1	-35.6	-45.7	-36.8
		$K_{d,int}$ (nM)	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>351</b> VD11-71		$K_{d,obs}$ (nM)	3300	500	ND	10 000	670	ND	3300	130	50	2900	67	43
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-32.5	-37.4	ND	-29.7	-36.7	ND	-32.5	-41.0	-43.3	-32.9	-42.6	-43.7
		$K_{d,int}$ (nM)	65	4.6	ND	60	9.3	ND	6.3	1.0	0.30	23	1.3	0.35
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.7	-49.5	ND	-42.9	-47.7	ND	-48.6	-53.4	-56.5	-45.3	-52.8	-56.1
<b>352</b> VD11-53-2		$K_{d,obs}$ (nM)	5000	2500	ND	ND	1000	5.0	3300	1700	8.2	2900	110	67
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-31.5	-33.2	ND	ND	-35.6	-49.3	-32.5	-34.3	-48.0	-32.9	-41.3	-42.6
		$K_{d,int}$ (nM)	97	23	ND	ND	14	0.052	6.3	13	0.049	23	2.1	0.54
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.6	-45.3	ND	ND	-46.6	-61.0	-48.6	-46.7	-61.2	-45.3	-51.5	-55.0

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>353</b> VD11-65		$K_{d,obs}$ (nM)	7100	2200	ND	$\geq 200\,000$	5000	50	$\geq 200\,000$	14\,000	17	1000	330	50
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-30.6	-33.5	ND	$\geq -22.0$	-31.5	-43.3	$\geq -22.0$	-28.8	-46.2	-35.6	-38.4	-43.3
		$K_{d,int}$ (nM)	140	21	ND	6000	70	0.52	1900	120	0.099	8.1	6.3	0.40
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.7	-45.6	ND	-31.0	-42.5	-55.1	-33.9	-41.2	-59.4	-48.0	-48.6	-55.7
<b>354</b> VD12-07		$K_{d,obs}$ (nM)	1700	3300	$\geq 200\,000$	2000	200	17	1600	4000	29	5000	40	500
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-34.3	-32.5	$\geq -22.0$	-33.8	-39.8	-46.2	-34.4	-32.0	-44.7	-31.5	-43.9	-37.4
		$K_{d,int}$ (nM)	32	31	1000	12	2.8	0.17	3.1	32	0.17	40	0.76	4.0
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-44.5	-44.6	-35.6	-47.0	-50.8	-57.9	-50.5	-44.4	-57.9	-43.9	-54.1	-49.8
<b>355</b> VD11-67		$K_{d,obs}$ (nM)	29\,000	5900	ND	170\,000	33\,000	$\geq 200\,000$	100\,000	$\geq 200\,000$	20\,000	100\,000	100\,000	11\,000
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-27.0	-31.0	ND	-22.4	-26.6	$\geq -22.0$	-23.7	$\geq -22.0$	-27.9	-23.7	-23.7	-29.4
		$K_{d,int}$ (nM)	550	55	ND	990	460	3200	190	8100	120	810	1900	90
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-37.1	-43.1	ND	-35.6	-37.6	-32.6	-39.9	-30.2	-41.1	-36.2	-33.9	-41.8
<b>356</b> VD11-62		$K_{d,obs}$ (nM)	11\,000	250	ND	2000	20\,000	100\,000	50\,000	170	3.8	500	500	ND
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-29.5	-39.2	ND	-33.8	-27.9	-23.7	-25.5	-40.2	-49.9	-37.4	-37.4	ND
		$K_{d,int}$ (nM)	210	2.3	ND	12	280	1000	95	1.3	0.023	4.0	9.5	ND
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-39.7	-51.2	ND	-47.0	-38.9	-35.5	-41.7	-52.6	-63.1	-49.8	-47.6	ND
<b>357</b> VD12-06		$K_{d,obs}$ (nM)	$\geq 200\,000$	1400	ND	ND	ND	170	14\,000	1000	11	1200	500	500
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	-34.7	ND	ND	ND	-40.2	-28.8	-35.6	-47.2	-35.0	-37.4	-37.4
		$K_{d,int}$ (nM)	19\,000	13	ND	ND	ND	1.7	27	8.1	0.066	10	9.5	4.0
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-28.0	-46.8	ND	ND	ND	-52.0	-44.9	-48.0	-60.4	-47.4	-47.6	-49.8
<b>358</b> VD11-59		$K_{d,obs}$ (nM)	$\geq 200\,000$	$\geq 200\,000$	ND	100\,000	ND	5000	$\geq 200\,000$	$\geq 200\,000$	6.8	4000	710	330
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	$\geq -22.0$	$\geq -22.0$	ND	-23.7	ND	-31.5	$\geq -22.0$	$\geq -22.0$	-48.5	-32.0	-36.5	-38.4
		$K_{d,int}$ (nM)	19\,000	9300	ND	600	ND	52	1900	8100	0.041	32	14	2.7
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-28.0	-29.9	ND	-36.9	ND	-43.2	-33.9	-30.2	-61.7	-44.4	-46.7	-50.9

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>359</b> PG7		$K_{d,obs}$ (nM) $\geq 200\,000$	$\geq 200\,000$	$\geq 200\,000$	$\geq 200\,000$	25 000	$\geq 200\,000$	$\geq 200\,000$	$\geq 200\,000$	7.8	$\geq 200\,000$	1700	4300
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $\geq -22.0$	$\geq -22.0$	$\geq -22.0$	$\geq -22.0$	-27.3	$\geq -22.0$	$\geq -22.0$	$\geq -22.0$	-48.1	$\geq -22.0$	-34.3	-31.8
		$K_{d,int}$ (nM) 19 000	9300	1000	6000	350	2100	1900	8100	0.046	8100	32	35
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -28.0	-29.9	-35.6	-31.0	-38.3	-33.7	-33.9	-30.2	-61.3	-30.2	-44.5	-44.2
<b>360</b> VD12-03		$K_{d,obs}$ (nM) 6700	$\geq 200\,000$	ND	ND	ND	$\geq 200\,000$	$\geq 200\,000$	$\geq 200\,000$	330	$\geq 200\,000$	3300	1800
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -30.7	$\geq -22.0$	ND	ND	ND	$\geq -22.0$	$\geq -22.0$	$\geq -22.0$	-38.4	$\geq -22.0$	-32.5	-34.1
		$K_{d,int}$ (nM) 130	9300	ND	ND	ND	10 000	1900	8100	2.0	8100	63	15
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -40.9	-29.9	ND	ND	ND	-29.6	-33.9	-30.2	-51.6	-30.2	-42.7	-46.5
<b>361</b> VD12-04		$K_{d,obs}$ (nM) 350	1800	ND	ND	910	ND	20 000	3100	52	10 000	16	400
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -38.3	-34.1	ND	ND	-35.8	ND	-27.9	-32.7	-43.2	-29.7	-46.2	-38.0
		$K_{d,int}$ (nM) 6.8	17	ND	ND	13	ND	38	26	0.31	81	0.31	3.2
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -48.5	-46.1	ND	ND	-46.9	ND	-44.0	-45.1	-56.4	-42.1	-56.4	-50.4
<b>362</b> VD11-64		$K_{d,obs}$ (nM) 5800	3300	ND	110 000	ND	250	6700	4000	3.3	1700	100	200
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) -31.1	-32.5	ND	-23.5	ND	-39.2	-30.7	-32.0	-50.3	-34.3	-41.5	-39.8
		$K_{d,int}$ (nM) 110	31	ND	660	ND	2.6	13	32	0.020	13	1.9	1.6
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -41.3	-44.6	ND	-36.7	ND	-50.9	-46.9	-44.4	-63.5	-46.7	-51.8	-52.2
<b>363</b> VD11-74		$K_{d,obs}$ (nM) $\geq 200\,000$	$\geq 200\,000$	ND	100 000	ND	ND	$\geq 200\,000$	$\geq 200\,000$	ND	$\geq 200\,000$	1000	170
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $\geq -22.0$	$\geq -22.0$	ND	-23.7	ND	ND	$\geq -22.0$	$\geq -22.0$	ND	$\geq -22.0$	-35.6	-40.2
		$K_{d,int}$ (nM) 19 000	9300	ND	600	ND	ND	1900	8100	ND	8100	19	1.3
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> ) -28.0	-29.9	ND	-36.9	ND	ND	-33.9	-30.2	ND	-30.2	-45.8	-52.6

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>364</b> VD11-75		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3500 -32.4 69 -42.5	$\geq 200\,000$ $\geq -22.0$ 9300 -29.9	ND ND ND ND	100 000 -23.7 600 -36.9	ND ND ND ND	$\geq 200\,000$ $\geq -22.0$ 2100 -33.7	$\geq 200\,000$ $\geq -22.0$ 1900 -33.9	$\geq 200\,000$ $\geq -22.0$ 8100 -30.2	31 -44.6 0.18 -57.8	$\geq 200\,000$ $\geq -22.0$ 8100 -30.2	330 -38.4 6.3 -48.6	500 -37.4 4.0 -49.8
<b>365</b> VD11-63		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\,000$ $\geq -22.0$ 19 000 -28.0	$\geq 200\,000$ $\geq -22.0$ 9300 -29.9	ND ND ND ND	$\geq 200\,000$ $\geq -22.0$ 6000 -31.0	ND ND ND ND	67 000 -24.8 700 -36.5	100 000 -23.7 190 -39.9	$\geq 200\,000$ $\geq -22.0$ 8100 -30.2	71 -42.4 0.42 -55.6	$\geq 200\,000$ $\geq -22.0$ 8100 -30.2	$\geq 200\,000$ $\geq -22.0$ 19 000 -28.0	2500 -33.2 20 -45.7
<b>366</b> VD12-57		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	67 000 -24.8 1300 -34.9	1100 -35.3 10 -47.4	ND ND ND ND	ND -26.6 ND -37.6	33 000 ND 460 ND	ND ND ND ND	6300 -30.9 12 -47.0	2500 -33.2 20 -45.7	0.39 -55.8 0.0023 -69.0	4000 -32.0 32 -44.4	50 -43.3 0.95 -53.5	ND ND ND ND
<b>367</b> AZ13-2-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	58 000 -25.2 3300 -32.5	2200 -33.5 61 -42.8	$\geq 200\,000$ $\geq -22.0$ 3000 -32.8	13 000 -29.1 220 -39.5	1700 -34.3 69 -42.5	1800 -34.1 57 -43.0	3900 -32.1 22 -45.5	500 -37.4 12 -47.0	0.40 -55.8 0.0071 -66.2	250 -39.2 6.0 -48.8	170 -40.2 9.4 -47.6	240 -39.3 5.7 -48.9
<b>368</b> VD10-39b		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	200 -39.8 23 -45.3	83 -42.0 4.6 -49.5	ND ND ND ND	90 -41.8 3.2 -50.4	330 -38.4 27 -44.9	3.3 -50.3 0.21 -57.5	130 -40.8 1.5 -52.3	130 -41.0 6.0 -48.8	0.63 -54.6 0.022 -63.2	25 -45.1 1.2 -52.9	14 -46.6 1.6 -52.2	13 -46.9 0.60 -54.7

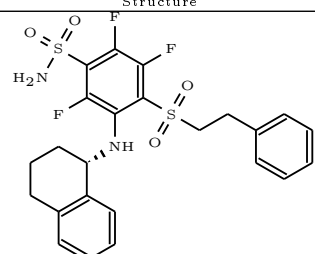
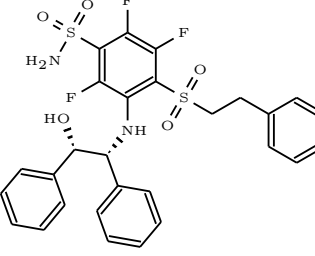
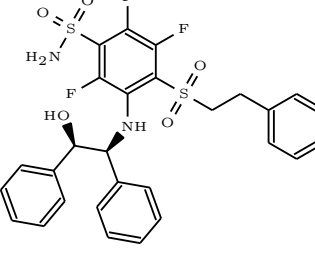
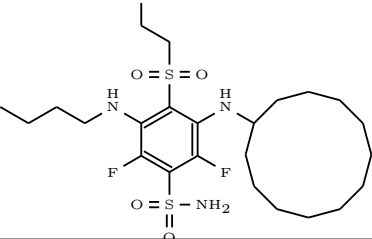
No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>369</b> VD11-4-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	830 -36.1 69 -42.5	56 -43.0 2.2 -51.4	34 000 -26.5 720 -36.4	61 -42.8 1.5 -52.3	3300 -32.5 200 -39.8	16 -46.3 0.70 -54.3	67 -42.6 0.54 -55.0	8.6 -47.9 0.30 -56.5	0.032 -62.3 0.000 80 -71.8	2.9 -50.6 0.10 -59.3	4.0 -49.8 0.33 -56.3	4.3 -49.6 0.15 -58.3
<b>370</b> VD12-30		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	520 -37.3 58 -43.0	42 -43.8 2.2 -51.4	ND ND ND ND	230 -39.4 7.7 -48.2	3400 -32.5 270 -39.0	200 -39.8 12 -47.0	200 -39.8 2.2 -51.4	71 -42.4 3.3 -50.4	52 -43.3 1.7 -52.0	5.0 -49.3 0.23 -57.2	0.91 -53.6 0.099 -59.4	17 -46.2 0.77 -54.1
<b>371</b> VD12-32		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	220 -39.5 27 -44.9	22 -45.4 1.3 -52.7	$\geq 200\ 000$ $\geq -22.0$ 6300 -30.9	140 -40.6 5.3 -49.1	1000 -35.6 88 -41.9	10 -47.5 0.66 -54.5	1000 -35.6 12 -47.0	40 -43.9 2.0 -51.6	0.67 -54.5 0.025 -62.9	67 -42.6 3.4 -50.3	25 -45.1 3.0 -50.6	25 -45.1 1.3 -52.8
<b>372</b> VD12-33		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	83 -42.0 9.2 -47.7	180 -40.1 9.3 -47.7	ND ND ND ND	400 -38.0 14 -46.7	67 -42.6 5.3 -49.1	33 -44.4 2.0 -51.6	500 -37.4 5.4 -49.1	14 -46.6 0.66 -54.5	2.5 -51.0 0.085 -59.8	83 -42.0 3.8 -49.9	4.3 -49.6 0.47 -55.4	500 -37.4 23 -45.3
<b>373</b> VD12-34		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 110 -41.2	17 -46.2 0.91 -53.6	ND ND ND ND	67 -42.6 2.3 -51.2	1600 -34.4 130 -40.8	8.3 -47.9 0.52 -55.1	100 -41.5 1.1 -53.1	5.0 -49.3 0.24 -57.1	0.11 -59.1 0.0039 -67.7	8.3 -47.9 0.40 -55.8	8.3 -47.9 0.94 -53.6	4.2 -49.7 0.20 -57.5

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
374 VD12-23		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1400 -34.7 160 -40.4	61 -42.8 3.2 -50.4	ND ND ND ND	200 -39.8 6.8 -48.5	1000 -35.6 79 -42.1	150 -40.4 9.1 -47.7	450 -37.6 4.9 -49.3	10 -47.5 0.46 -55.4	0.050 -61.1 0.0017 -69.9	13 -46.8 0.60 -54.7	10 -47.5 1.1 -53.2	6.5 -48.6 0.30 -56.5
375 VD12-25-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	22 000 -27.6 2400 -33.3	64 -42.7 3.3 -50.3	ND ND ND ND	ND ND ND ND	5000 -31.5 390 -38.0	10 -47.5 0.58 -54.8	370 -38.2 3.9 -49.9	34 -44.4 1.5 -52.3	ND ND ND ND	16 -46.3 0.71 -54.3	4.9 -49.3 0.52 -55.1	ND ND ND ND
376 VD11-26		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	75 -42.3 8.2 -48.0	5.9 -48.8 0.31 -56.4	ND ND ND ND	100 000 -23.7 3400 -32.5	500 -37.4 40 -43.9	6.7 -48.5 0.40 -55.8	100 -41.5 1.1 -53.2	8.3 -47.9 0.38 -55.9	7.6 -48.2 0.26 -56.9	290 -38.8 13 -46.8	1.2 -52.8 0.14 -58.6	5.0 -49.3 0.23 -57.2
377 VD11-25		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	670 -36.7 73 -42.3	1.7 -52.1 0.088 -59.7	ND ND ND ND	250 -39.2 8.3 -47.9	720 -36.5 57 -43.0	0.50 -55.2 0.030 -62.5	50 -43.3 0.54 -55.0	0.22 -57.3 0.010 -65.2	0.86 -53.8 0.029 -62.5	67 -42.6 3.1 -50.5	5.0 -49.3 0.54 -55.0	ND ND ND ND
378 VD11-28		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	53 -43.2 5.8 -48.9	6.7 -48.5 0.35 -56.1	ND ND ND ND	910 -35.9 31 -44.6	250 -39.2 20 -45.7	6.7 -48.5 0.40 -55.8	110 -41.3 1.2 -52.9	5.0 -49.3 0.23 -57.2	3.3 -50.3 0.11 -59.0	40 -43.9 1.8 -51.8	2.5 -51.0 0.27 -56.8	ND ND ND ND

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>379</b> VD11-54-2		910	17	ND	2500	500	5.0	330	4.0	3.3	33	6.7	14
		$K_{d,obs}$ (nM)											
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-35.8	-46.2	ND	-33.2	-37.4	-49.3	-38.4	-49.8	-50.3	-44.4	-48.5
		$K_{d,int}$ (nM)	100	0.88	ND	85	40	0.30	3.6	0.18	0.11	1.5	0.72
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.5	-53.7	ND	-42.0	-43.9	-56.5	-50.1	-57.8	-59.0	-52.3	-54.5
<b>380</b> VD11-15		100	1.2	ND	1200	500	4.0	40	2.5	5.6	150	5.0	4.1
		$K_{d,obs}$ (nM)											
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.5	-52.8	ND	-35.0	-37.4	-49.8	-43.9	-51.0	-49.0	-40.4	-49.3
		$K_{d,int}$ (nM)	11	0.066	ND	42	40	0.24	0.43	0.11	0.19	7.1	0.54
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.2	-60.4	ND	-43.8	-43.9	-57.1	-55.6	-59.0	-57.7	-48.4	-55.0
<b>381</b> VD11-43-2		410	13	ND	1000	2500	10	200	3.3	0.050	6.7	3.3	50
		$K_{d,obs}$ (nM)											
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-37.9	-46.9	ND	-35.6	-33.2	-47.5	-39.8	-50.3	-61.1	-48.5	-50.3
		$K_{d,int}$ (nM)	45	0.66	ND	34	200	0.59	2.2	0.15	0.0017	0.31	0.36
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.6	-54.5	ND	-44.3	-39.8	-54.8	-51.4	-58.2	-69.9	-56.5	-56.0
<b>382</b> VD12-39		2200	710	ND	13 000	6700	610	2500	29 000	0.083	65	1.2	33
		$K_{d,obs}$ (nM)											
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-33.5	-36.5	ND	-29.1	-30.7	-36.9	-33.2	-26.9	-59.8	-42.7	-52.9
		$K_{d,int}$ (nM)	250	37	ND	420	530	36	27	1300	0.0028	3.0	0.13
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-39.2	-44.1	ND	-37.8	-37.3	-44.2	-44.9	-34.9	-68.5	-50.6	-58.6
<b>383</b> VD12-41		100	22	≥200 000	1700	1000	4.0	220	670	ND	170	8.3	20
		$K_{d,obs}$ (nM)											
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-41.5	-45.4	≥-22.0	-34.3	-35.6	-49.8	-39.5	-36.7	ND	-40.2	-47.9
		$K_{d,int}$ (nM)	11	1.1	5600	55	78	0.23	2.4	30	ND	7.5	0.88
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.2	-53.1	-31.2	-43.1	-42.2	-57.2	-51.2	-44.6	ND	-48.2	-53.7

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>384</b> VD12-43		$K_{d,obs}$ (nM)	210	36	110 000	29 000	200	2.5	670	6.7	3.3	250	3.3	33
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-39.6	-44.2	-23.5	-27.0	-39.8	-51.0	-36.7	-48.5	-50.3	-39.2	-50.3	-44.4
		$K_{d,int}$ (nM)	23	1.9	3200	970	16	0.15	7.2	0.31	0.11	11	0.36	1.5
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.3	-51.8	-32.6	-35.7	-46.3	-58.3	-48.3	-56.5	-59.0	-47.1	-56.0	-52.3
<b>385</b> VD11-17		$K_{d,obs}$ (nM)	650	50	ND	1700	14 000	67	330	5.0	ND	17	5.6	50
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-36.7	-43.3	ND	-34.3	-28.8	-42.6	-38.4	-49.3	ND	-46.2	-49.0	-43.3
		$K_{d,int}$ (nM)	71	2.6	ND	56	1100	4.0	3.6	0.23	ND	0.77	0.60	2.3
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.4	-50.9	ND	-43.0	-35.3	-49.9	-50.1	-57.2	ND	-54.1	-54.7	-51.3
<b>386</b> VD11-16		$K_{d,obs}$ (nM)	940	35	ND	ND	830	2.0	2000	15	ND	67	1.0	14
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-35.8	-44.2	ND	ND	-36.1	-51.6	-33.8	-46.4	ND	-42.6	-53.4	-46.6
		$K_{d,int}$ (nM)	100	1.9	ND	ND	66	0.12	22	0.70	ND	3.1	0.11	0.66
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.4	-51.8	ND	ND	-42.6	-58.9	-45.5	-54.3	ND	-50.5	-59.1	-54.5
<b>387</b> VD12-42		$K_{d,obs}$ (nM)	50	2.9	ND	180	3300	1.2	330	1.0	6.7	41	2.0	2.0
		$\Delta G_{obs}$ (kJ mol <sup>-1</sup> )	-43.3	-50.7	ND	-40.0	-32.5	-52.8	-38.4	-53.4	-48.5	-43.9	-51.6	-51.6
		$K_{d,int}$ (nM)	5.5	0.15	ND	6.0	260	0.074	3.6	0.046	0.23	1.9	0.22	0.092
		$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-49.0	-58.3	ND	-48.8	-39.0	-60.1	-50.1	-61.3	-57.2	-51.8	-57.4	-59.6



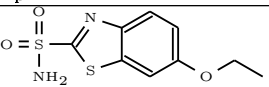
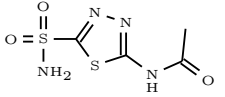
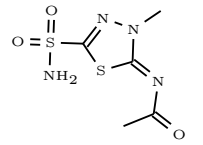
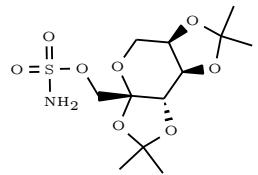
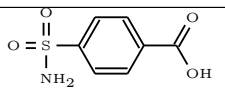
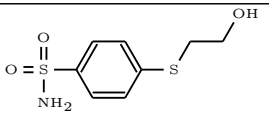
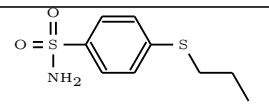
No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>388</b> VD12-40		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 110 -41.3	6.7 -48.5 0.35 -56.1	ND ND ND ND	1200 -35.0 42 -43.8	1000 -35.6 79 -42.1	6.7 -48.5 0.40 -55.8	130 -41.0 1.4 -52.6	13 -46.9 0.57 -54.8	ND ND ND ND	50 -43.3 2.3 -51.3	1.4 -52.5 0.15 -58.2	100 000 -23.7 4600 -31.7
<b>389</b> VD11-39		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	580 -37.0 64 -42.7	33 -44.4 1.8 -52.0	ND ND ND ND	300 -38.7 10 -47.4	2000 -33.8 160 -40.4	20 -45.7 1.2 -53.0	1000 -35.6 11 -47.3	10 -47.5 0.46 -55.4	50 -43.3 1.7 -52.1	250 -39.2 11 -47.1	5.6 -49.0 0.60 -54.7	100 -41.5 4.6 -49.5
<b>390</b> VD11-33		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1400 -34.8 150 -40.5	91 -41.8 4.8 -49.4	ND ND ND ND	1400 -34.7 48 -43.4	3300 -32.5 260 -39.0	140 -40.6 8.5 -47.9	290 -38.8 3.1 -50.5	40 -43.9 1.8 -51.8	20 -45.7 0.68 -54.4	400 -38.0 18 -45.9	6.7 -48.5 0.72 -54.3	98 -41.6 4.5 -49.5
<b>391</b> VD12-55		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	17 000 -28.3 ND ND	960 -35.7 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	17 000 -28.4 ND ND	33 000 -26.6 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	10 000 -29.7 ND ND	$\geq 200\ 000$ $\geq -22.0$ ND ND	0.26 -56.9 ND ND	120 -41.1 ND ND	260 -39.1 ND ND	1200 -35.0 ND ND

No. Cpd	Structure		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
392 VD12-33-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	2000 -33.8 ND ND	670 -36.7 ND ND	ND ND ND ND	2900 -32.8 ND ND	2500 -33.2 ND ND	330 -38.4 ND ND	17 000 -28.4 ND ND	440 -37.7 ND ND	43 -43.7 ND ND	1000 -35.6 ND ND	230 -39.4 ND ND	ND ND ND ND
393 VD12-65		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.8 ND ND	≥200 000 ≥-22.0 ND ND	ND ND ND ND	100 000 -23.7 ND ND	33 000 -26.6 ND ND	≥200 000 ≥-22.0 ND ND	5600 -31.2 ND ND	≥200 000 ≥-22.0 ND ND	1.8 -51.9 ND ND	500 -37.4 ND ND	330 -38.4 ND ND	2000 -33.8 ND ND
394 VD11-57		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	ND ND ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	330 -38.4 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND	≥200 000 ≥-22.0 ND ND
<b>Brominated compounds</b>														
395 LJ14-2		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	1000 -35.6 ND ND	620 -36.8 ND ND	≥200 000 ≥-22.0 ND ND	1300 -34.9 ND ND	3400 -32.4 ND ND	220 -39.5 ND ND	5000 -31.5 ND ND	1500 -34.5 ND ND	740 -36.4 ND ND	2500 -33.2 ND ND	240 -39.3 ND ND	83 -42.0 ND ND
396 LJ14-3		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	18 000 -28.1 84 -42.0	420 -37.9 0.92 -53.6	14 000 -28.8 17 -46.2	1200 -35.2 1.7 -52.1	27 000 -27.1 90 -41.8	ND ND ND ND	7700 -30.3 3.5 -50.2	130 -41.0 0.24 -57.1	620 -36.8 0.89 -53.7	620 -36.8 1.2 -52.9	290 -38.8 1.3 -52.7	510 -37.3 0.98 -53.5

No. Cpd	Structure	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>397</b> LJ14-4		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	20 000 -27.9 ND ND	91 -41.8 ND ND	$\geq 200\,000$ $\geq -22.0$ ND ND	140 -40.6 ND ND	3700 -32.2 ND ND	33 -44.4 ND ND	290 -38.8 ND ND	56 -43.1 ND ND	120 -41.2 ND ND	330 -38.4 ND ND	63 -42.8 ND ND	40 -43.9 ND ND
<b>398</b> LJ14-5		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	$\geq 200\,000$ $\geq -22.0$ 1800 -34.0	100 -41.5 0.44 -55.5	17 000 -28.4 40 -43.9	110 -41.3 0.31 -56.4	5900 -31.0 39 -44.0	250 -39.2 1.2 -52.9	1200 -35.2 1.1 -53.3	17 -46.2 0.064 -60.5	150 -40.4 0.43 -55.6	130 -40.8 0.51 -55.1	530 -37.3 4.7 -49.4	77 -42.2 0.29 -56.6
<b>399</b> LJ14-6		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	110 000 -23.5 1300 -35.0	25 -45.1 0.14 -58.5	13 000 -29.1 37 -44.1	50 -43.3 0.18 -57.9	4000 -32.0 33 -44.4	18 -45.9 0.11 -59.0	290 -38.8 0.32 -56.3	6.7 -48.5 0.032 -62.3	29 -44.8 0.10 -59.3	43 -43.7 0.21 -57.4	370 -38.2 4.2 -49.7	21 -45.6 0.10 -59.3
<b>400</b> LJ14-7		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	3100 -32.7 29 -44.8	50 -43.3 0.22 -57.3	22 000 -27.6 53 -43.2	ND ND ND ND	3400 -32.4 23 -45.4	500 -37.4 2.5 -51.1	1700 -34.3 1.5 -52.4	13 -46.7 0.051 -61.1	13 -46.9 0.035 -62.0	2.0 -51.6 0.0077 -66.0	100 -41.5 0.90 -53.7	13 -46.9 0.048 -61.2
<b>401</b> LJ14-10		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	14 000 -28.9 120 -41.0	40 -43.9 0.18 -57.9	12 000 -29.3 28 -44.8	ND ND ND ND	2500 -33.2 16 -46.2	330 -38.4 1.7 -52.1	1300 -34.9 1.2 -52.9	18 -45.9 0.070 -60.3	17 -46.2 0.047 -61.3	36 -44.2 0.14 -58.5	130 -41.0 1.1 -53.1	14 -46.6 0.055 -60.9
<b>402</b> LJ14-9		$K_{d,obs}$ (nM) $\Delta G_{obs}$ (kJ mol <sup>-1</sup> ) $K_{d,int}$ (nM) $\Delta G_{int}$ (kJ mol <sup>-1</sup> )	830 -36.1 6.1 -48.8	10 -47.5 0.035 -62.1	6700 -30.7 13 -46.9	3.5 -50.2 0.0077 -65.9	3300 -32.5 17 -46.0	29 -44.8 0.11 -59.0	830 -36.1 0.60 -54.7	2.9 -50.7 0.0087 -65.6	2.5 -51.0 0.0056 -66.8	0.80 -54.0 0.0024 -68.9	130 -41.0 0.90 -53.7	4.0 -49.8 0.012 -64.8

## 1.2 Table 2

Table 2: Intrinsic thermodynamic parameters of compound binding to CAs at pH7.0 and 37°C

No. Cpd	Structure	Intrinsic thermodynamic binding parameters														
		CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV			
<b>Non-halogenated compounds</b>																
1		$pK_{a,SA}$	7.82	$K_{d,int}$ (nM)	2.0	0.073	160	3.1	2.3	0.57	0.40	0.031	0.071	3.6	2.3	0.51
EZA		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.4	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-51.6	-60.2	-40.3	-50.6	-51.3	-54.9	-55.8	-62.4	-60.3	-50.1	-51.3	-55.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.9	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-53.6	-74.9	ND	-48.0	ND	-58.3	-55.2	-56.1	-58.2	-51.9	-50.8	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	2.0	14.7	ND	-2.6	ND	3.4	-0.6	-6.3	-2.1	1.7	-0.5	ND
2		$pK_{a,SA}$	7.03	$K_{d,int}$ (nM)	1100	9.8	4600	12	270	34	9.8	2.4	2.9	24	35	12
AZM		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-41.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-35.5	-47.5	-31.7	-47.0	-39.0	-44.3	-47.6	-51.2	-50.7	-45.2	-44.3	-47.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-18.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-50.3	-51.5	ND	-47.1	ND	ND	-35.5	-36.4	-56.1	-47.9	-51.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.9	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	14.8	4.0	ND	0.0	ND	ND	-12.0	-14.8	5.5	2.7	7.3	ND
3		$pK_{a,SA}$	6.86	$K_{d,int}$ (nM)	110	27	5600	41	ND	19	44	11	6.0	110	110	25
MZM		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-40.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.4	-45.0	-31.2	-43.8	ND	-45.8	-43.7	-47.2	-48.8	-41.3	-41.4	-45.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-20.5	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-47.6	-45.7	ND	ND	ND	ND	ND	ND	ND	ND	-37.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.2	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	6.3	0.8	ND	ND	ND	ND	ND	ND	ND	ND	-3.8	ND
4		$pK_{a,SA}$	8.50	$K_{d,int}$ (nM)	970	1.4	1500	0.58	20 000	0.038	35	0.30	0.30	0.97	6.8	0.24
TPM		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-50.5	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-35.7	-52.5	-34.6	-54.8	-27.8	-61.9	-44.3	-56.6	-56.6	-53.5	-48.5	-57.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	-25.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	-23.3	ND
5		$pK_{a,SA}$	9.24	$K_{d,int}$ (nM)	61	10	270	5.4	12	57	5.8	8.9	3.0	7.4	30	8.9
CARBS		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-54.9	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.8	-47.5	-39.0	-49.1	-47.1	-43.0	-48.9	-47.8	-50.6	-48.3	-44.7	-47.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-17.1	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-28.7	-32.1	ND	ND	ND	ND	ND	ND	ND	ND	-33.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	37.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-14.2	-15.4	ND	ND	ND	ND	ND	ND	ND	ND	-11.3	ND
10		$pK_{a,SA}$	9.96	$K_{d,int}$ (nM)	0.11	0.070	ND	1.2	4.2	5.5	0.50	0.086	0.26	1.2	1.4	0.11
VD11-31		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-59.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.1	-60.3	ND	-52.9	-49.7	-49.1	-55.2	-59.8	-56.9	-52.9	-52.5	-59.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-38.9	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-55.6	-56.5	ND	ND	ND	ND	ND	-43.2	ND	-41.1	-39.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.2	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-3.5	-3.8	ND	ND	ND	ND	ND	-16.5	ND	-11.8	-13.0	ND
11		$pK_{a,SA}$	10.2	$K_{d,int}$ (nM)	0.0029	0.0070	ND	0.30	1.5	0.021	0.048	0.0098	0.018	0.081	0.16	0.0063
VD12-10		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-60.6	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.5	-66.2	ND	-56.5	-52.3	-63.4	-61.3	-65.4	-63.8	-59.9	-58.1	-66.5
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-39.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-62.7	-69.0	ND	ND	ND	ND	ND	-45.0	ND	-56.4	-47.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.3	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-5.8	2.8	ND	ND	ND	ND	ND	-20.3	ND	-3.5	-10.6	ND

No. Cpd	Structure				CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
12 VD11-36		$pK_{a,SA}$	10.1	$K_{d,int}$ (nM)	0.0032	0.0039	36	ND	0.65	0.0054	0.077	0.0049	0.017	0.063	0.034	0.0055
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-60.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.3	-67.8	-44.2	ND	-54.5	-66.9	-60.1	-67.2	-64.0	-60.6	-62.1	-66.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-40.2	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-57.5	-58.4	ND	ND	ND	ND	ND	-45.7	ND	-52.0	-55.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.9	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-10.7	-9.4	ND	ND	ND	ND	ND	-21.4	ND	-8.6	-6.7	ND
44 JS45		$pK_{a,SA}$	10.1	$K_{d,int}$ (nM)	0.41	0.032	1.9	1.1	ND	1.3	0.90	0.041	0.015	0.51	0.0014	0.077
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-60.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-55.7	-62.3	-51.8	-53.1	ND	-52.7	-53.7	-61.7	-64.3	-55.2	-70.3	-60.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-21.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-35.0	-49.1	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	39.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-20.7	-13.3	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
53 E63		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.090	0.022	ND	0.41	3.8	7.9	1.8	0.085	ND	1.5	0.10	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.6	-63.3	ND	-55.8	-50.0	-48.1	-51.9	-59.8	ND	-52.3	-59.3	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-51.6	-60.6	ND	ND	ND	ND	ND	-60.0	ND	-28.4	-61.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-8.1	-2.6	ND	ND	ND	ND	ND	0.2	ND	-24.0	2.4	ND
54 E66		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.054	0.15	ND	0.23	1.8	2.0	0.45	0.38	ND	0.14	0.23	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-61.0	-58.4	ND	-57.2	-52.0	-51.7	-55.5	-55.9	ND	-58.5	-57.3	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-60.1	-35.5	ND	ND	ND	ND	ND	-33.6	ND	-28.1	-43.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-0.9	-22.9	ND	ND	ND	ND	ND	-22.3	ND	-30.4	-13.4	ND
55 E67		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.0063	0.12	ND	0.44	4.1	4.0	1.8	0.074	0.036	0.26	0.018	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-66.5	-59.0	ND	-55.6	-49.8	-49.9	-51.9	-60.1	-62.0	-56.9	-63.9	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-61.5	-34.7	ND	ND	ND	ND	ND	-37.2	ND	-23.5	-48.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-5.0	-24.3	ND	ND	ND	ND	ND	-23.0	ND	-33.4	-15.7	ND
56 E61		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.080	0.022	ND	0.23	4.1	12	1.8	0.10	ND	2.2	0.082	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.9	-63.3	ND	-57.2	-49.8	-46.9	-51.9	-59.3	ND	-51.4	-59.9	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-52.6	-41.8	ND	ND	ND	ND	ND	-50.3	ND	-27.3	-58.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-7.4	-21.5	ND	ND	ND	ND	ND	-9.0	ND	-24.1	-1.0	ND
57 E59		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.24	0.12	ND	0.43	1.3	5.0	1.3	0.26	ND	0.85	1.3	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.1	-59.0	ND	-55.6	-52.7	-49.3	-52.7	-57.0	ND	-53.9	-52.8	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-47.4	-40.2	ND	ND	ND	ND	ND	-64.1	ND	-24.6	-48.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-9.7	-18.7	ND	ND	ND	ND	ND	7.1	ND	-29.2	-4.3	ND
58 E60		$pK_{a,SA}$	9.40	$K_{d,int}$ (nM)	0.12	0.039	ND	0.33	2.9	7.9	0.45	0.22	ND	1.1	0.030	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-55.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-58.9	-61.8	ND	-56.3	-50.7	-48.1	-55.5	-57.4	ND	-53.2	-62.5	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-47.2	-38.0	ND	ND	ND	ND	ND	-38.3	ND	ND	-48.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	26.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-11.6	-23.8	ND	ND	ND	ND	ND	-19.1	ND	ND	-13.9	ND



No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
101		9.40	$K_{d,int}$ (nM)	3.1	2.2	ND	4.0	13	26	4.0	6.1	ND	5.7	5.5	ND
E11-19		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-50.6	-51.4	ND	-49.8	-46.8	-45.1	-49.9	-48.8	ND	-49.0	-49.0	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-48.4	-29.5	ND	ND	ND	ND	ND	-28.5	ND	-25.4	-38.0	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-2.2	-22.0	ND	ND	ND	ND	ND	-20.3	ND	-23.5	-11.0	ND
103		9.40	$K_{d,int}$ (nM)	0.37	0.88	ND	23	26	33	16	0.77	ND	1.9	0.60	ND
E11-27		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-56.0	-53.8	ND	-45.4	-45.0	-44.4	-46.2	-54.1	ND	-51.8	-54.8	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-50.3	-28.8	ND	ND	ND	ND	ND	-14.4	ND	-26.2	-50.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-5.7	-25.0	ND	ND	ND	ND	ND	-39.8	ND	-25.6	-3.9	ND
105		9.40	$K_{d,int}$ (nM)	8.2	2.0	ND	7.5	2.6	3.3	1.2	19	ND	10	5.1	ND
E11-21		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-48.0	-51.7	ND	-48.2	-50.9	-50.4	-53.0	-45.8	ND	-47.4	-49.2	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-50.2	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	2.1	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
<b>Chlorinated compounds</b>															
141		8.90	$K_{d,int}$ (nM)	0.12	0.061	ND	3.2	3.0	ND	2.8	0.024	0.70	4.0	0.19	ND
E11-8		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-59.0	-60.6	ND	-50.4	-50.6	ND	-50.8	-63.1	-54.4	-49.9	-57.7	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-47.2	-47.6	ND	ND	ND	ND	ND	-35.8	ND	-32.0	-57.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-11.8	-13.1	ND	ND	ND	ND	ND	-27.3	ND	-17.9	0.1	ND
144		8.90	$K_{d,int}$ (nM)	0.077	0.047	ND	2.2	3.3	9.6	5.7	0.048	ND	2.1	0.024	ND
E11-12		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.1	-61.4	ND	-51.4	-50.4	-47.6	-49.0	-61.3	ND	-51.5	-63.1	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-36.0	ND	ND	ND	ND	ND	-24.4	ND	ND	-50.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-25.4	ND	ND	ND	ND	ND	-36.8	ND	ND	-12.4	ND
145		8.90	$K_{d,int}$ (nM)	0.061	0.039	ND	1.7	2.8	11	3.8	0.080	ND	2.8	0.014	ND
E11-14		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.7	-61.8	ND	-52.1	-50.8	-47.2	-50.0	-59.9	ND	-50.8	-64.4	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-35.3	ND	ND	ND	ND	ND	-25.8	ND	-24.6	-56.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-26.4	ND	ND	ND	ND	ND	-34.1	ND	-26.2	-8.0	ND
146		8.90	$K_{d,int}$ (nM)	0.072	0.042	ND	1.4	2.8	10	3.8	0.053	ND	1.7	0.021	ND
E11-16		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.2	-61.6	ND	-52.5	-50.8	-47.4	-50.0	-61.0	ND	-52.0	-63.5	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-40.6	ND	ND	ND	ND	ND	ND	ND	ND	-39.5	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-19.6	ND	ND	ND	ND	ND	ND	ND	ND	-12.6	ND	ND

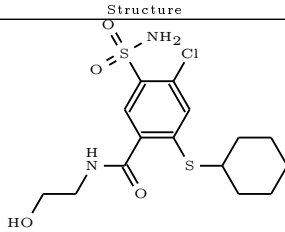
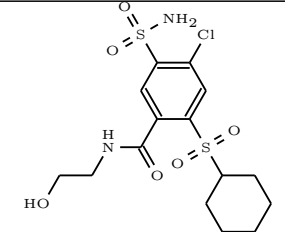
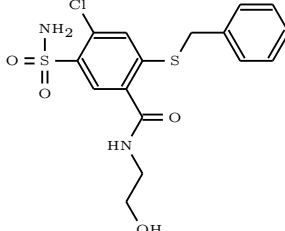
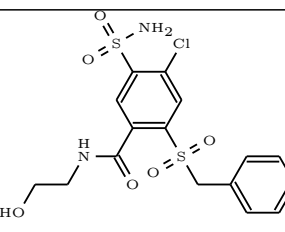
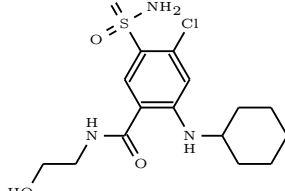
No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
147 E11-10		8.90	$K_{d,int}$ (nM)	0.058	0.092	ND	4.7	6.4	ND	3.2	0.060	ND	4.4	0.11	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.8	-59.6	ND	-49.4	-48.7	ND	-50.4	-60.7	ND	-49.6	-59.1	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-46.6	-41.1	ND	ND	ND	ND	ND	-24.6	ND	-36.4	-51.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-14.2	-18.5	ND	ND	ND	ND	ND	-36.1	ND	-13.3	-7.5	ND
148 E11-18		8.90	$K_{d,int}$ (nM)	0.077	0.15	ND	2.0	1.7	21	2.8	0.17	ND	1.6	0.38	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.1	-58.3	ND	-51.7	-52.1	-45.6	-50.8	-58.0	ND	-52.2	-56.0	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-35.6	-30.5	ND	ND	ND	ND	ND	-24.1	ND	-19.1	-41.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-24.5	-27.8	ND	ND	ND	ND	ND	-33.9	ND	-33.2	-14.5	ND
150 E11-26		8.90	$K_{d,int}$ (nM)	0.0041	0.15	ND	4.4	0.41	1.6	10	0.036	ND	1.2	0.013	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-67.6	-58.4	ND	-49.6	-55.7	-52.3	-47.4	-62.0	ND	-53.0	-64.6	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-44.2	-24.1	ND	ND	ND	ND	ND	-19.9	ND	-49.2	-44.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-23.5	-34.3	ND	ND	ND	ND	ND	-42.1	ND	-3.8	-20.2	ND
153 E11-20		8.90	$K_{d,int}$ (nM)	0.23	0.37	ND	2.5	1.7	3.1	2.1	0.48	ND	4.4	0.28	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.2	-56.0	ND	-51.0	-52.1	-50.5	-51.5	-55.3	ND	-49.6	-56.7	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-50.1	-26.1	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-7.1	-29.9	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
184 E38		8.90	$K_{d,int}$ (nM)	14	0.34	ND	ND	0.055	ND	3.1	0.60	ND	2.8	0.63	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-46.6	-56.2	ND	ND	-60.9	ND	-50.5	-54.8	ND	-50.8	-54.6	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-37.3	ND	ND	ND	ND	ND	ND	ND	ND	-40.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-18.9	ND	ND	ND	ND	ND	ND	ND	ND	-14.2	ND
187 E89		8.85	$K_{d,int}$ (nM)	55	2.1	ND	2.3	0.62	ND	0.70	3.8	ND	7.8	4.2	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.1	-51.6	ND	-51.3	-54.7	ND	-54.3	-50.0	ND	-48.2	-49.7	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-32.1	-32.9	ND	ND	ND	ND	ND	-48.9	ND	-26.6	-33.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-11.0	-18.7	ND	ND	ND	ND	ND	-1.1	ND	-21.5	-16.2	ND
188 E50		8.90	$K_{d,int}$ (nM)	21	0.79	ND	1.4	0.052	ND	0.75	1.6	ND	6.0	1.3	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.6	-54.1	ND	-52.5	-61.1	ND	-54.2	-52.2	ND	-48.8	-52.9	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-28.1	-33.9	ND	ND	ND	ND	ND	-32.0	ND	ND	-40.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-17.5	-20.1	ND	ND	ND	ND	ND	-20.2	ND	ND	-12.2	ND

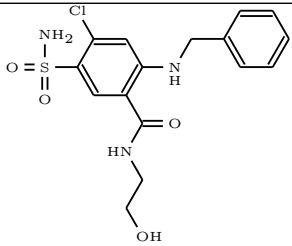
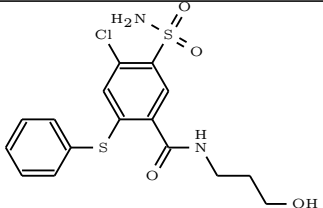
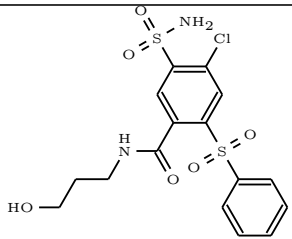
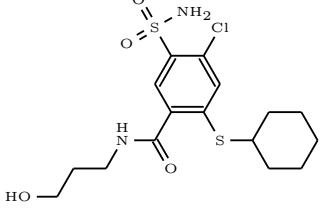
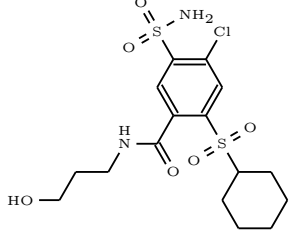




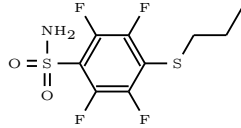
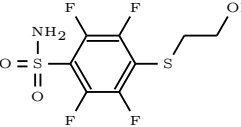
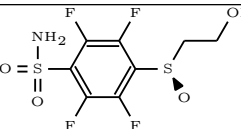
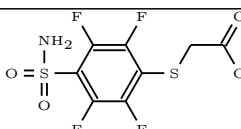
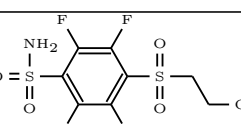
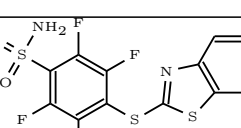
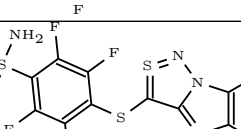
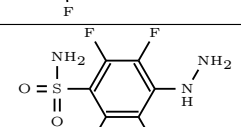
No. Cpd	Structure				CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
<b>207</b> E2		$pK_{a,SA}$	8.90	$K_{d,int}$ (nM)	130	8.6	600	2.3	0.0021	21	0.81	4.8	2.7	15	4.0	1.5
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.9	-47.9	-37.0	-51.3	-69.4	-45.6	-54.0	-49.4	-50.8	-46.4	-49.8	-52.5
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-28.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-15.0	ND	ND	ND	ND	ND	ND	ND	ND	-31.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	24.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-32.9	ND	ND	ND	ND	ND	ND	ND	ND	-18.8	ND
<b>221</b> EA3-1		$pK_{a,SA}$	8.80	$K_{d,int}$ (nM)	1400	0.58	31	1.8	52	3.1	0.89	0.060	0.74	0.75	7.9	0.40
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-34.7	-54.9	-44.6	-52.0	-43.3	-50.5	-53.8	-60.7	-54.2	-54.2	-48.1	-55.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-32.7	ND	ND	ND	ND	ND	ND	ND	ND	-47.9	-45.2
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.6	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-22.2	ND	ND	ND	ND	ND	ND	-26.2	ND	-6.3	-2.9
<b>222</b> EA4-1		$pK_{a,SA}$	8.80	$K_{d,int}$ (nM)	2900	0.069	94	0.032	87	6.0	1.4	0.060	0.22	1.0	8.9	0.38
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-32.9	-60.3	-41.7	-62.3	-41.9	-48.8	-52.5	-60.7	-57.3	-53.4	-47.8	-56.0
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-30.4	ND	ND	ND	ND	ND	-23.1	-25.8	-39.7	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-30.0	ND	ND	ND	ND	ND	-37.6	-31.6	-13.7	ND	ND
<b>223</b> EA5-1		$pK_{a,SA}$	8.75	$K_{d,int}$ (nM)	540	0.15	30	0.41	58	0.73	0.26	0.034	0.25	0.34	6.3	0.34
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-37.2	-58.3	-44.7	-55.7	-43.0	-54.3	-56.9	-62.2	-57.0	-56.2	-48.7	-56.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-35.2	ND	ND	ND	ND	ND	-22.7	ND	-33.2	-32.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.6	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-23.1	ND	ND	ND	ND	ND	-39.4	ND	-23.1	-16.2	ND
<b>224</b> EA8-1		$pK_{a,SA}$	8.75	$K_{d,int}$ (nM)	810	0.48	51	0.050	40	2.2	0.93	0.075	0.36	1.4	11	0.27
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-36.2	-55.3	-43.3	-61.2	-43.9	-51.4	-53.6	-60.1	-56.1	-52.7	-47.2	-56.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-33.3	ND	ND	ND	ND	ND	-29.3	ND	-39.8	-38.8	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.3	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-22.0	ND	ND	ND	ND	ND	-30.8	ND	-12.8	-8.3	ND
<b>225</b> EA12-1		$pK_{a,SA}$	8.87	$K_{d,int}$ (nM)	2500	0.84	150	1.1	18	15	1.7	0.34	1.1	0.21	8.1	0.45
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-33.3	-53.9	-40.6	-53.3	-46.0	-46.4	-52.0	-56.2	-53.2	-57.5	-48.1	-55.5
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-37.5	ND	ND	ND	ND	ND	-21.4	ND	-48.2	-59.0	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.4	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-16.4	ND	ND	ND	ND	ND	-34.8	ND	-9.3	11.0	ND

No. Cpd	Structure			CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
226 EA11-1		$pK_{a,SA}$	8.75	$K_{d,int}$ (nM)	1600	0.39	210	0.55	15	0.58	1.6	0.14	0.69	0.84	7.9	0.40
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-34.4	-55.9	-39.7	-55.0	-46.5	-54.8	-52.2	-58.6	-54.4	-53.9	-48.1	-55.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-30.0	ND	ND	ND	ND	ND	-26.3	ND	-40.8	-52.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.6	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-25.9	ND	ND	ND	ND	ND	-32.3	ND	-13.1	4.5	ND
228 EA7-1		$pK_{a,SA}$	8.75	$K_{d,int}$ (nM)	3200	1.5	420	1.7	2300	35	2.3	0.23	0.77	2.7	19	1.1
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-32.6	-52.3	-37.9	-52.1	-33.4	-44.3	-51.3	-57.3	-54.1	-50.9	-45.9	-53.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-18.9	ND	ND	ND	ND	ND	-23.8	ND	-34.2	-43.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-33.4	ND	ND	ND	ND	ND	-33.5	ND	-16.7	-2.0	ND
229 EA9-1		$pK_{a,SA}$	8.80	$K_{d,int}$ (nM)	1000	1.2	750	0.74	26	0.60	2.0	0.17	1.1	10	2.6	0.40
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-35.5	-53.1	-36.4	-54.2	-45.0	-54.8	-51.6	-58.0	-53.2	-47.5	-51.0	-55.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-28.3	ND	ND	ND	ND	ND	-8.9	ND	-27.1	-48.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.6	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-24.7	ND	ND	ND	ND	ND	-49.1	ND	-20.4	-2.3	ND
230 EA10-1		$pK_{a,SA}$	8.80	$K_{d,int}$ (nM)	360	0.14	7.5	0.099	6.9	0.060	0.20	0.030	0.40	0.75	4.7	0.080
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-38.3	-58.5	-48.2	-59.4	-48.4	-60.7	-57.6	-62.5	-55.8	-54.2	-49.4	-59.9
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-27.6	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-27.4	ND	ND	ND	ND	ND	-26.1	ND	-39.5	-42.8	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	24.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-31.1	ND	ND	ND	ND	ND	-36.4	ND	-14.7	-6.6	ND
246 EA3-2		$pK_{a,SA}$	8.98	$K_{d,int}$ (nM)	96	0.14	38	0.0042	38	1.7	1.3	0.045	0.012	0.025	0.94	0.012
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-53.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.7	-58.4	-44.0	-67.5	-44.0	-52.0	-52.7	-61.5	-64.9	-62.9	-53.6	-64.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-38.6	ND	ND	ND	ND	ND	-28.7	ND	-62.4	-40.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-19.8	ND	ND	ND	ND	ND	-32.8	ND	-0.6	-12.9	ND
247 EA3-2o		$pK_{a,SA}$	8.25	$K_{d,int}$ (nM)	99	0.12	110	ND	35	0.44	4.4	0.026	0.046	0.11	0.81	0.062
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-49.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.6	-59.0	-41.4	ND	-44.2	-55.5	-49.6	-62.9	-61.4	-59.0	-54.0	-60.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-30.2	ND	ND	ND	ND	ND	-31.0	ND	-52.1	-38.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.2	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-28.7	ND	ND	ND	ND	ND	-31.9	ND	-6.9	-15.4	ND

No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
248 EA3-3		9.00	$K_{d,int}$ (nM)	9.2	0.044	30	0.028	3.9	0.38	1.1	0.0096	0.0035	0.0077	0.26	0.0042
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.7	-61.5	-44.7	-62.6	-49.9	-55.9	-53.1	-65.4	-68.0	-66.0	-56.9	-67.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-32.9	ND	ND	ND	ND	ND	-21.8	ND	-52.5	-40.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-28.6	ND	ND	ND	ND	ND	-43.7	ND	-13.5	-16.8	ND
249 EA3-3o		8.22	$K_{d,int}$ (nM)	75	0.084	340	0.54	13	0.28	6.5	0.088	0.051	0.44	1.3	0.040
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.3	-59.8	-38.4	-55.0	-46.9	-56.7	-48.6	-59.7	-61.1	-55.6	-52.8	-61.7
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-25.1	ND	ND	ND	ND	ND	-38.1	ND	-41.9	-37.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-34.7	ND	ND	ND	ND	ND	-21.6	ND	-13.7	-15.1	ND
250 EA3-4		9.15	$K_{d,int}$ (nM)	14	0.040	84	0.067	2.3	0.54	1.0	0.0091	0.029	0.027	0.58	0.034
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-46.7	-61.7	-42.0	-60.4	-51.2	-55.0	-53.4	-65.6	-62.5	-62.7	-54.8	-62.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-33.8	ND	-60.4	-41.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-31.8	ND	-2.4	-13.2	ND
251 EA3-4o		8.20	$K_{d,int}$ (nM)	340	0.94	200	4.2	28	2.3	13	0.21	0.77	1.9	6.7	0.46
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-38.4	-53.6	-39.8	-49.7	-44.8	-51.3	-46.9	-57.5	-54.1	-51.8	-48.5	-55.4
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-24.2	ND	-31.2	-35.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-33.3	ND	-20.6	-13.4	ND
252 EA3-7		9.70	$K_{d,int}$ (nM)	26	0.37	240	ND	66	50	6.0	2.6	0.011	ND	1.2	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.0	-56.0	-39.3	ND	-42.6	-43.4	-48.8	-51.0	-65.0	ND	-53.0	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-19.4	-33.0	-53.1	-44.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-31.6	-32.0	ND	-8.1	ND

No. Cpd	Structure			CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>253</b> EA3-8		$pK_{a,SA}$	10.2	$K_{d,int}$ (nM)	3.7	0.021	30	ND	ND	0.63	0.38	0.055	0.0072	0.041	0.23	0.0049
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-60.6	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-50.1	-63.3	-44.6	ND	ND	-54.6	-55.9	-60.9	-66.2	-61.7	-57.2	-67.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-38.1	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-39.7	ND	-53.5	-49.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	-21.3	ND	-8.2	-7.5	ND
<b>264</b> EA4-2		$pK_{a,SA}$	8.95	$K_{d,int}$ (nM)	69	0.025	89	0.0053	34	0.69	0.84	0.0054	0.0063	0.0036	1.8	0.024
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-53.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.5	-63.0	-41.9	-67.0	-44.4	-54.4	-53.9	-66.9	-66.5	-68.0	-51.9	-63.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-33.7	ND	ND	ND	ND	ND	-32.4	ND	-52.1	-42.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-29.3	ND	ND	ND	ND	ND	-34.5	ND	-15.9	-9.8	ND
<b>265</b> EA4-2o		$pK_{a,SA}$	8.25	$K_{d,int}$ (nM)	70	0.079	210	0.42	200	0.50	6.9	0.0069	0.023	0.064	3.2	0.082
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-49.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.5	-60.0	-39.6	-55.7	-39.8	-55.2	-48.5	-66.3	-63.1	-60.5	-50.4	-59.9
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-28.2	ND	ND	ND	ND	ND	-22.9	ND	-25.8	-38.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	24.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-31.8	ND	ND	ND	ND	ND	-43.4	ND	-34.7	-11.7	ND
<b>266</b> EA4-3		$pK_{a,SA}$	8.85	$K_{d,int}$ (nM)	16	0.023	84	0.13	4.0	0.20	2.1	0.0036	0.0028	0.0054	0.84	0.011
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.5	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-46.3	-63.2	-42.0	-58.7	-49.8	-57.6	-51.5	-68.0	-68.6	-66.9	-53.9	-65.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-30.1	ND	ND	ND	ND	ND	-25.3	ND	-52.4	-44.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-33.1	ND	ND	ND	ND	ND	-42.7	ND	-14.5	-8.9	ND
<b>267</b> EA4-3o		$pK_{a,SA}$	8.30	$K_{d,int}$ (nM)	44	0.022	380	ND	45	0.27	5.4	0.026	0.0091	0.15	2.2	0.092
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-49.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.7	-63.3	-38.1	ND	-43.6	-56.9	-49.1	-62.8	-65.6	-58.3	-51.4	-59.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-20.5	ND	ND	ND	ND	ND	-15.4	ND	-29.6	-34.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	25.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-42.7	ND	ND	ND	ND	ND	-47.4	ND	-28.7	-16.8	ND

No. Cpd	Structure			CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
268 EA4-7		$pK_{a,SA}$	9.80	$K_{d,int}$ (nM)	49	0.13	60	ND	170	20	3.6	0.87	0.0038	0.013	ND	0.047
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-58.2	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.4	-58.6	-42.9	ND	-40.2	-45.7	-50.1	-53.8	-67.8	-64.7	ND	-61.3
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-39.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-23.9	ND	ND	ND	ND	ND	-16.8	ND	-50.4	-48.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	18.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-34.7	ND	ND	ND	ND	ND	-37.0	ND	-14.2	ND	ND
269 EA4-8		$pK_{a,SA}$	10.2	$K_{d,int}$ (nM)	15	0.0056	7.6	ND	20	2.4	0.72	0.016	0.0056	0.030	0.64	0.012
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-60.6	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-46.5	-66.8	-48.2	ND	-45.7	-51.2	-54.3	-64.1	-66.8	-62.4	-54.6	-64.9
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-36.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-39.3	ND	ND	ND	ND	ND	-28.0	ND	-47.1	-42.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-27.5	ND	ND	ND	ND	ND	-36.0	ND	-15.3	-12.2	ND
283 EA4-2c		$pK_{a,SA}$	9.03	$K_{d,int}$ (nM)	86	0.10	170	0.0076	14	0.46	1.2	0.028	0.013	0.036	2.8	0.022
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-53.6	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.0	-59.3	-40.2	-66.0	-46.7	-55.4	-53.0	-62.7	-64.6	-62.0	-50.8	-63.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-28.5	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-25.1	ND	ND	ND	ND	ND	-17.7	-24.8	-38.5	-35.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	25.1	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-34.3	ND	ND	ND	ND	ND	-45.0	-39.8	-23.5	-15.6	ND
<b>Fluorinated compounds</b>																
303 TFMSA		$pK_{a,SA}$	6.02	$K_{d,int}$ (nM)	51	8.4	220	17	24	ND	1.2	2.9	11	38	33	15
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-35.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-43.3	-47.9	-39.6	-46.2	-45.3	ND	-53.0	-50.7	-47.2	-44.0	-44.4	-46.5
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-16.7	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-46.5	-36.7	ND	-24.7	ND	ND	ND	-25.5	-31.1	-36.1	-42.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	3.2	-11.3	ND	-21.5	ND	ND	ND	-25.2	-16.1	-7.9	-2.2	ND
304 VD12-22		$pK_{a,SA}$	8.21	$K_{d,int}$ (nM)	0.22	0.73	400	9.2	11	0.053	3.5	0.25	2.5	7.5	1.1	1.2
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-48.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.3	-54.2	-38.0	-47.7	-47.2	-61.0	-50.2	-57.0	-51.1	-48.2	-53.3	-52.9
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-25.9	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-72.5	-42.4	ND	ND	ND	ND	ND	-26.5	-33.5	-31.7	-42.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	15.2	-11.8	ND	ND	ND	ND	ND	-30.5	-17.6	-16.6	-10.8	ND
305 VD10-9		$pK_{a,SA}$	8.12	$K_{d,int}$ (nM)	0.22	1.4	ND	15	21	1.3	2.7	1.5	3.0	21	4.9	0.96
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-48.2	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.4	-52.5	ND	-46.5	-45.6	-52.7	-50.8	-52.3	-50.6	-45.6	-49.3	-53.5
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-69.4	-40.7	ND	ND	ND	ND	ND	-24.7	ND	-32.9	-38.3	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	12.1	-11.8	ND	ND	ND	ND	ND	-27.6	ND	-12.7	-11.1	ND

No. Cpd	Structure			CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
306 VD12-05		$pK_{a,SA}$	8.15	$K_{d,int}$ (nM)	0.0035	0.065	60	2.0	8.8	0.0017	0.86	0.028	0.10	0.93	0.14	0.093
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-48.4	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.0	-60.5	-42.9	-51.7	-47.8	-70.0	-53.8	-62.6	-59.4	-53.6	-58.5	-59.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-74.9	-46.4	ND	ND	ND	ND	ND	-29.8	ND	-30.9	-54.3	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	6.9	-14.1	ND	ND	ND	ND	ND	-32.8	ND	-22.8	-4.2	ND
307 VD10-13		$pK_{a,SA}$	8.14	$K_{d,int}$ (nM)	0.0094	0.32	480	8.5	18	0.056	1.2	0.34	0.61	5.8	0.68	0.13
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-48.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-65.5	-56.4	-37.5	-47.9	-46.0	-60.9	-52.9	-56.2	-54.7	-48.9	-54.4	-58.7
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-84.1	-50.7	ND	ND	ND	ND	ND	-27.8	-43.6	-33.5	-57.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.9	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	18.6	-5.8	ND	ND	ND	ND	ND	-28.4	-11.1	-15.4	2.9	ND
308 AZ13-1		$pK_{a,SA}$	7.43	$K_{d,int}$ (nM)	0.22	2.4	2200	150	36	5.4	12	1.5	2.3	26	12	3.0
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-44.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.3	-51.2	-33.6	-40.4	-44.2	-49.1	-47.0	-52.4	-51.3	-45.0	-47.0	-50.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-23.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-70.6	-49.3	ND	ND	ND	ND	ND	-29.2	-34.0	-40.7	-48.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	13.3	-1.8	ND	ND	ND	ND	ND	-23.2	-17.3	-4.3	1.1	ND
309 VD12-01		$pK_{a,SA}$	8.14	$K_{d,int}$ (nM)	0.020	0.45	ND	5.5	15	0.56	6.1	0.13	1.3	1.3	0.41	2.2
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-48.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-63.6	-55.5	ND	-49.0	-46.5	-54.9	-48.8	-58.7	-52.8	-52.8	-55.7	-51.4
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-73.7	-53.0	ND	ND	ND	ND	ND	-32.7	ND	-30.5	-63.8	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.9	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	10.1	-2.5	ND	ND	ND	ND	ND	-25.9	ND	-22.2	8.1	ND
310 VD10-35		$pK_{a,SA}$	7.28	$K_{d,int}$ (nM)	0.064	2.5	1700	50	71	3.8	2.1	0.95	4.0	33	8.9	4.4
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-43.2	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.5	-51.0	-34.3	-43.3	-42.5	-50.0	-51.5	-53.6	-49.9	-44.4	-47.8	-49.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-23.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-76.8	-45.9	ND	ND	ND	ND	ND	-28.3	-35.5	-24.2	-50.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.4	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	16.2	-5.1	ND	ND	ND	ND	ND	-25.3	-14.3	-20.2	2.6	ND
311 VD10-49		$pK_{a,SA}$	7.83	$K_{d,int}$ (nM)	0.13	0.037	ND	27	17	0.13	2.3	0.011	0.19	5.9	0.037	0.025
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.5	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-58.8	-61.9	ND	-45.0	-46.1	-58.7	-51.2	-65.1	-57.8	-48.9	-61.9	-63.0
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-53.0	-37.2	ND	ND	ND	ND	ND	-28.5	ND	-31.5	-43.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-5.8	-24.7	ND	ND	ND	ND	ND	-36.5	ND	-17.3	-18.3	ND
312 VD10-28		$pK_{a,SA}$	7.69	$K_{d,int}$ (nM)	0.063	0.50	ND	4.2	2.8	0.42	3.4	0.82	0.40	7.3	0.39	0.33
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-45.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-60.6	-55.2	ND	-49.7	-50.8	-55.7	-50.3	-54.0	-55.8	-48.3	-55.9	-56.3
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-54.6	-34.6	ND	ND	ND	ND	ND	-21.5	ND	-33.1	-43.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-5.9	-20.7	ND	ND	ND	ND	ND	-32.5	ND	-15.2	-12.2	ND
313 VD10-14		$pK_{a,SA}$	8.84	$K_{d,int}$ (nM)	0.18	0.57	ND	4.8	10	7.1	1.3	1.7	2.9	6.2	1.9	0.92
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-52.5	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-57.9	-54.9	ND	-49.4	-47.4	-48.4	-52.8	-52.1	-50.7	-48.7	-51.9	-53.7
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-69.6	-43.0	ND	ND	ND	ND	ND	-28.2	ND	-30.3	-48.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	11.6	-11.9	ND	ND	ND	ND	ND	-23.9	ND	-18.4	-3.3	ND

No. Cpd	Structure			CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
314 VD10-16		$pK_{a,SA}$	8.47	$K_{d,int}$ (nM)	0.0061	0.13	ND	7.5	22	0.14	3.7	0.55	0.23	4.2	0.15	0.048
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-50.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-66.6	-58.7	ND	-48.3	-45.5	-58.6	-50.0	-55.0	-57.2	-49.7	-58.3	-61.3
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.8	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-76.4	-55.1	ND	ND	ND	ND	ND	-26.3	ND	-39.2	-52.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	18.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	9.8	-3.6	ND	ND	ND	ND	ND	-28.7	ND	-10.5	-6.2	ND
315 VD12-70		$pK_{a,SA}$	8.50	$K_{d,int}$ (nM)	0.0048	0.14	ND	580	10	ND	5.1	0.24	0.16	4.0	0.070	0.079
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-50.5	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-67.2	-58.6	ND	-37.0	-47.4	ND	-49.3	-57.2	-58.2	-49.9	-60.3	-60.0
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-31.2	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-76.7	-56.5	ND	ND	ND	ND	ND	-37.1	ND	-43.5	-55.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	19.3	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	9.5	-2.1	ND	ND	ND	ND	ND	-20.1	ND	-6.4	-5.1	ND
316 VD12-13		$pK_{a,SA}$	8.61	$K_{d,int}$ (nM)	0.011	0.018	ND	2.4	5.3	0.023	ND	0.0046	0.076	1.4	0.0087	0.062
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-51.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-65.0	-63.8	ND	-51.1	-49.1	-63.2	ND	-67.3	-60.1	-52.5	-65.7	-60.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-30.1	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-67.9	-46.6	ND	ND	ND	ND	ND	-34.5	ND	-39.6	-69.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	2.8	-17.3	ND	ND	ND	ND	ND	-32.8	ND	-12.9	3.6	ND
318 VD12-63		$pK_{a,SA}$	8.26	$K_{d,int}$ (nM)	0.0026	0.29	ND	53	18	0.65	7.9	0.29	0.22	2.0	0.59	0.17
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-49.0	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-68.8	-56.6	ND	-43.2	-46.0	-54.5	-48.1	-56.7	-57.3	-51.6	-54.8	-58.0
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-25.5	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-59.7	-45.0	ND	ND	ND	ND	ND	-25.6	ND	-31.5	-35.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	23.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-9.1	-11.7	ND	ND	ND	ND	ND	-31.1	ND	-20.2	-19.2	ND
319 VD10-12		$pK_{a,SA}$	8.61	$K_{d,int}$ (nM)	0.0022	0.19	ND	11	20	12	2.4	0.42	0.34	4.6	0.60	0.13
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-51.1	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-69.3	-57.7	ND	-47.2	-45.7	-47.0	-51.2	-55.7	-56.2	-49.5	-54.8	-58.7
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-29.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-84.8	-51.5	ND	ND	ND	ND	ND	-40.0	ND	-44.7	-49.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	15.5	-6.2	ND	ND	ND	ND	ND	-15.6	ND	-4.8	-5.6	ND
320 VD10-51		$pK_{a,SA}$	8.58	$K_{d,int}$ (nM)	0.0012	0.057	ND	3.3	4.3	0.064	1.2	0.0099	0.024	0.17	0.012	0.0066
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-50.9	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-70.8	-60.8	ND	-50.4	-49.7	-60.5	-53.0	-65.3	-63.0	-58.1	-64.9	-66.4
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-25.9	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-50.2	-24.6	ND	ND	ND	ND	ND	-31.7	ND	-38.2	-30.3	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	25.0	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-20.6	-36.2	ND	ND	ND	ND	ND	-33.6	ND	-19.9	-34.6	ND
321 VD12-47		$pK_{a,SA}$	7.86	$K_{d,int}$ (nM)	0.011	0.085	ND	29	11	0.061	4.4	0.047	0.58	2.3	0.11	0.16
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-65.0	-59.8	ND	-44.8	-47.3	-60.7	-49.6	-61.3	-54.9	-51.2	-59.1	-58.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-26.4	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-77.5	-57.3	ND	ND	ND	ND	ND	-24.6	ND	-39.5	-43.9	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	20.3	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	12.4	-2.5	ND	ND	ND	ND	ND	-36.7	ND	-11.8	-15.2	ND
323 VD11-56		$pK_{a,SA}$	7.97	$K_{d,int}$ (nM)	0.036	0.86	ND	11	18	3.2	4.4	0.37	1.4	3.4	1.8	1.2
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-47.3	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-62.0	-53.8	ND	-47.3	-45.9	-50.4	-49.6	-56.0	-52.6	-50.3	-52.0	-52.9
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-25.5	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-80.6	-55.2	ND	ND	ND	ND	ND	-32.3	ND	-25.4	-54.3	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	21.8	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	18.5	1.4	ND	ND	ND	ND	ND	-23.7	ND	-24.9	2.3	ND





No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
335 VD12-36		8.78	$K_{d,int}$ (nM)	9.3	1.7	ND	6.8	13	0.16	5.9	1.8	0.047	4.6	2.1	0.53
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.7	-52.1	ND	-48.5	-46.9	-58.1	-48.8	-51.9	-61.3	-49.5	-51.6	-55.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-7.5	-31.6	ND	ND	ND	ND	ND	-5.8	-18.8	-24.4	-9.6	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-40.2	-20.6	ND	ND	ND	ND	ND	-46.1	-42.6	-25.2	-41.9	ND
337 VD12-38		8.62	$K_{d,int}$ (nM)	260	32	ND	270	160	0.78	7.6	130	0.39	23	8.2	3.0
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-39.1	-44.5	ND	-39.0	-40.4	-54.1	-48.2	-40.8	-55.9	-45.4	-48.0	-50.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-5.3	ND	ND	ND	ND	ND	ND	-14.8	-19.3	4.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-39.2	ND	ND	ND	ND	ND	ND	-41.1	-26.1	-52.2	ND
341 VD12-09		8.68	$K_{d,int}$ (nM)	460	9.1	980	8.9	45	1.0	9.3	1.6	0.0045	1.9	1.8	1.1
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-37.6	-47.7	-35.7	-47.8	-43.6	-53.4	-47.7	-52.2	-67.4	-51.8	-51.9	-53.1
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-7.3	ND	ND	ND	-50.3	ND	-2.2	-18.8	-24.8	-12.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-40.4	ND	ND	ND	-3.1	ND	-50.0	-48.6	-27.0	-39.2	ND
345 VD12-15		8.61	$K_{d,int}$ (nM)	180	29	ND	45	160	4.0	7.3	15	0.051	12	0.73	1.5
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.0	-44.7	ND	-43.6	-40.4	-49.9	-48.3	-46.4	-61.1	-47.1	-54.3	-52.3
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	-13.6	-18.1	-11.0	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	ND	ND	ND	ND	ND	ND	ND	-47.5	-29.0	-43.3	ND
367 AZ13-2-2		8.18	$K_{d,int}$ (nM)	3300	61	3000	220	69	57	22	12	0.0071	6.0	9.4	5.7
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-32.5	-42.8	-32.8	-39.5	-42.5	-43.0	-45.5	-47.0	-66.2	-48.8	-47.7	-49.0
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	0.9	ND	ND	ND	ND	ND	-1.1	-20.9	-28.6	-2.1	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-43.8	ND	ND	ND	ND	ND	-45.9	-45.3	-20.2	-45.5	ND
368 VD10-39b		7.85	$K_{d,int}$ (nM)	23	4.6	ND	3.2	27	0.21	1.5	6.0	0.022	1.2	1.6	0.60
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-45.4	-49.5	ND	-50.4	-44.9	-57.5	-52.4	-48.8	-63.3	-53.0	-52.2	-54.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-53.7	-22.1	ND	ND	ND	ND	-16.2	-14.7	-25.8	-35.5	-32.4	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	8.3	-27.4	ND	ND	ND	ND	-36.1	-34.1	-37.5	-17.5	-19.8	ND

No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
369 VD11-4-2		8.01	$K_{d,int}$ (nM)	69	2.2	720	1.5	200	0.70	0.54	0.30	0.00080	0.10	0.33	0.15
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.5	-51.4	-36.5	-52.3	-39.8	-54.3	-55.0	-56.6	-71.8	-59.3	-56.3	-58.4
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	0.8	-7.7	ND	ND	ND	ND	ND	-12.2	-24.3	-40.9	-11.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-43.4	-43.7	ND	ND	ND	ND	ND	-44.4	-47.5	-18.4	-45.1	ND
371 VD12-32		7.82	$K_{d,int}$ (nM)	27	1.3	6300	5.3	88	0.66	12	2.0	0.025	3.4	3.0	1.3
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-44.9	-52.8	-30.9	-49.1	-41.9	-54.5	-47.0	-51.6	-63.0	-50.3	-50.6	-52.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-54.8	-51.9	ND	ND	ND	ND	ND	-21.3	-22.9	-17.1	-2.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	9.9	-0.8	ND	ND	ND	ND	ND	-30.3	-40.0	-33.2	-48.2	ND
372 VD12-33		7.87	$K_{d,int}$ (nM)	9.2	9.3	ND	14	5.3	2.0	5.4	0.66	0.085	3.8	0.47	23
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.7	-47.7	ND	-46.7	-49.1	-51.7	-49.1	-54.5	-59.8	-50.0	-55.4	-45.4
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-24.1	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-23.6	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
373 VD12-34		7.85	$K_{d,int}$ (nM)	110	0.91	ND	2.3	130	0.52	1.1	0.24	0.0039	0.40	0.94	0.20
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-41.2	-53.7	ND	-51.2	-40.8	-55.1	-53.1	-57.1	-67.7	-55.8	-53.6	-57.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	-15.9	-36.4	ND	ND	ND	ND	ND	-12.0	-27.9	-47.0	-21.2	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	-25.3	-17.3	ND	ND	ND	ND	ND	-45.2	-39.9	-8.8	-32.4	ND
374 VD12-23		7.87	$K_{d,int}$ (nM)	160	3.2	ND	6.8	79	9.1	4.9	0.46	0.0017	0.60	1.1	0.30
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-40.4	-50.5	ND	-48.5	-42.2	-47.7	-49.3	-55.4	-69.9	-54.8	-53.2	-56.6
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-45.1	ND	ND	ND	ND	ND	-39.1	ND	-29.5	-45.7	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-5.4	ND	ND	ND	ND	ND	-16.3	ND	-25.3	-7.5	ND

No. Cpd	Structure				CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV
375 VD12-25-2		$pK_{a,SA}$	7.88	$K_{d,int}$ (nM)	2400	3.3	ND	ND	390	0.58	3.9	1.5	ND	0.71	0.52	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.8	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-33.3	-50.4	ND	ND	-38.1	-54.8	-49.9	-52.4	ND	-54.3	-55.1	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.3	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	1.3	ND	ND	ND	ND	ND	-3.4	ND	-24.3	-25.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.5	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-51.7	ND	ND	ND	ND	ND	-49.0	ND	-30.1	-29.6	ND
376 VD11-26		$pK_{a,SA}$	7.87	$K_{d,int}$ (nM)	8.2	0.31	ND	3400	40	0.40	1.1	0.38	0.26	13	0.14	0.23
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-48.0	-56.5	ND	-32.5	-44.0	-55.8	-53.2	-55.9	-57.0	-46.8	-58.6	-57.2
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-49.0	ND	ND	ND	ND	ND	ND	ND	-27.5	-42.0	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-7.4	ND	ND	ND	ND	ND	ND	ND	-19.2	-16.6	ND
377 VD11-25		$pK_{a,SA}$	7.87	$K_{d,int}$ (nM)	73	0.088	ND	8.3	57	0.030	0.54	0.010	0.029	3.1	0.54	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.4	-59.7	ND	-48.0	-43.0	-62.5	-55.0	-65.3	-62.6	-50.6	-55.0	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-19.6	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-40.1	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
378 VD11-28		$pK_{a,SA}$	7.87	$K_{d,int}$ (nM)	5.8	0.35	ND	31	20	0.40	1.2	0.23	0.11	1.8	0.27	ND
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-48.9	-56.1	ND	-44.6	-45.7	-55.8	-53.0	-57.2	-59.1	-51.9	-56.8	ND
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-22.9	ND	ND	ND	ND	ND	ND	ND	ND	-17.5	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-33.3	ND	ND	ND	ND	ND	ND	ND	ND	-39.3	ND
380 VD11-15		$pK_{a,SA}$	7.87	$K_{d,int}$ (nM)	11	0.066	ND	42	40	0.24	0.43	0.11	0.19	7.1	0.54	0.19
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-47.3	-60.5	ND	-43.8	-44.0	-57.1	-55.6	-59.0	-57.7	-48.4	-55.0	-57.8
		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-27.6	ND	ND	ND	ND	ND	ND	ND	-19.0	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-32.9	ND	ND	ND	ND	ND	ND	ND	-29.4	ND	ND

No. Cpd	Structure	$pK_{a,SA}$	$K_{d,int}$ (nM)	CA I	CA II	CA III	CA IV	CA VA	CA VB	CA VI	CA VII	CA IX	CA XII	CA XIII	CA XIV	
<b>385</b>		$pK_{a,SA}$	7.87	71	2.6	ND	56	1100	4.0	3.6	0.23	ND	0.77	0.60	2.3	
		$\Delta G_{pr,SA}$ (kJ mol <sup>-1</sup> )	-46.7	$\Delta G_{int}$ (kJ mol <sup>-1</sup> )	-42.4	-50.9	ND	-43.0	-35.3	-49.9	-50.1	-57.2	ND	-54.1	-54.8	-51.3
VD11-17		$\Delta H_{pr,SA}$ (kJ mol <sup>-1</sup> )	-24.0	$\Delta H_{int}$ (kJ mol <sup>-1</sup> )	ND	-19.6	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
		$T\Delta S_{pr,SA}$ (kJ mol <sup>-1</sup> )	22.7	$-T\Delta S_{int}$ (kJ mol <sup>-1</sup> )	ND	-31.3	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND

## 2 Supplementary figures

### 2.1 X-Ray crystallographic structures of unliganded human CA isoforms

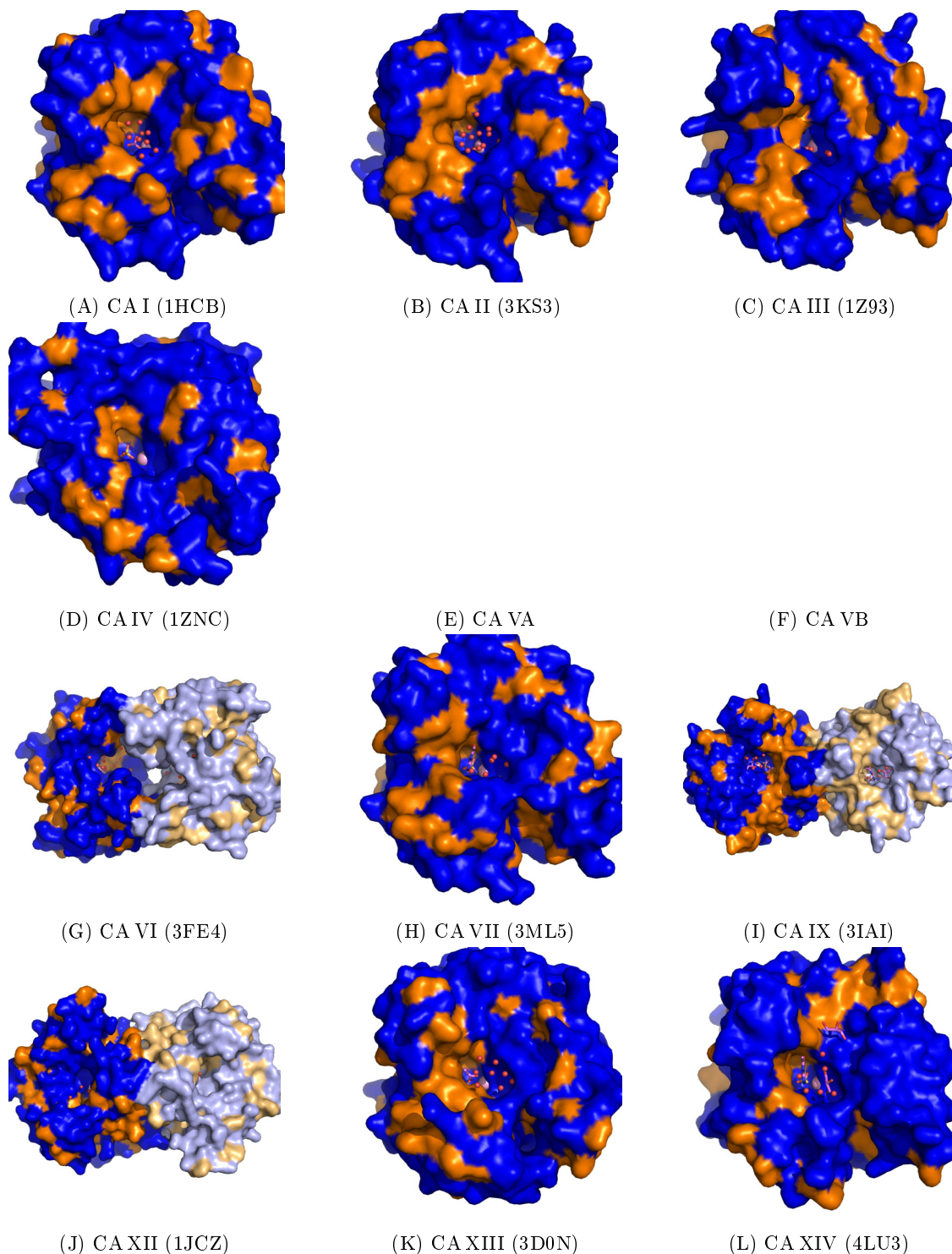


Figure 1: X-ray crystallographic structures of 10 catalytically active human CA isoforms, without an inhibitor in the active site. The monomeric ones are oriented in the same orientation with the active site cavities containing  $Zn^{II}$  in the front center of each picture. Hydrophobic amino acids are shown in yellow while hydrophilic – in blue. Water molecules in the active site are shown as red spheres while the catalytic  $Zn^{II}$  – as a pink sphere. The PDB IDs are listed in the brackets.

## 2.2 Crystal structure-thermodynamics correlations

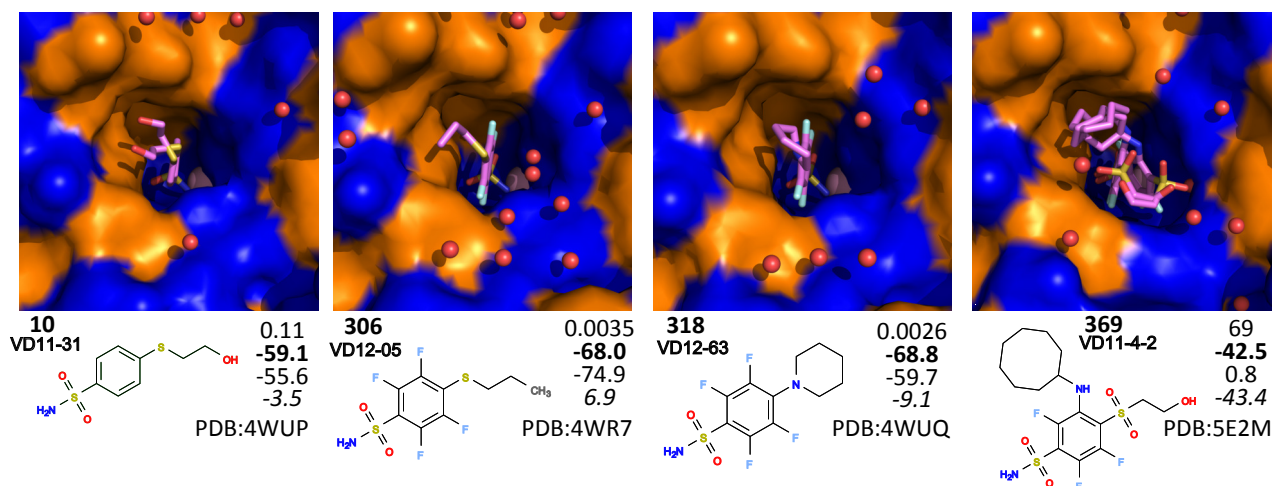


Figure 2: The X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of CA I together with the intrinsic thermodynamic parameters of compound binding. Compound chemical structures are shown below the crystal structures. Compound number and local name is listed on the left, while the numbers on the right show the  $K_{d\_intr}$  in nM, the intrinsic Gibbs energy of binding in kJ mol<sup>-1</sup>, the intrinsic enthalpy in kJ mol<sup>-1</sup>, the intrinsic entropy  $-T\Delta S$  in kJ mol<sup>-1</sup>, and the PDB ID of the crystal structure.

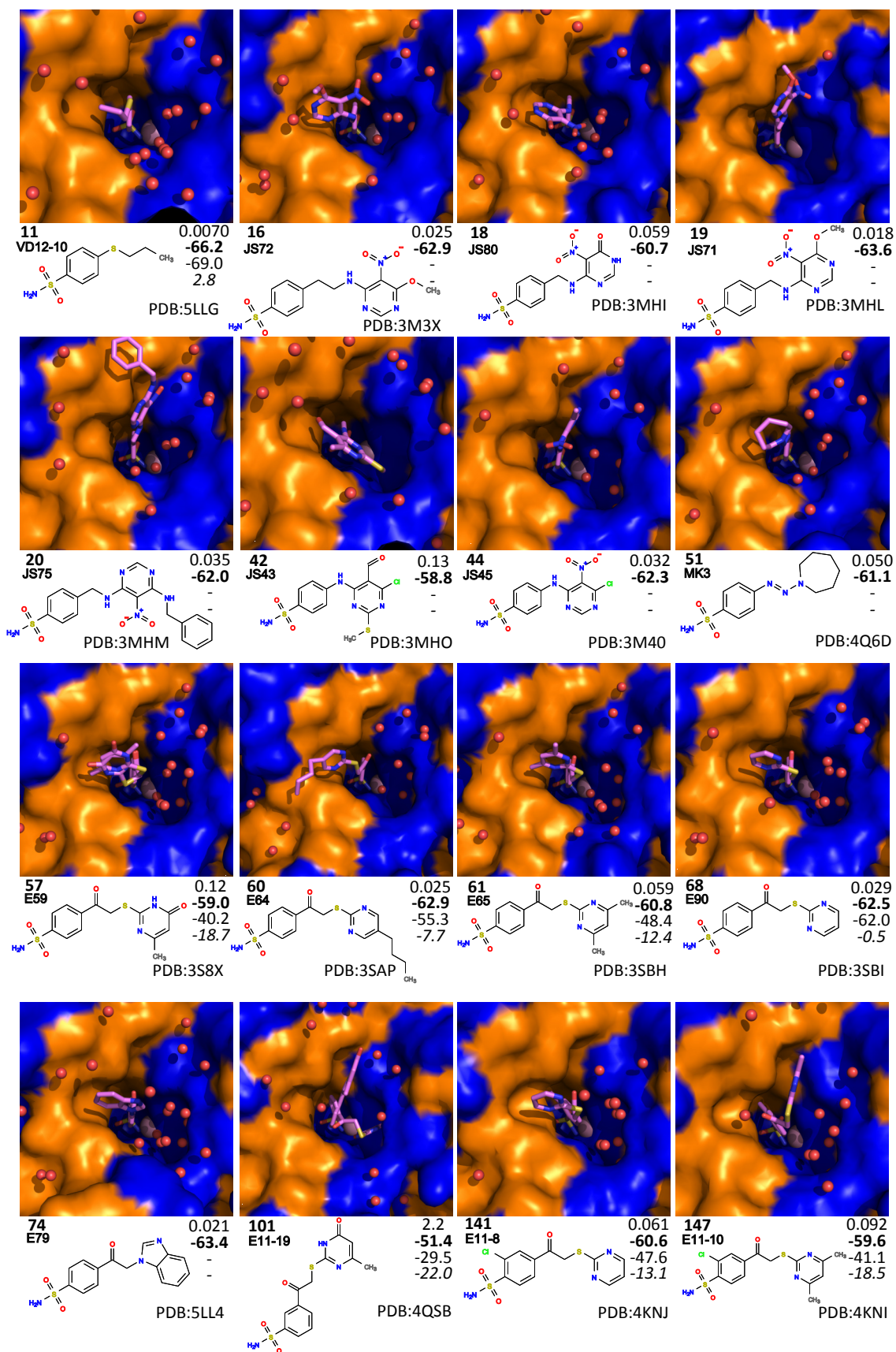


Figure 3: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAII. See explanation in the legend of Figure 2.



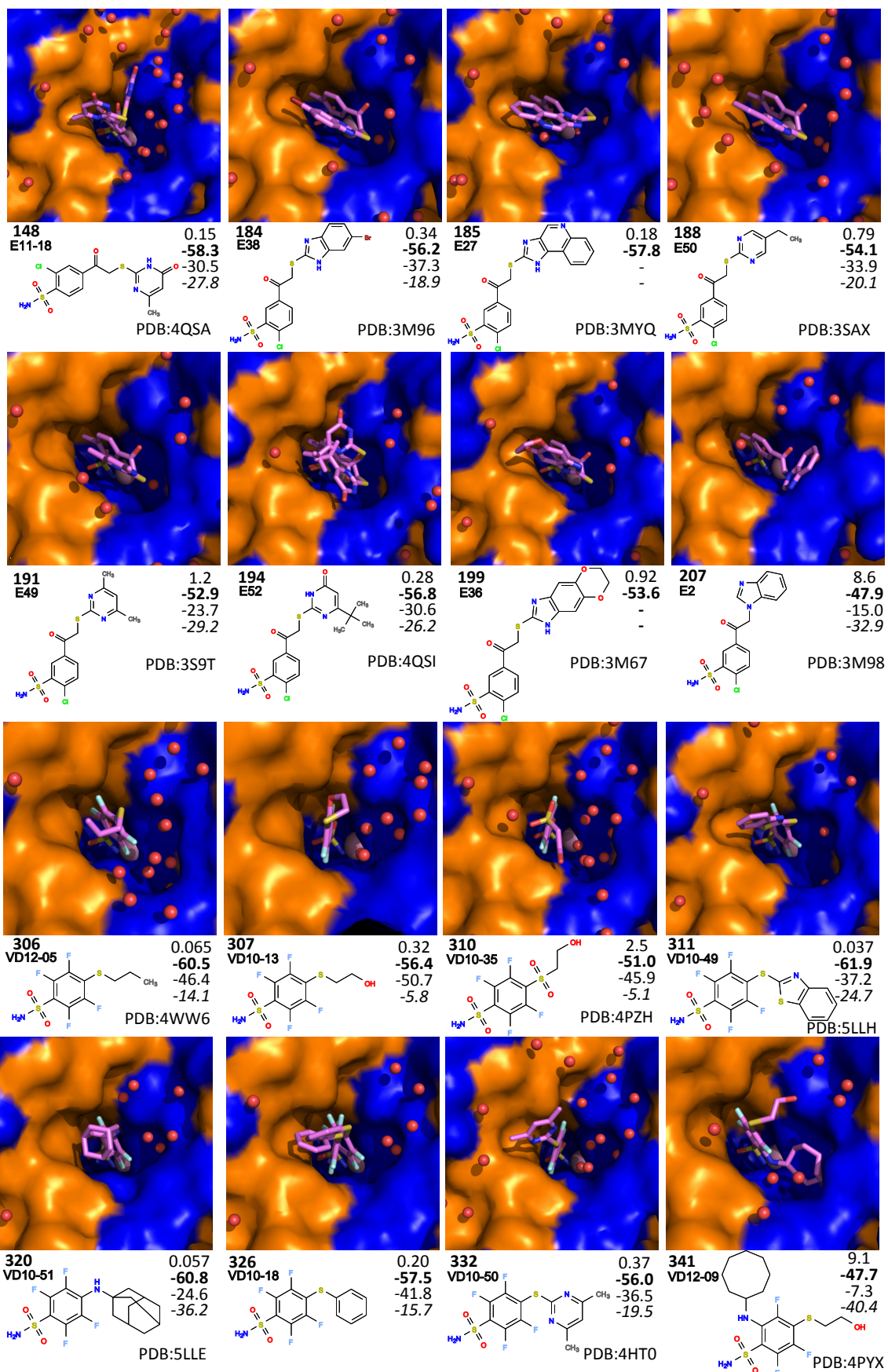


Figure 4: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAII. See explanation in the legend of Figure 2.

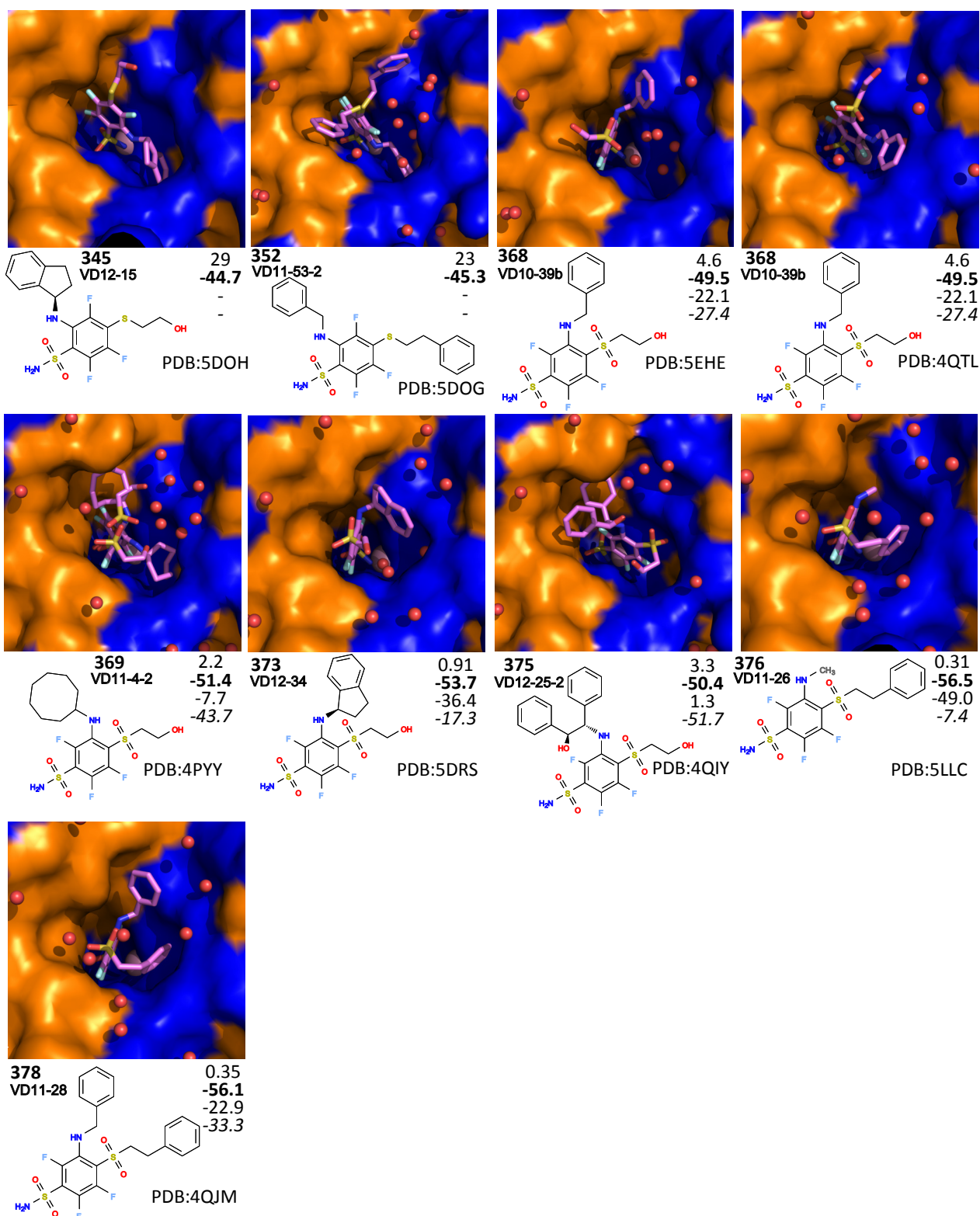


Figure 5: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAII. See explanation in the legend of Figure 2.

CA II complexes with ligands (intrinsic thermodynamic data at 25 C, Whitesides data)

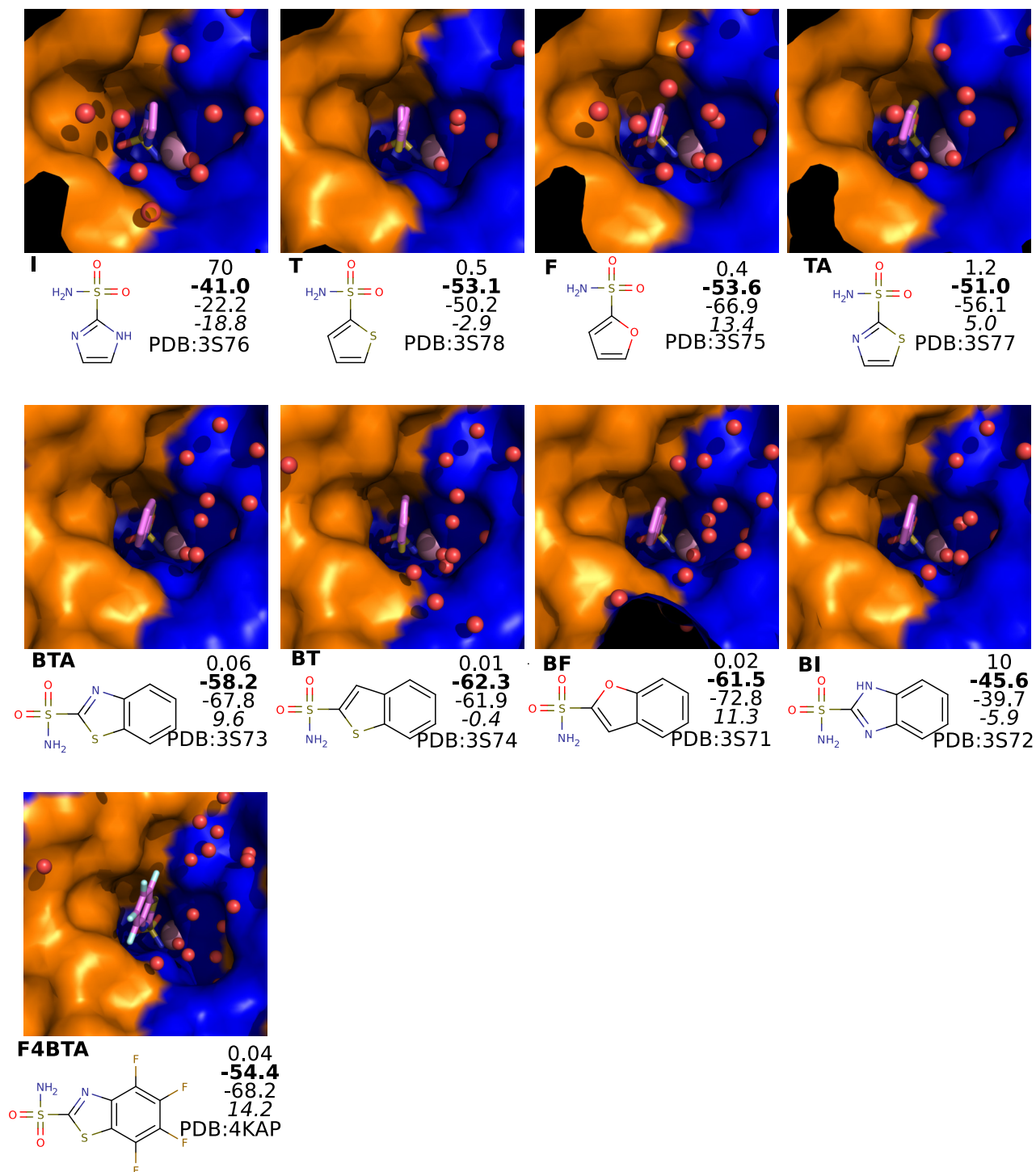


Figure 6: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. The structures are taken from the study by Whitesides group (Snyder,2011; Lockett, 2013), the inhibitors are bound in the active site of CA II. See explanation in the legend of Figure 2.



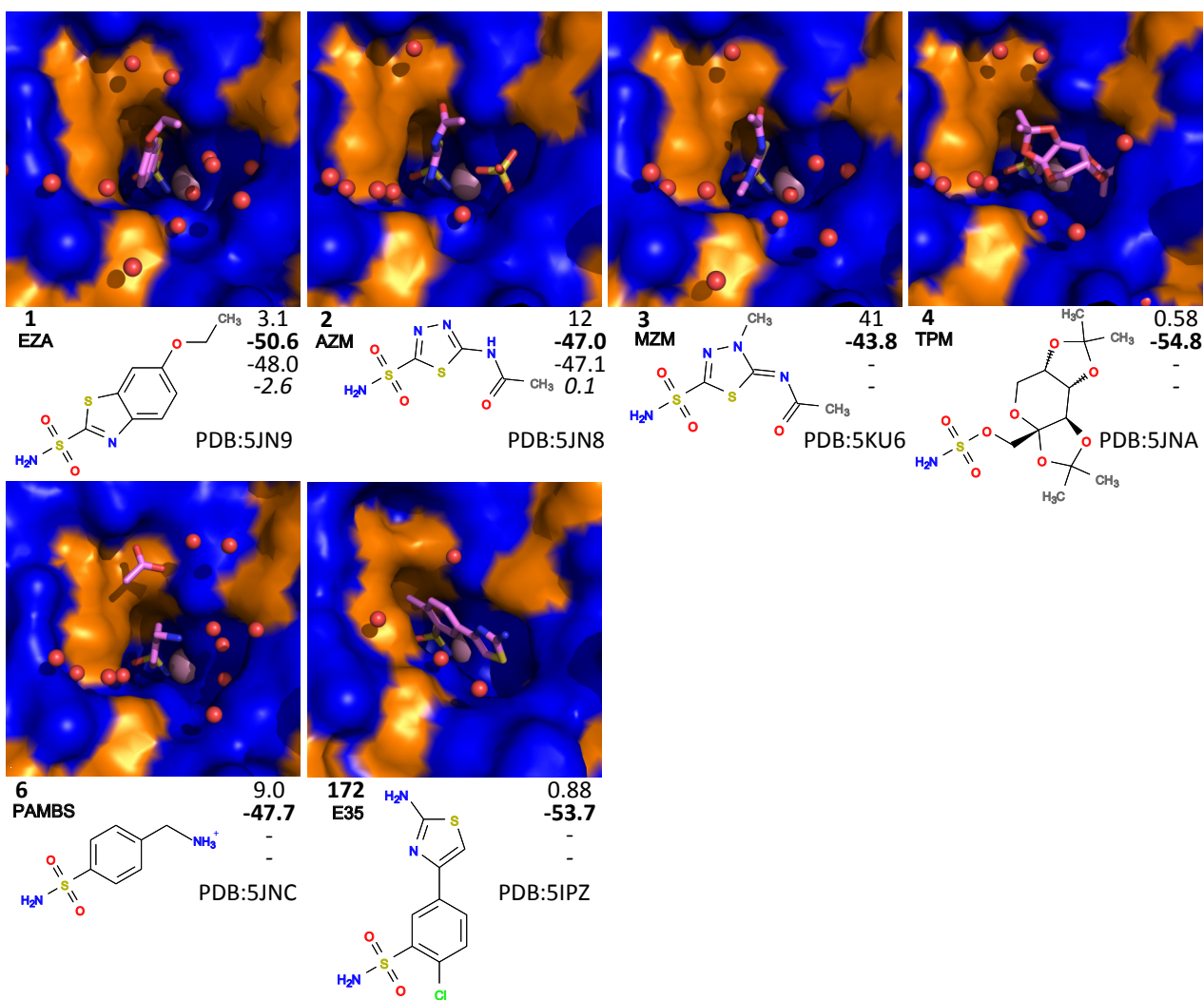


Figure 7: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAIV. See explanation in the legend of Figure 2.

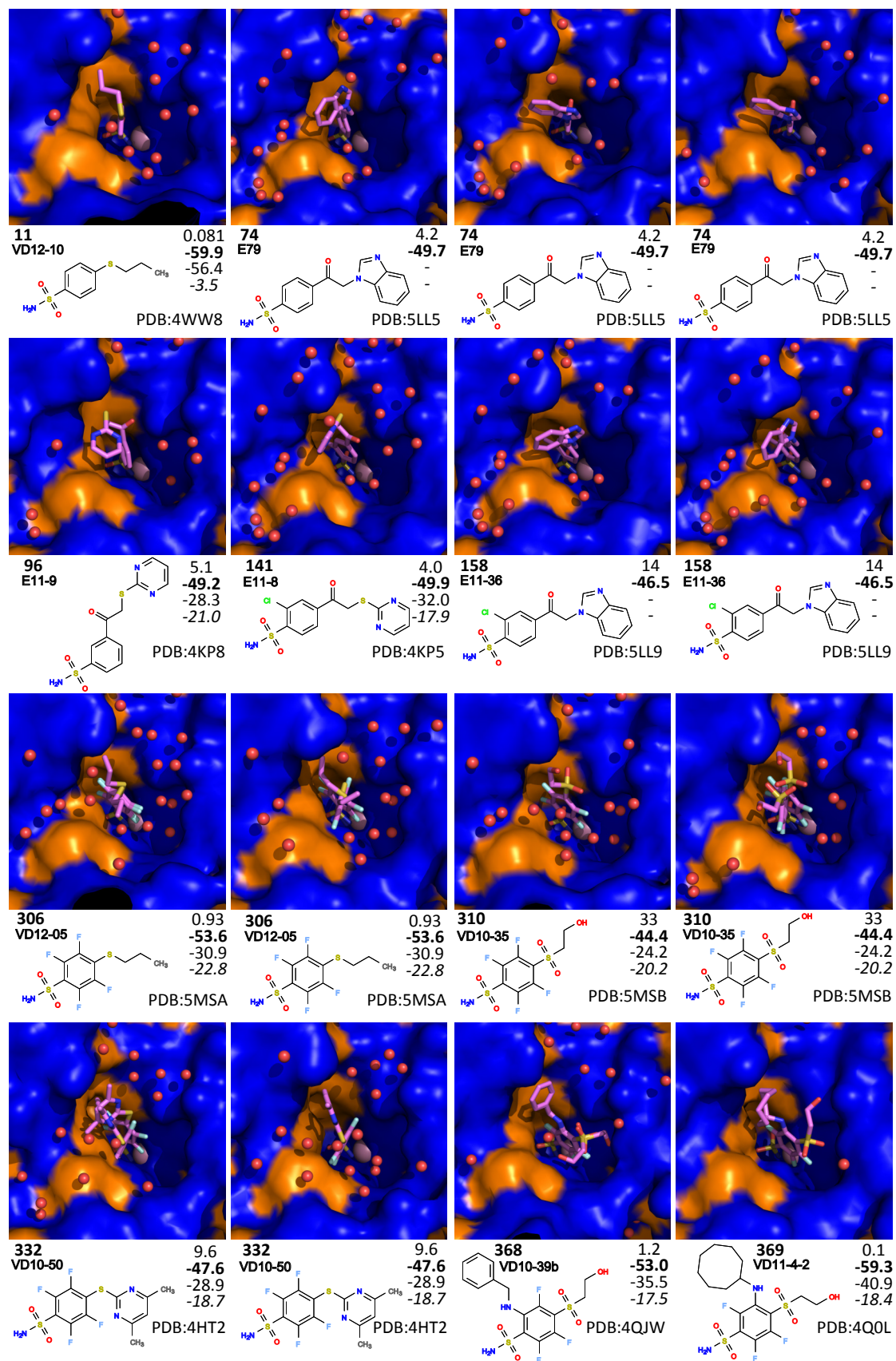


Figure 8: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAXII. See explanation in the legend of Figure 2.

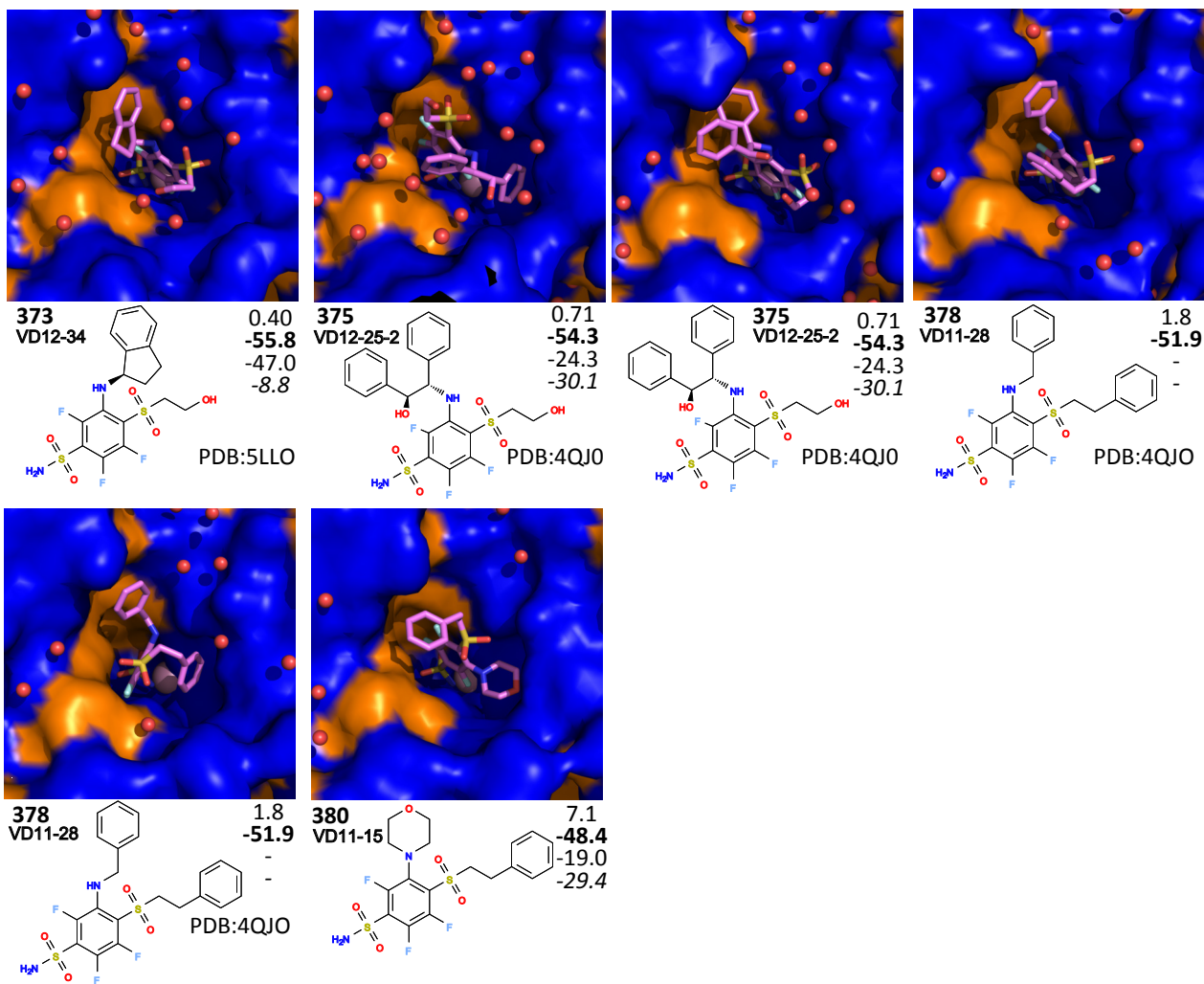


Figure 9: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CAXII. See explanation in the legend of Figure 2.



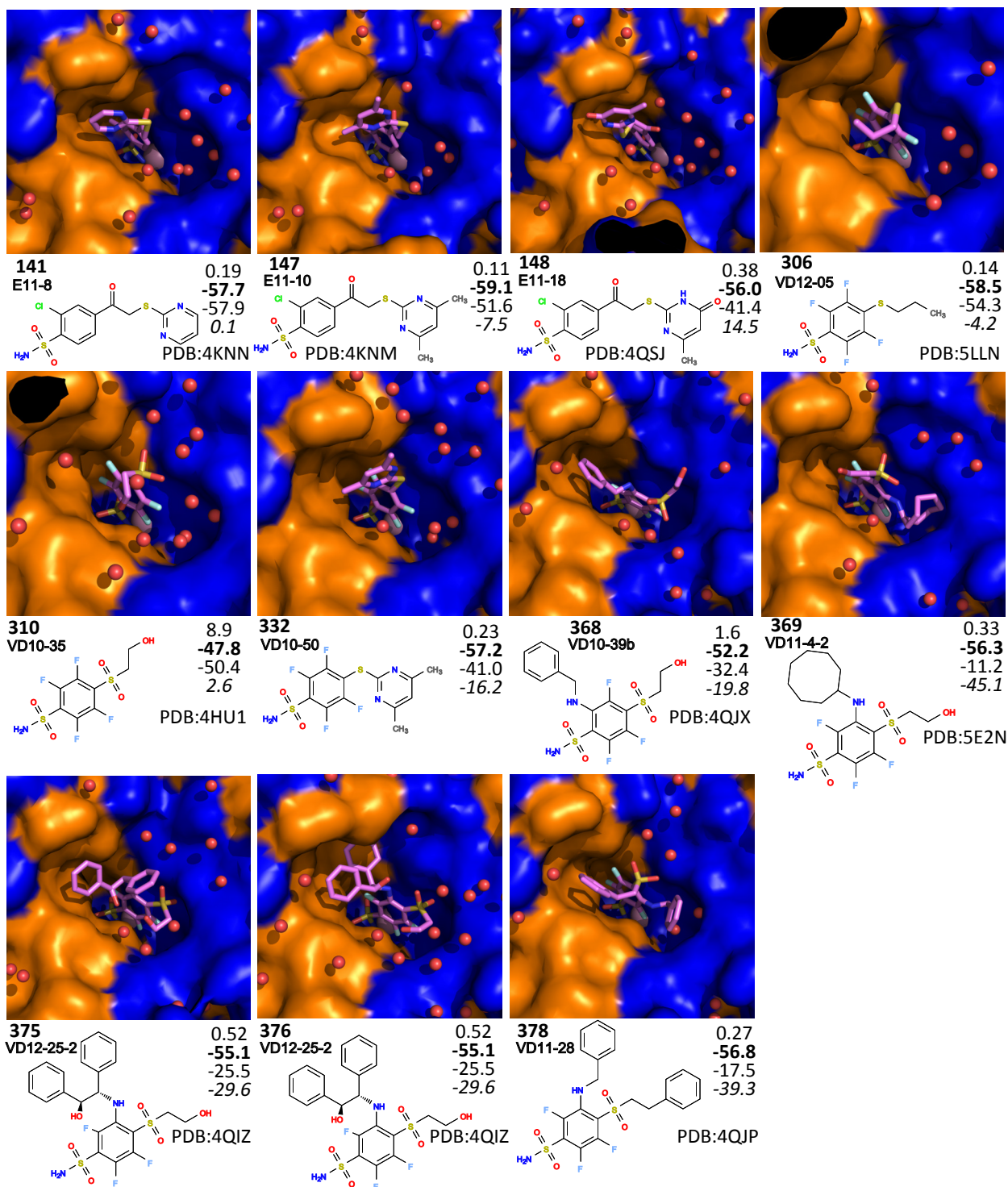


Figure 10: Continuation of the X-Ray crystallographic structure Pymol renderings of the inhibitors bound in the active site of a CA. This page lists inhibitors bound to CA XIII. See explanation in the legend of Figure 2.

## 2.3 Compound structure-thermodynamics correlation maps

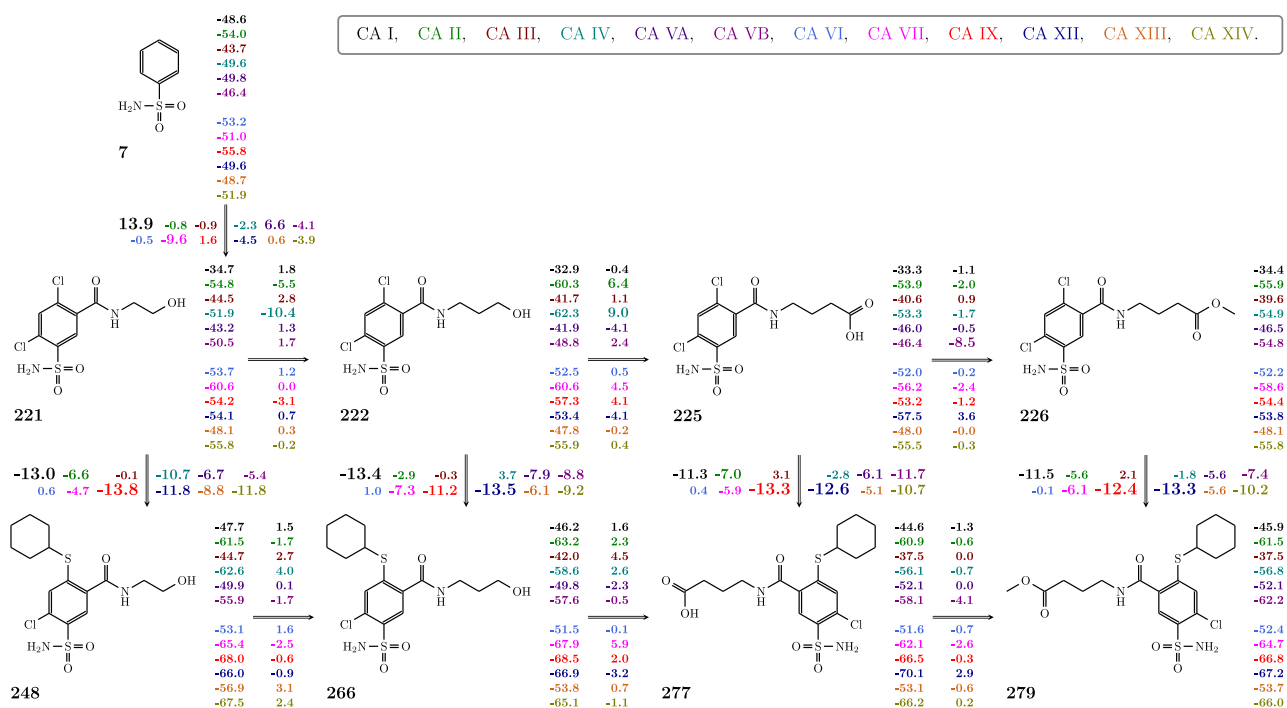


Figure 11: Gibbs energy contributions of compound functional groups in the search of chlorinated compounds that would selectively bind and inhibit CA XII. The map shows a series of compounds connected by arrows beginning with benzenesulfonamide as the weakest inhibitor and ending with the best inhibitors on the right. Numbers next to the structures show the intrinsic Gibbs energies of compound binding to each recombinant human CA isoform. Numbers at the arrows show the differences between the affinities to two connected isoforms. Larger differences are depicted in larger font size to emphasize the largest energy gains upon chemical modifications of the compounds.



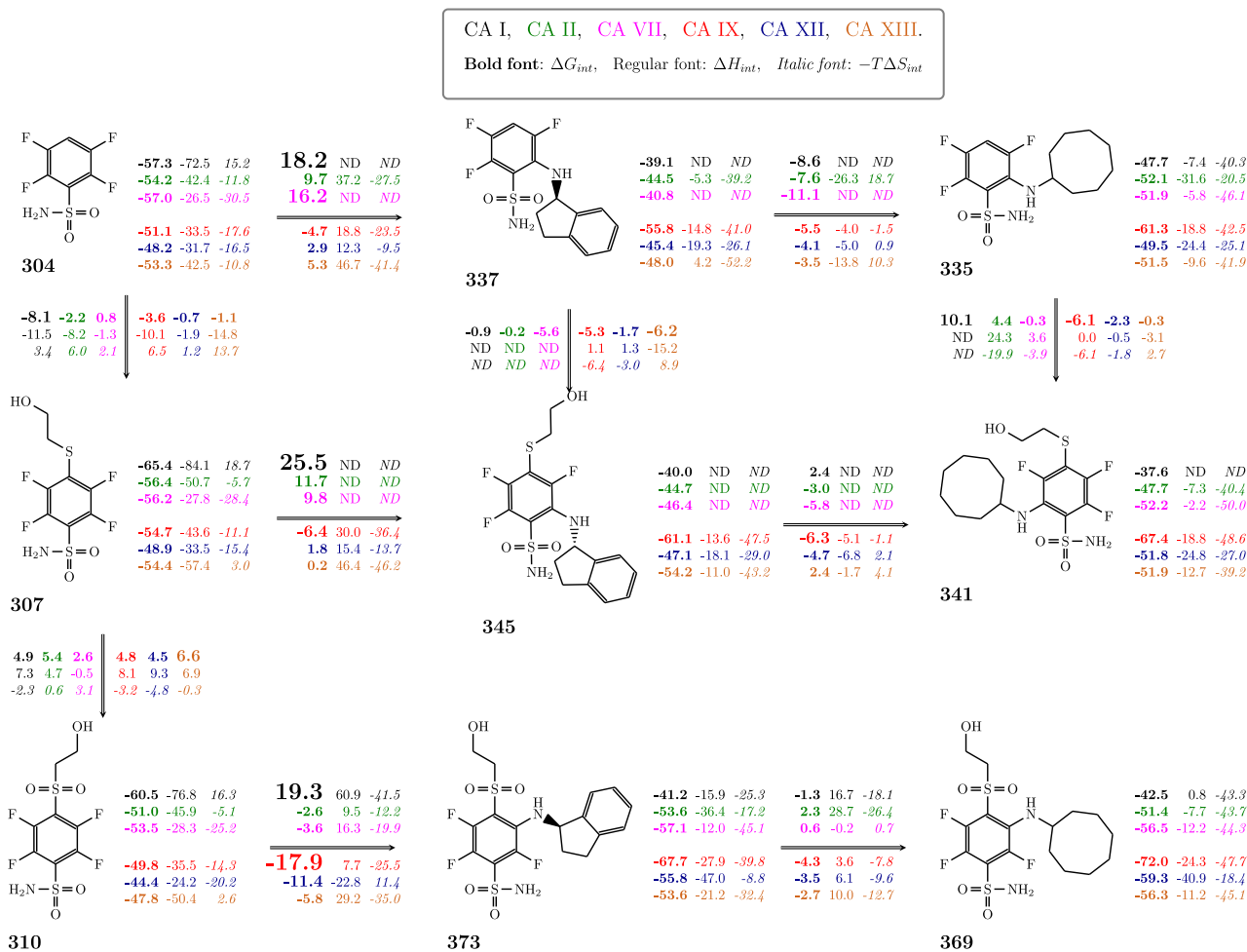


Figure 12: A map of intrinsic Gibbs energy, enthalpy, and entropy gains or loses upon chemical modification of compounds. The map begins with 2,3,5,6-tetrafluorobenzenesulfonamide on the left upper corner as a relatively weak binder and ends with high-affinity and high selectivity CA IX-binding compounds such as **369**. The numbers next to the compounds show the Gibbs energies, enthalpies, and entropies of binding to the tested six CA isoforms, while the numbers on the arrows show the differences in energetic parameters of binding between neighboring compounds. Quite often, the significant gain in affinity was not followed by a gain in exothermic enthalpy.