

Figures to be held in the editorial files

(1)

Numerical analysis of gas-particle two-phase flows

(Numerical Results)

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(2)

Table 1. Physical constants of gas and particles used in the numerical calculations.

Gas (Air)

$$\gamma = 1.4$$

$$\bar{C}_{p,g} = 1005 \text{ J/kg.K}$$

$$\bar{\mu} = 1.79 \times 10^{-5} \text{ kg/m.s}$$

(for $\bar{T} = 288 \text{ K}$)

$$\delta = 0.5$$

$$Pr = 0.75$$

Particles (Al_2O_3)

$$\bar{\rho}_{mp} = 4.0 \times 10^3 \text{ kg/m}^3$$

$$\bar{C}_{p,p} = 1686 \text{ J/kg.m}$$

Calculated flowfields

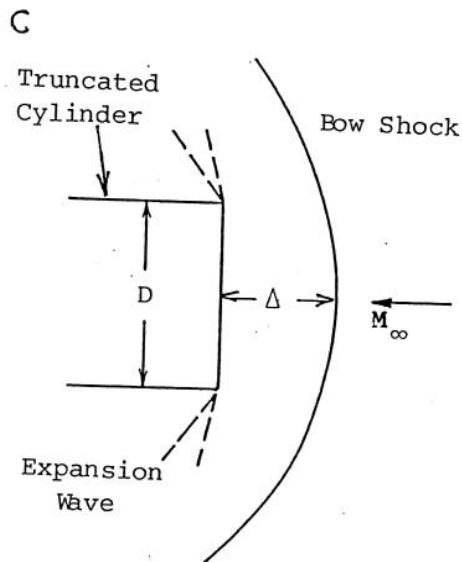
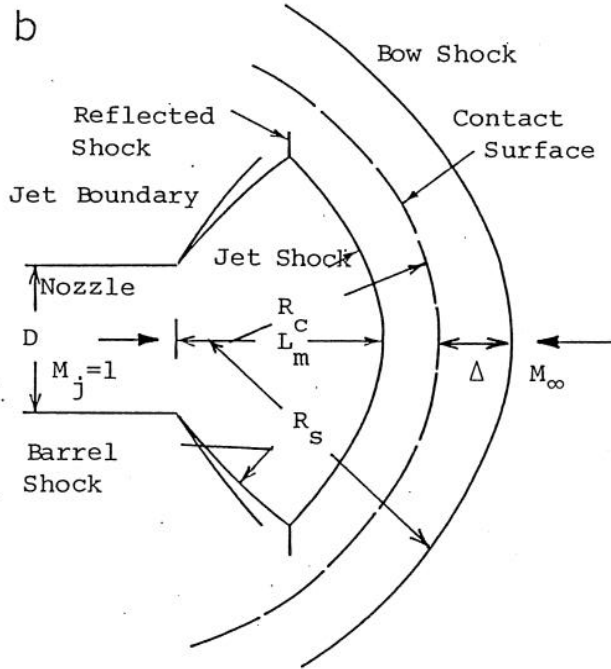
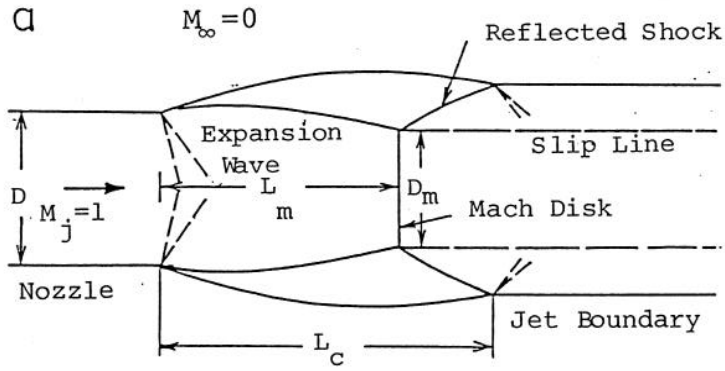


Figure captions

- B-1) Time history of density profile along the jet axis of a dust-free jet for $\bar{p}_0/\bar{p}_\infty = 20$. The jet begins to blow into a stagnant ambient gas region at $t = 0$ ($n = 0$). The flow Mach number of the jet at the nozzle exit is $M_j = 1$; $\Delta x = \Delta y = 0.1$.
- B-2) Time history of density profile along the axis of a dust-free opposing jet for $\bar{p}_0/\bar{p}_\infty = 20$. The jet begins to blow opposing to a uniform mainstream ($M_\infty = 2.0$) at $t = 0$ ($n=0$). The flow Mach number at the nozzle exit is $M_j = 1.0$; $\Delta x = \Delta y = 0.1$.
- B-3) Time history of density profile along the body axis. A uniform supersonic flow ($M_\infty = 2.0$) impinges on a truncated cylinder at time $t = 0$ ($n = 0$); $\Delta x = \Delta y = 0.02$.
- B-4) Time history of density profile along the jet axis of a dusty jet; $\bar{L} = 5$ cm, $\bar{p}_0 = 5$ atm, $\bar{p}_0/\bar{p}_\infty = 20$, $\bar{T}_0 = \bar{T}_\infty = 290$ K, $M_j = 1.0$, $M_\infty = 0$, $\nu_j = 0.3$, $\bar{r}_p = 1.0$ μ m, $\Delta x = \Delta y = 0.1$, $K = 50$, $F=0.8$. The particles are injected into the dust-free jet at the nozzle exit after $n = 6000$.
- B-5) Time history of density profile along the jet axis of a dusty opposing jet; $\bar{L} = 5$ cm, $\bar{p}_0 = 5$ atm, $\bar{p}_0/\bar{p}_\infty = 20$, $\bar{T}_0 = \bar{T}_\infty = 290$ K, $M_j = 1$, $M_\infty = 2.0$, $\nu_j = 0.3$, $\bar{r}_p = 1.0$ μ m, $\Delta x = \Delta y = 0.1$, $K = 50$, $F = 0.8$. The particles are injected into the dust-free jet at the nozzle exit after $n = 9000$.
- B-6) Time history of density profile along the body axis of a dusty supersonic flow around a truncated cylinder; $\bar{L} = 5$ cm, $\bar{p}_\infty = 0.5$ atm, $\bar{T}_\infty = 290$ K, $M_\infty = 2$, $\nu_\infty = 0.3$, $\bar{r}_p = 2$ μ m, $\Delta x = \Delta y = 0.05$, $K = 250$, $F = 0.8$. The particles are injected into the dust-free flow at a plane perpendicular to the body axis ahead of the bow shock after $n=4000$.

- B-7) Velocity field of the dust-free jet shown in figure B-1.
- B-8) Velocity field of the dust-free opposing jet shown in figure B-2.
- B-9) Flow field of the dust-free supersonic flow around a truncated cylinder shown in figure B-3. These are obtained with finer mesh than those shown in the text.
- B-10) Particle trajectories in the jet shown in figure B-1.
- B-11) Particle trajectories in the opposing jet shown in figure B-2.
- B-12) Particle trajectories in the supersonic flow around a truncated cylinder shown in figure B-3.
- B-13) Velocity and temperature distributions along the jet axis of the dusty jet shown in figure B-4.
- B-14) Velocity and temperature distributions along the jet axis of dusty opposing jet shown in figure B-5.
- B-15) Distributions of flow quantities in the dusty shock layer shown in figure B-6:
 - a) Density distributions along the body axis.
 - b) Pressure distributions along the body axis.
 - c) Temperature distributions along the body axis.
 - d) Velocity distributions along the body axis.
 - e) Density distributions along the body wall.
 - f) Pressure distributions along the body wall.
- B-16) Constant density contours of particle phase in the dusty shock layer shown in figure B-6.
- B-17) Spatial distributions of particle clouds in the whole computational region for the dusty supersonic flow around a truncated cylinder shown in figure B-6.

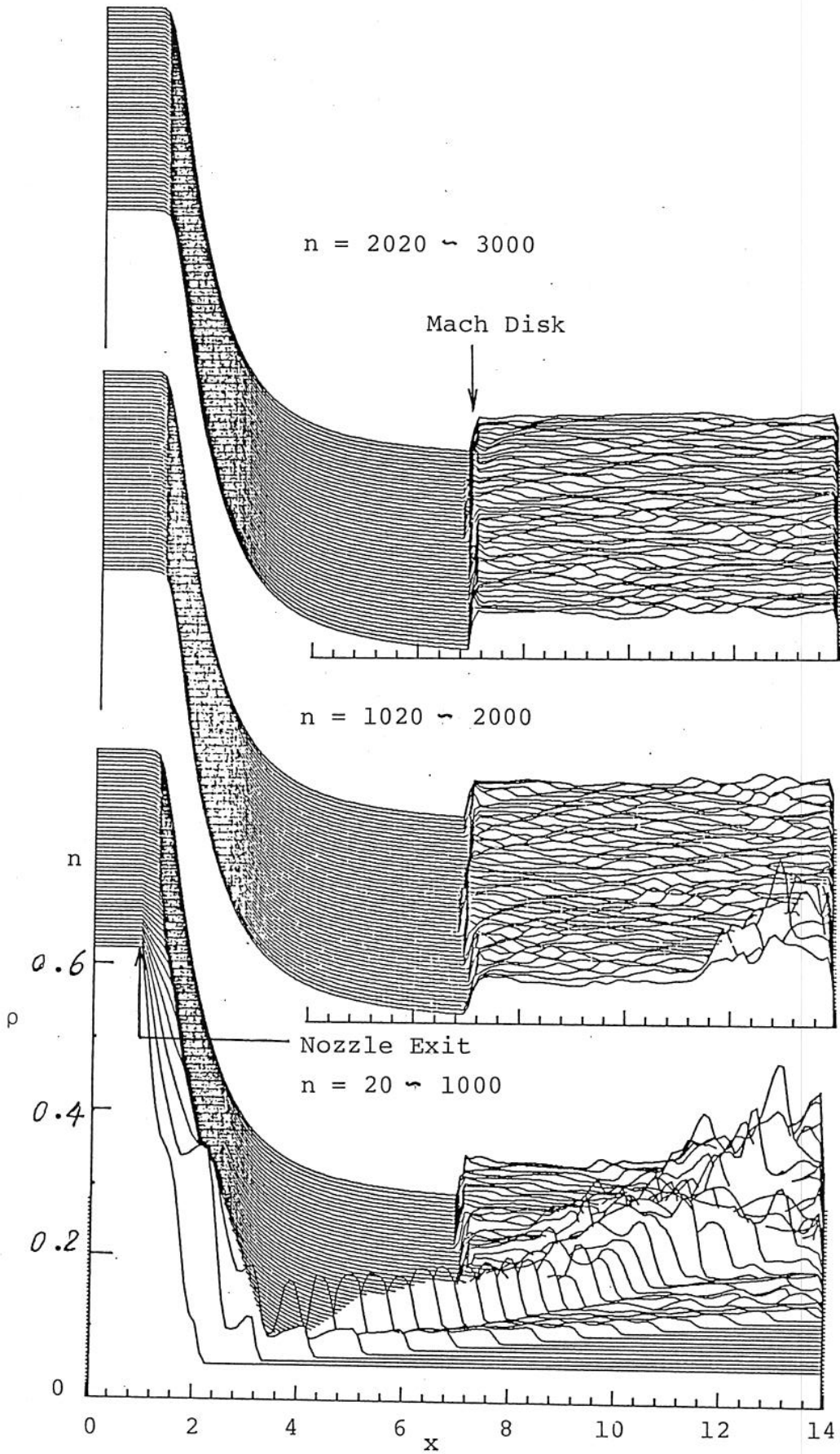


Fig. B-1 -1

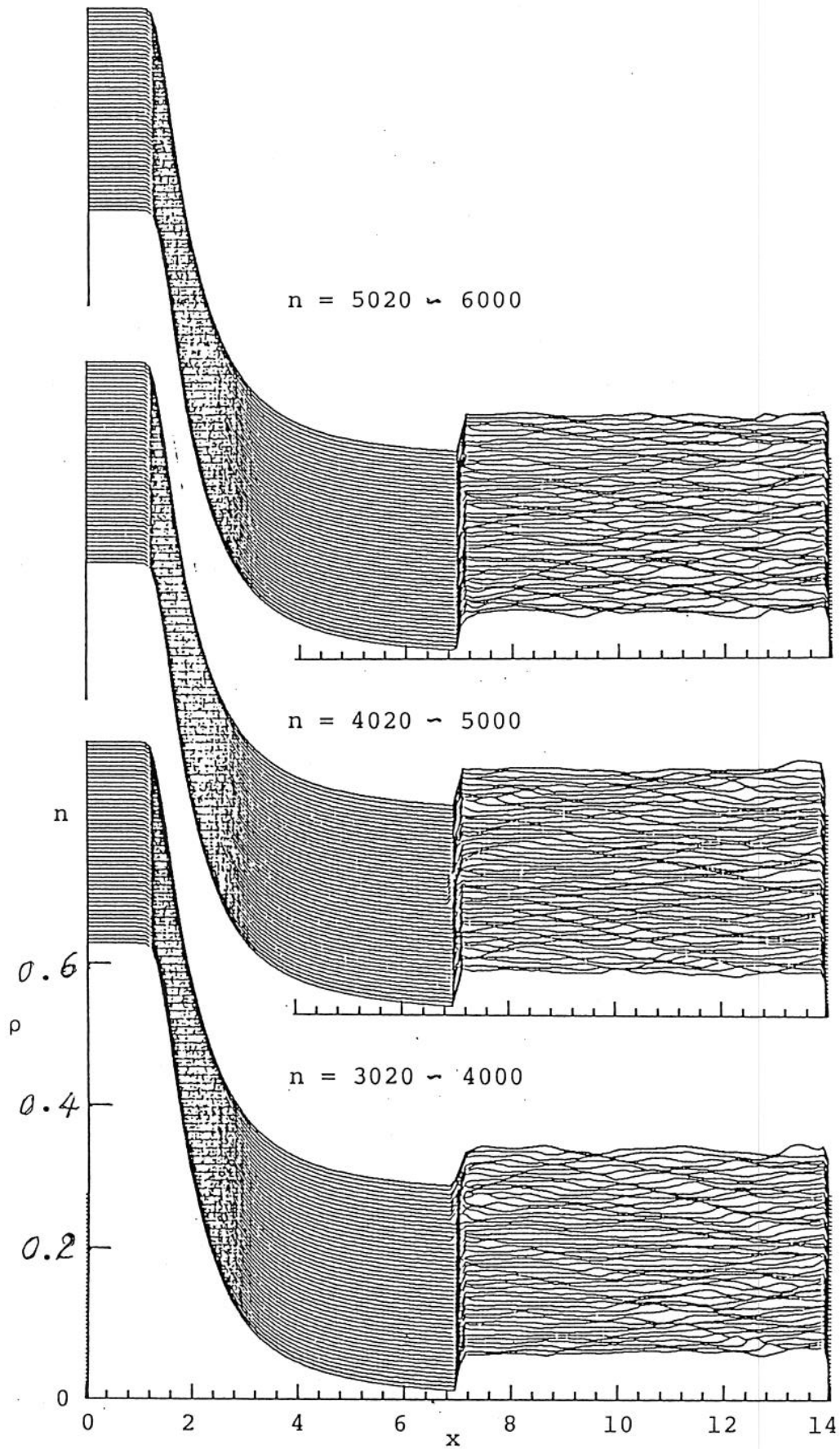


Fig. B-1 - 2

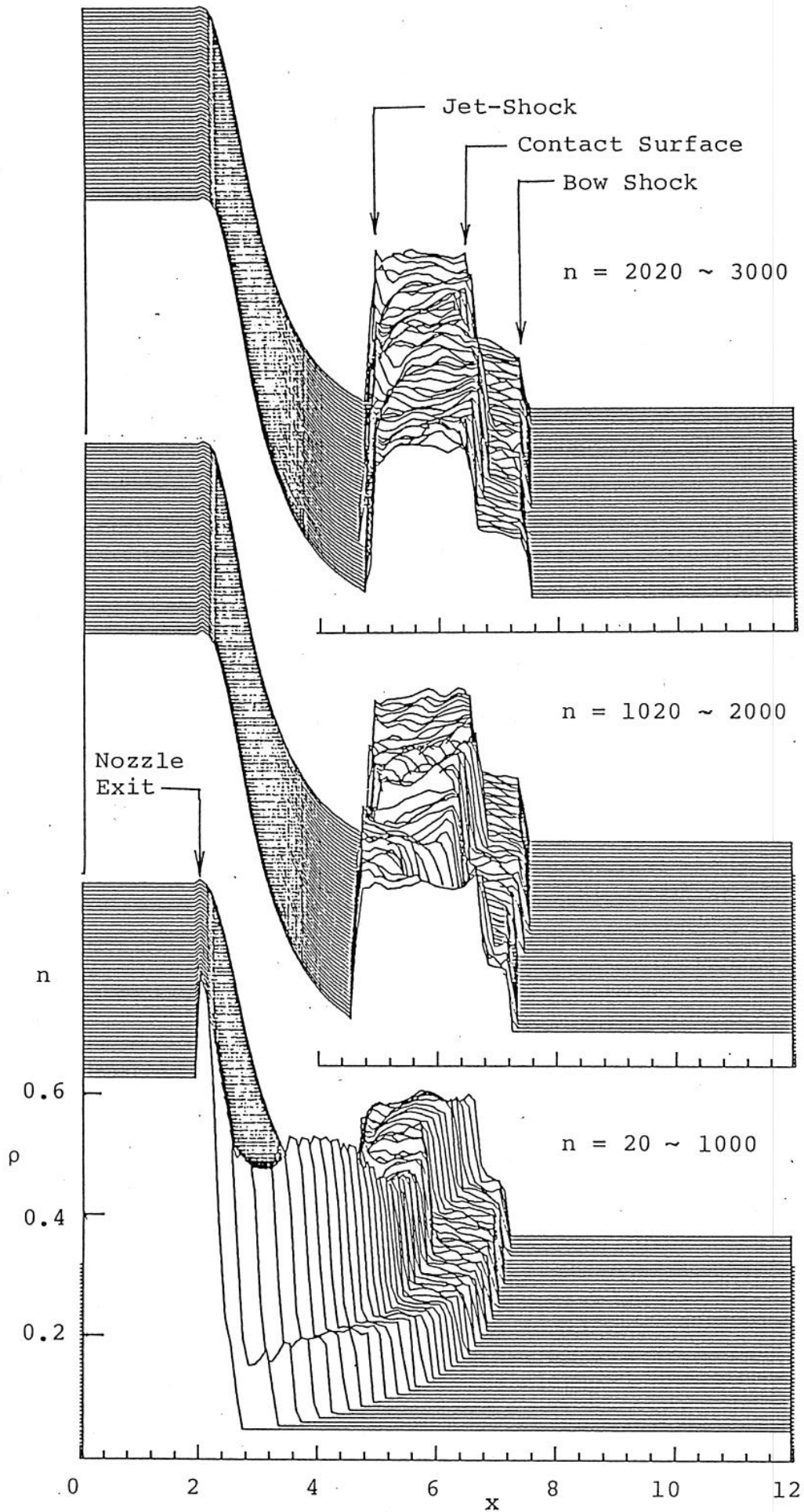


Fig. B-2 -1

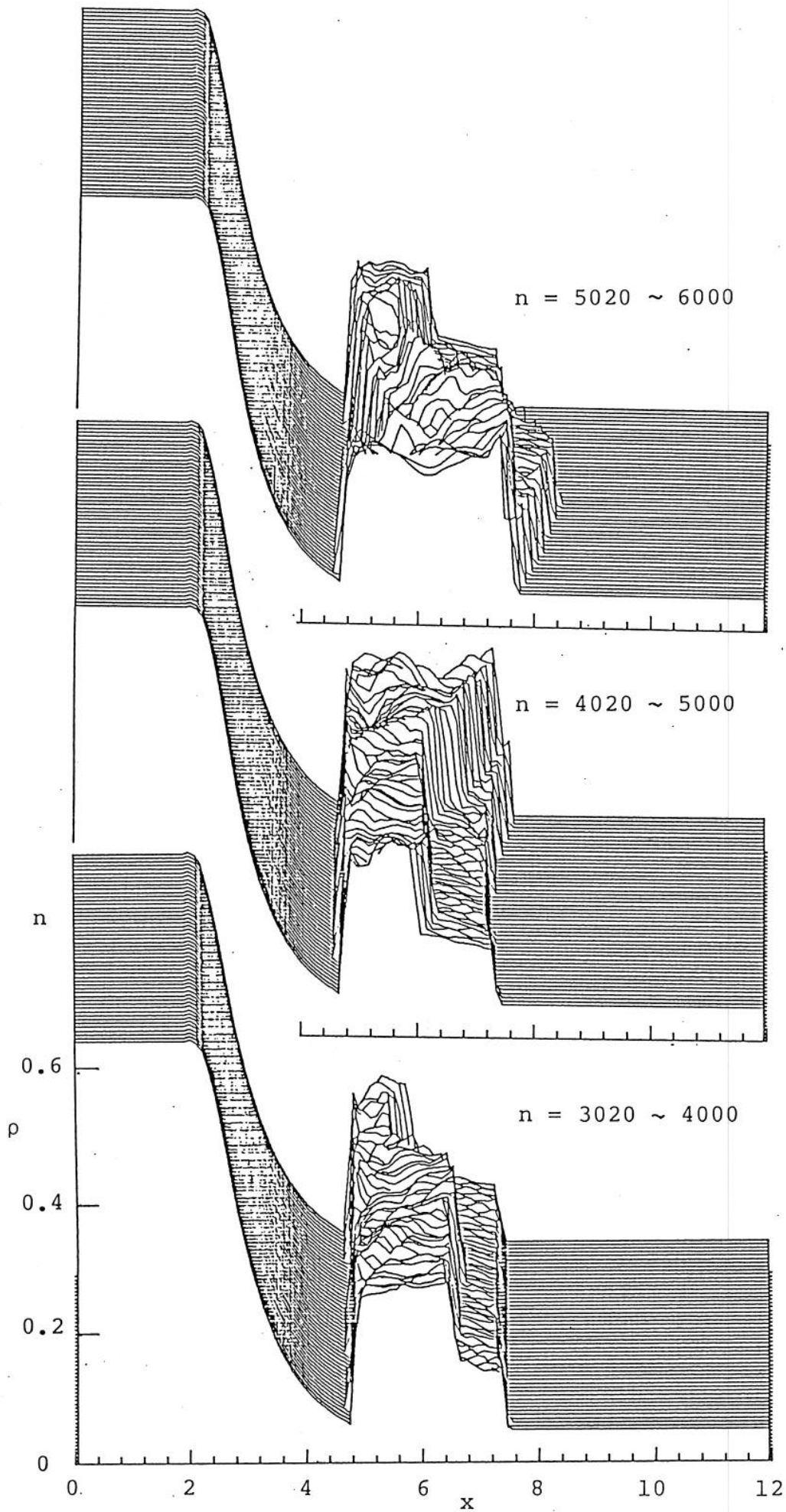


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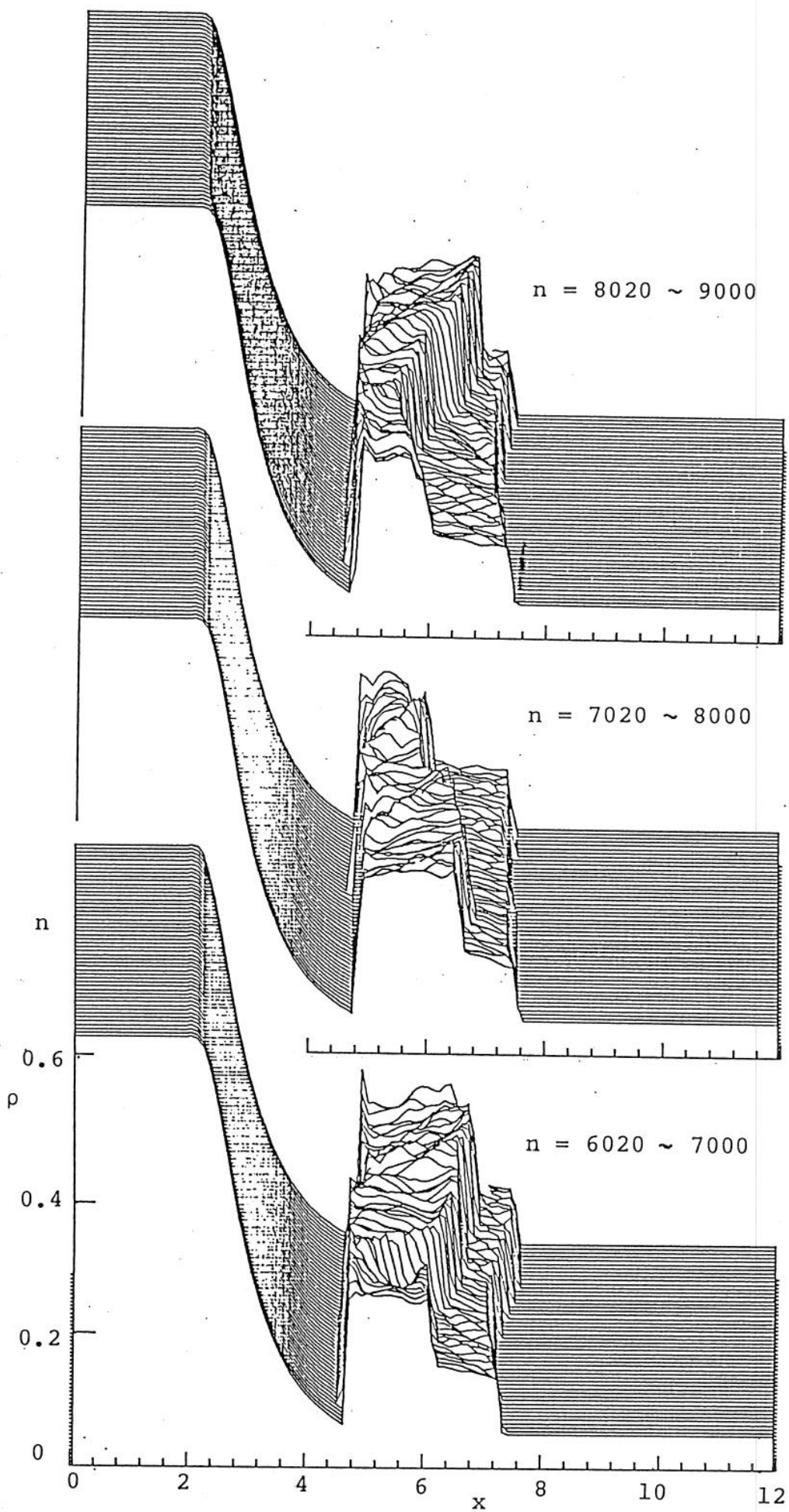


Fig. B-2 -3

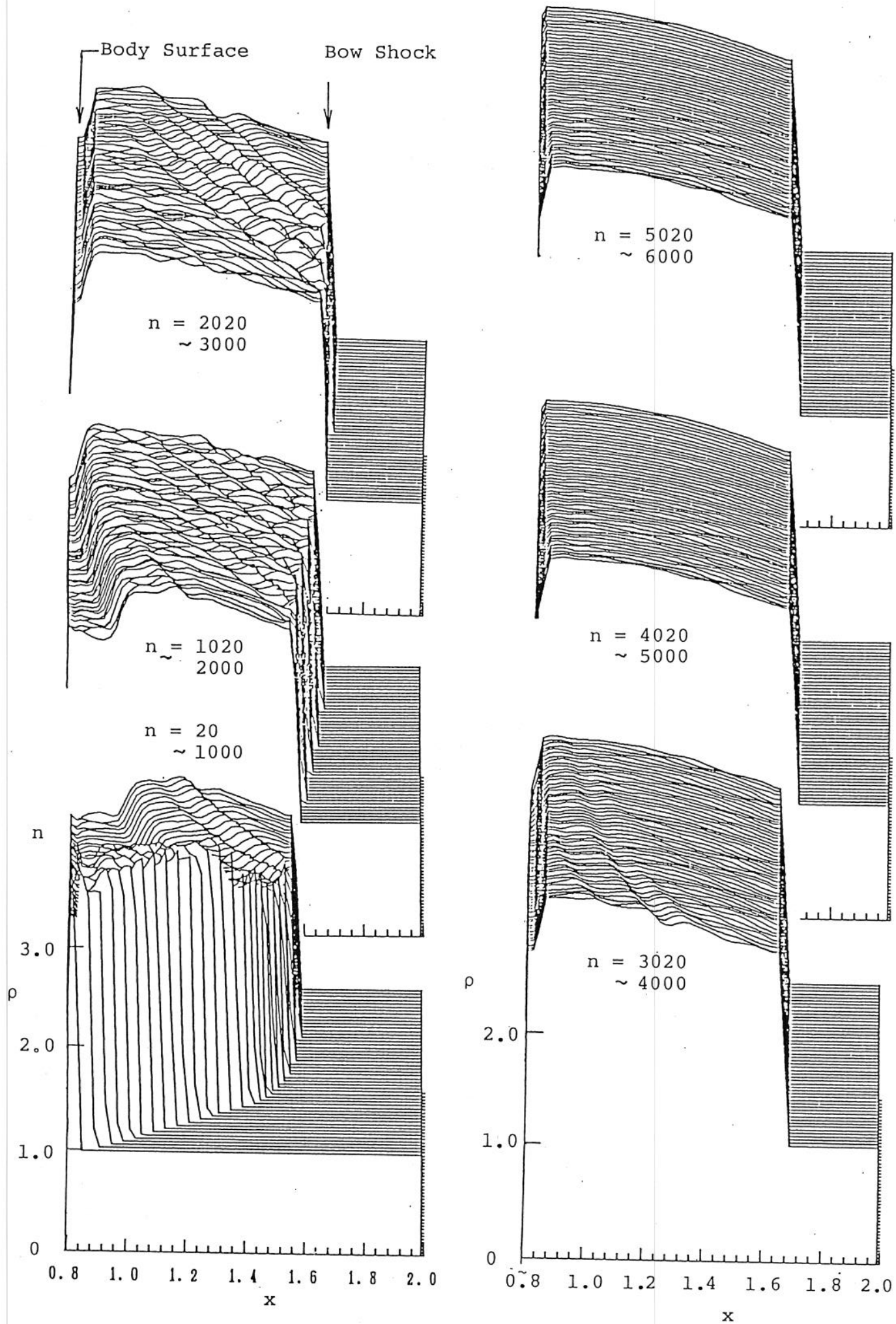


Fig. B-3

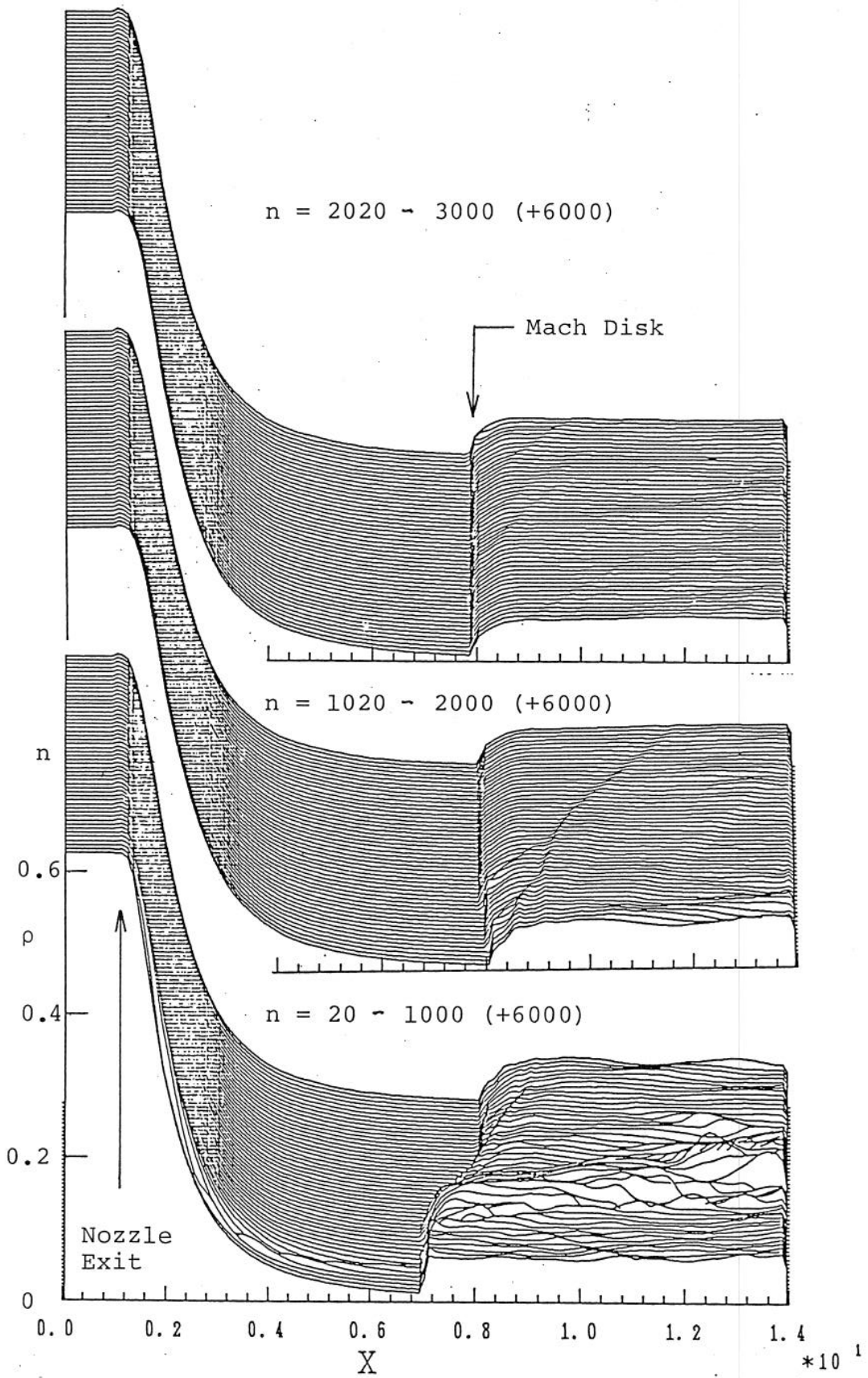


Fig. B-4 - 1

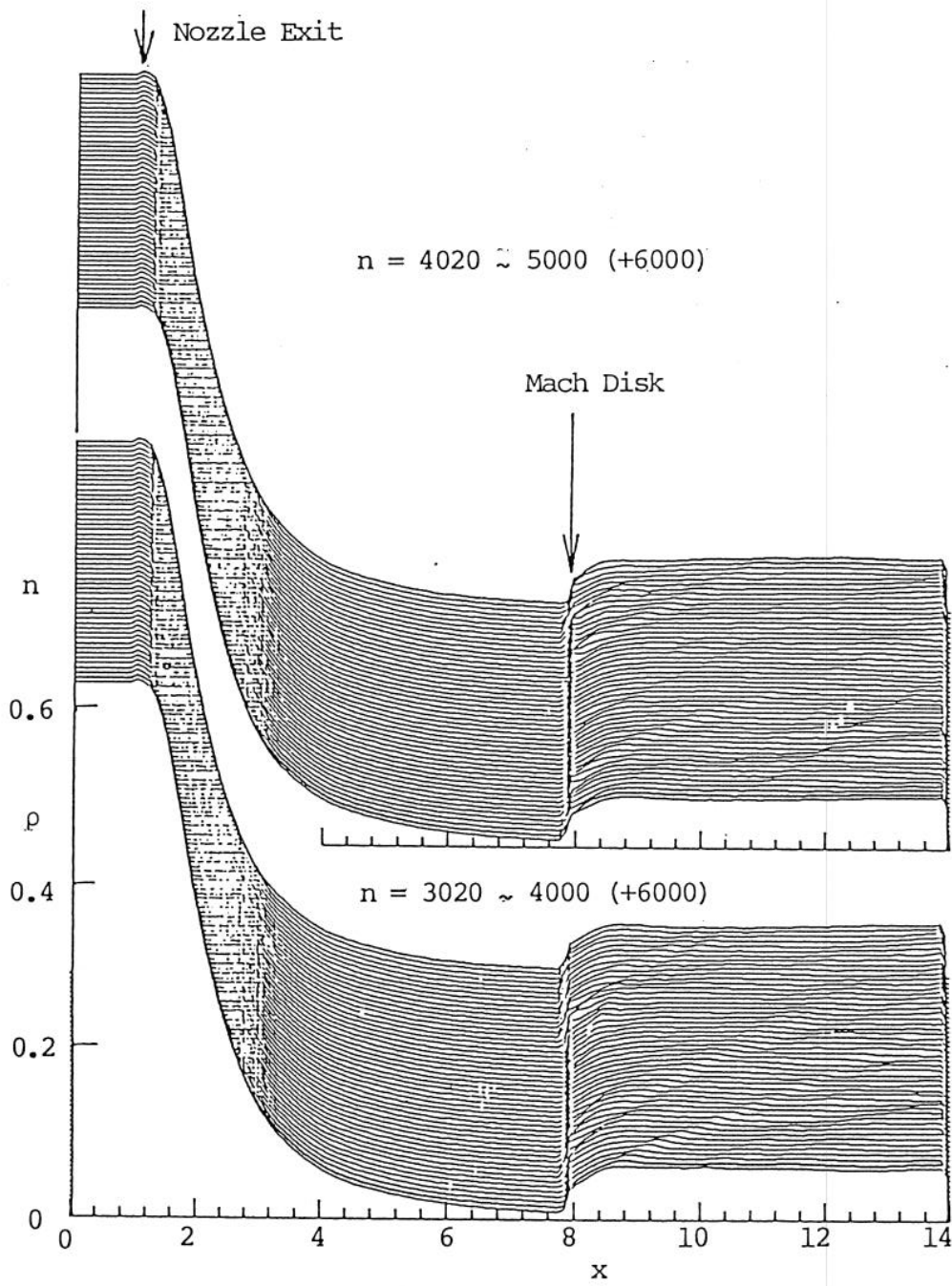


Fig. B-4 -2

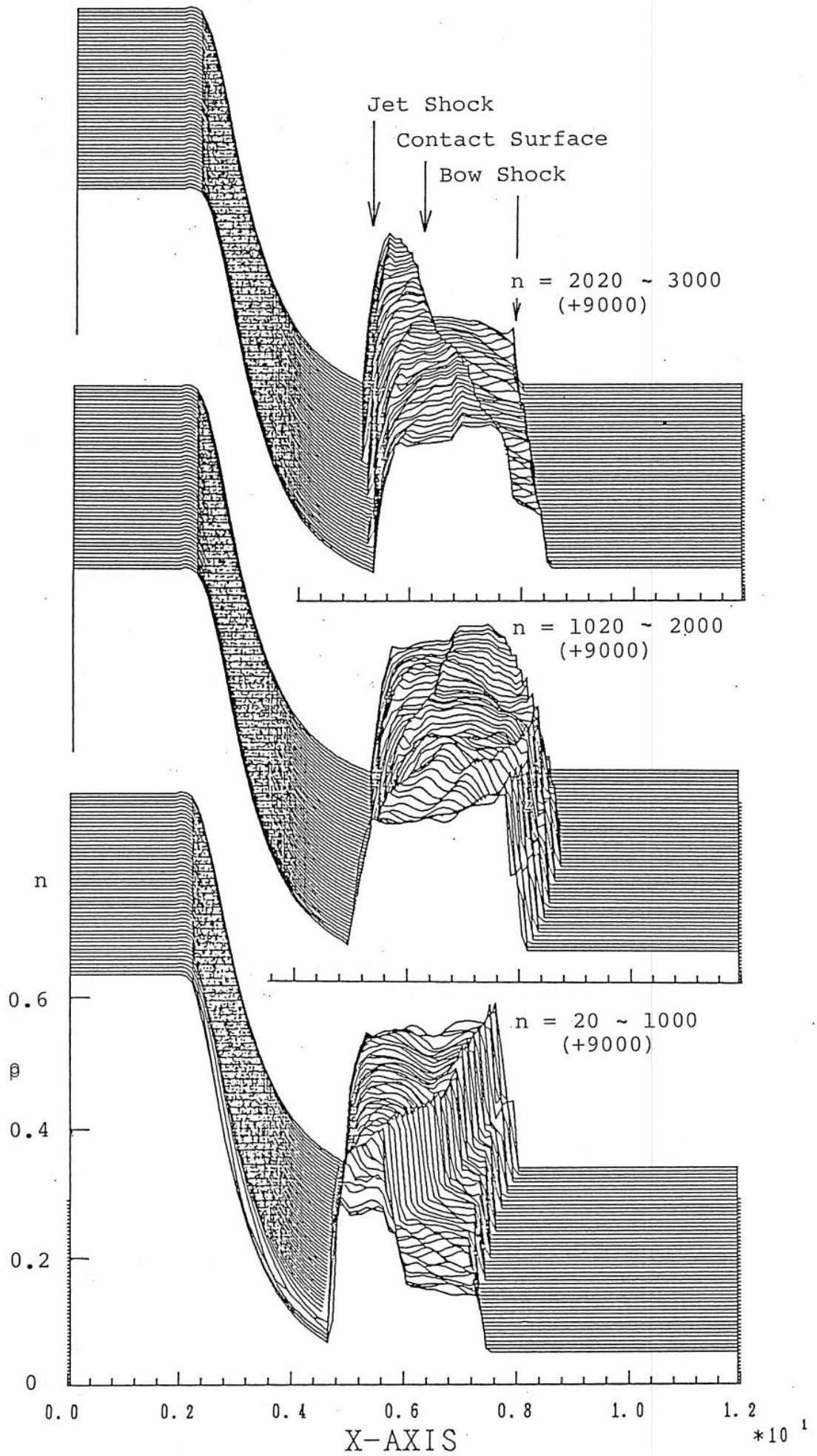


Fig. B-5-1

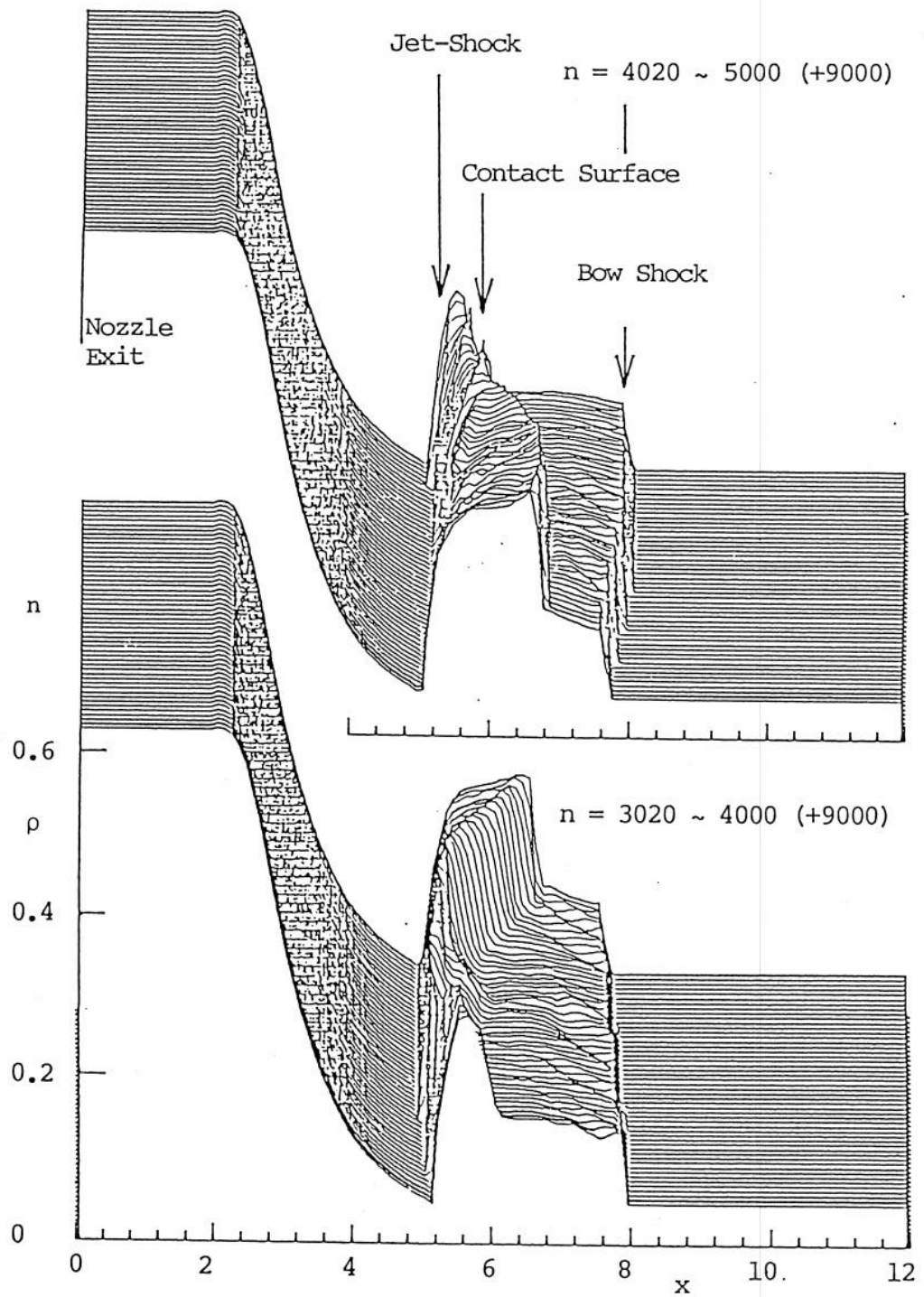


Fig. B-5 - 2

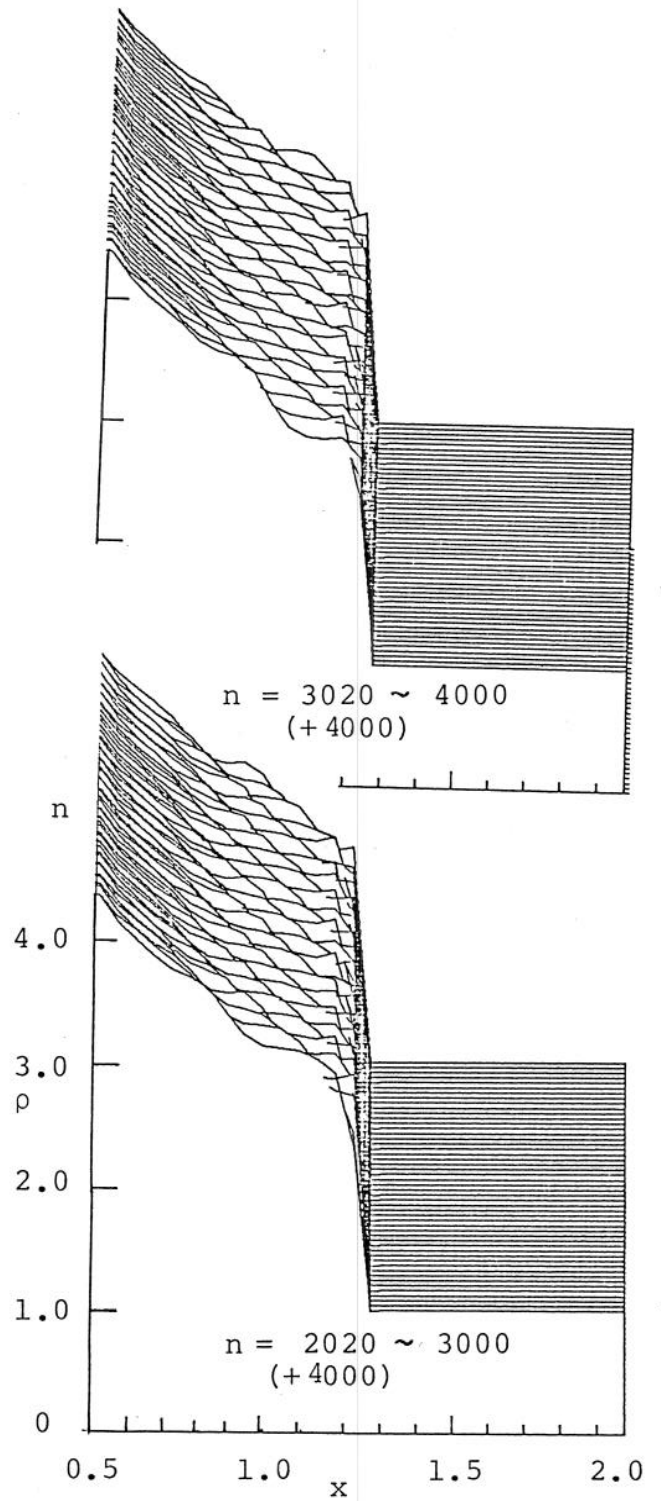
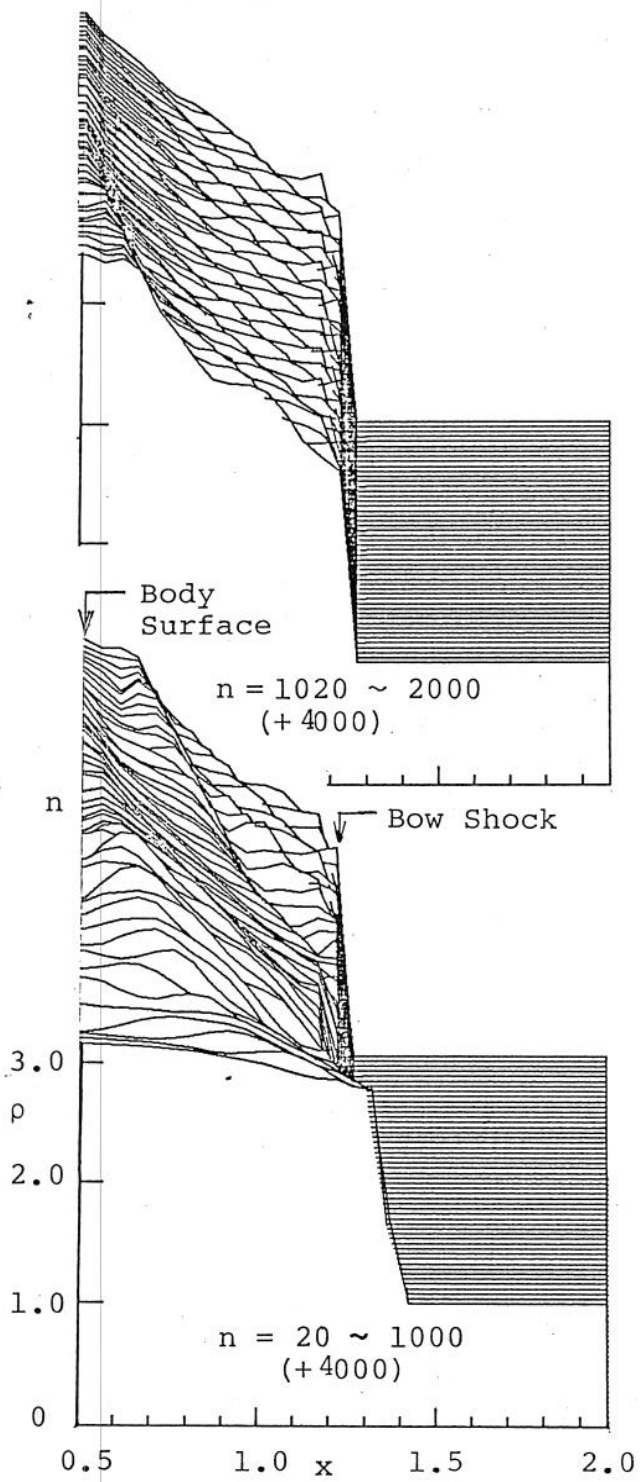


Fig. B-6

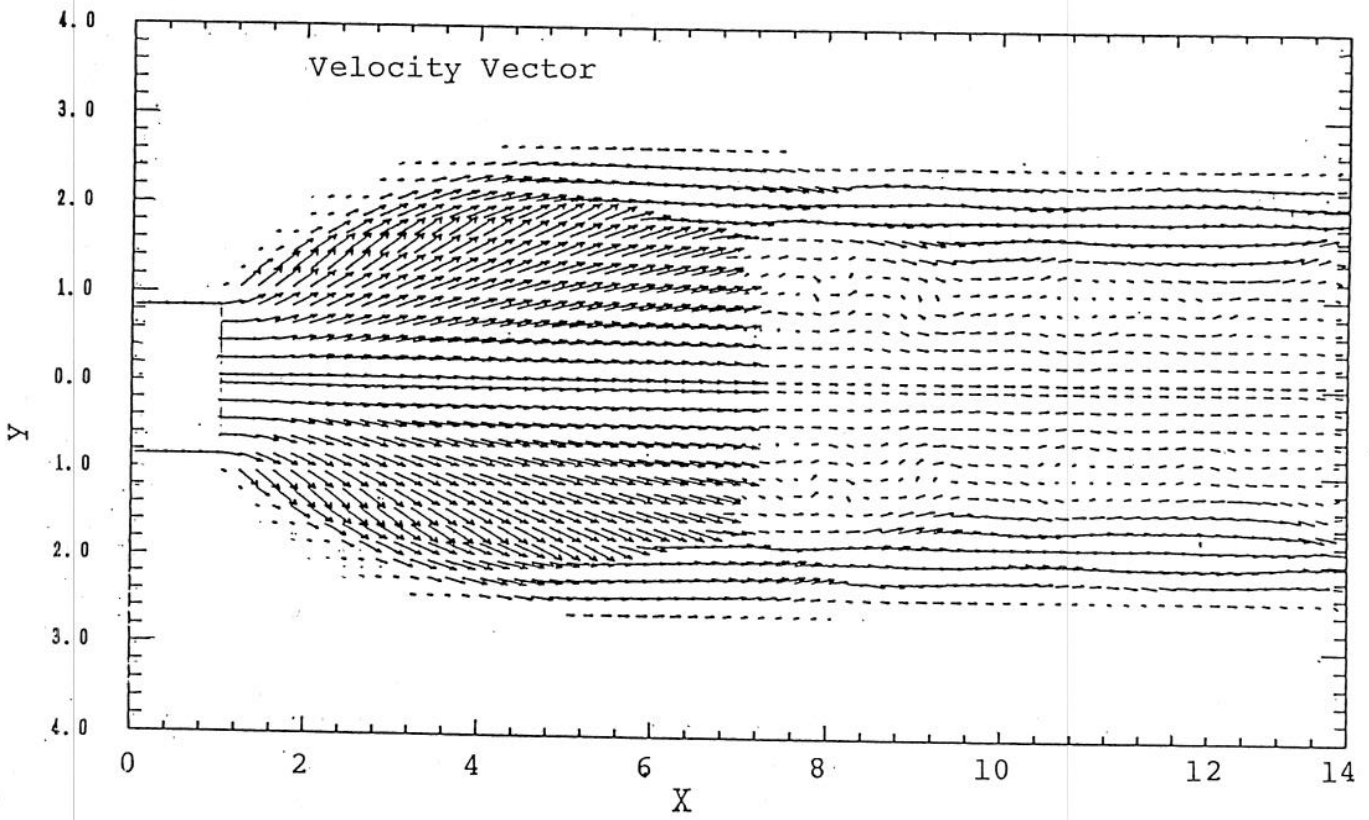
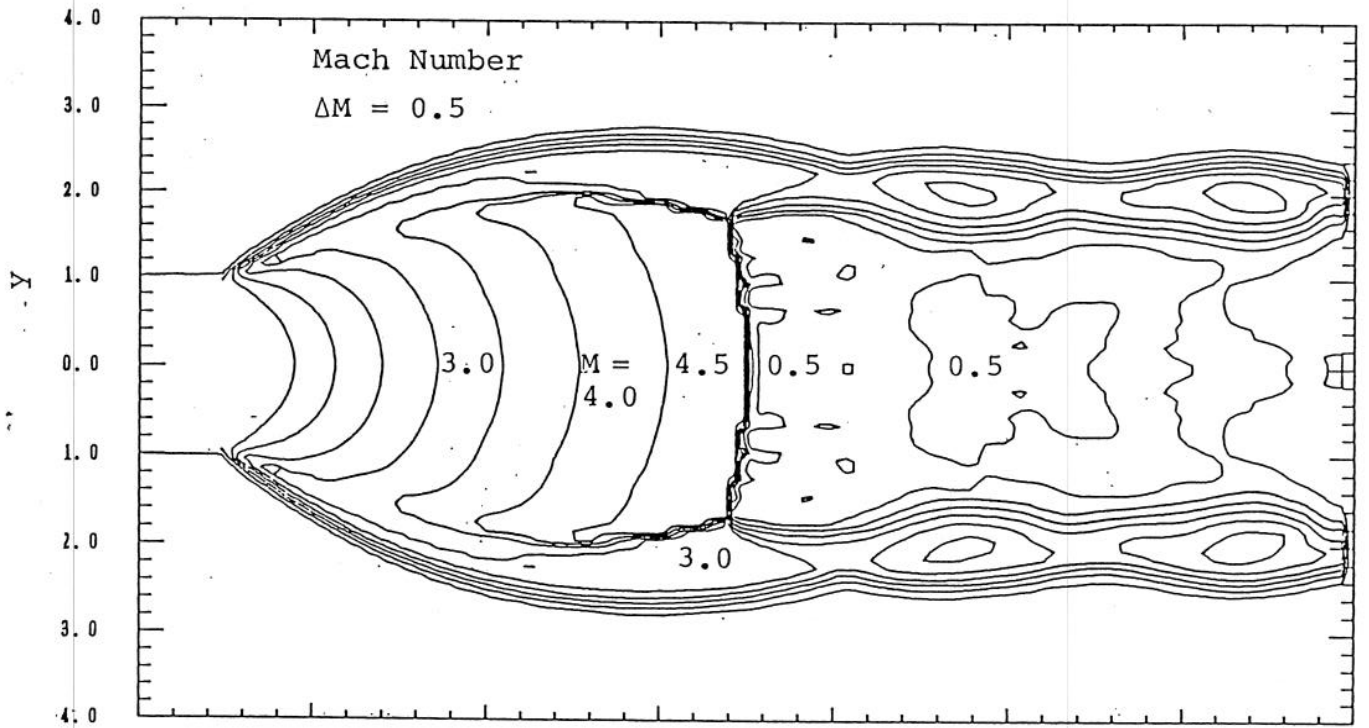


Fig. B-7

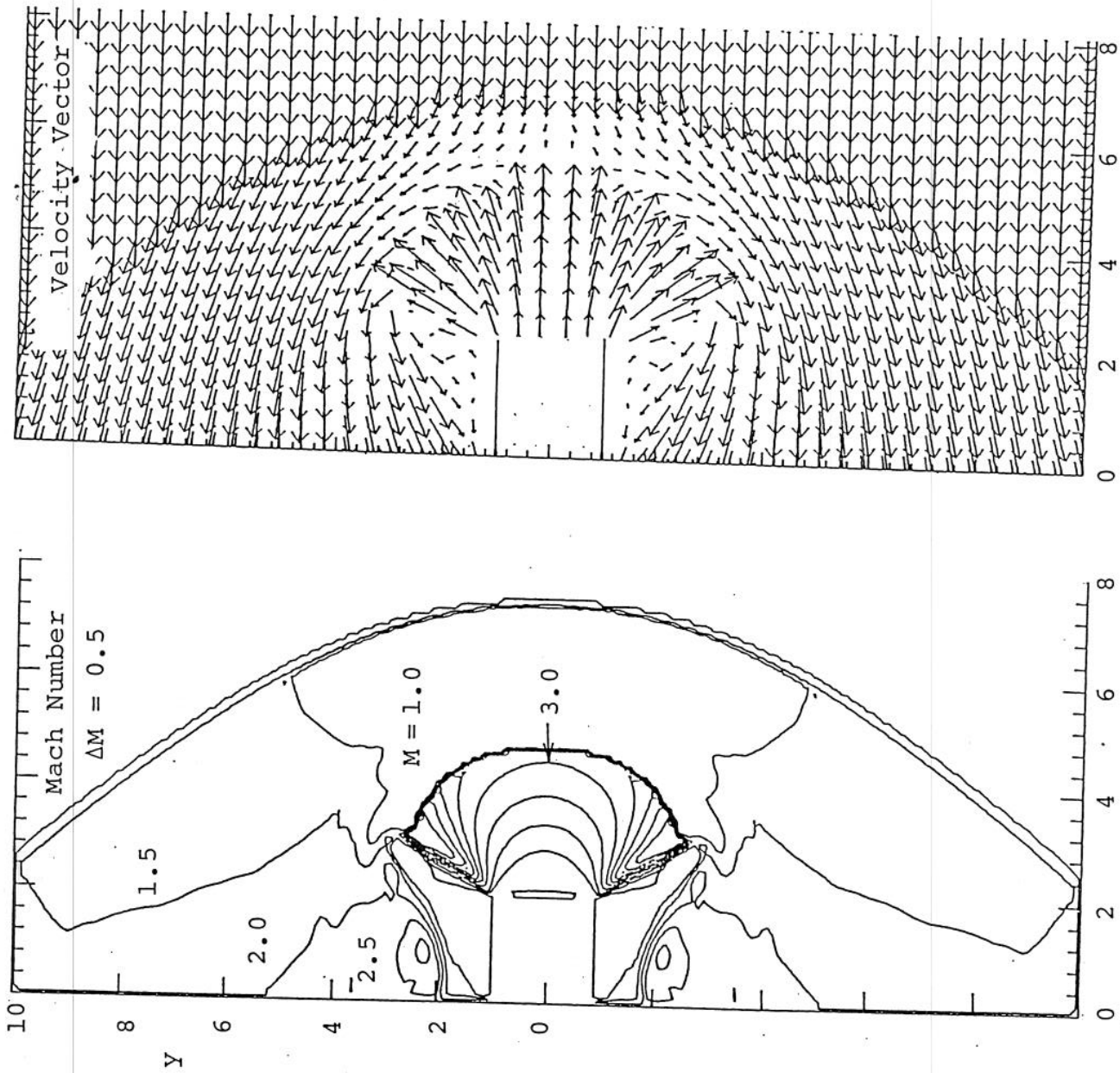


Fig. B-8

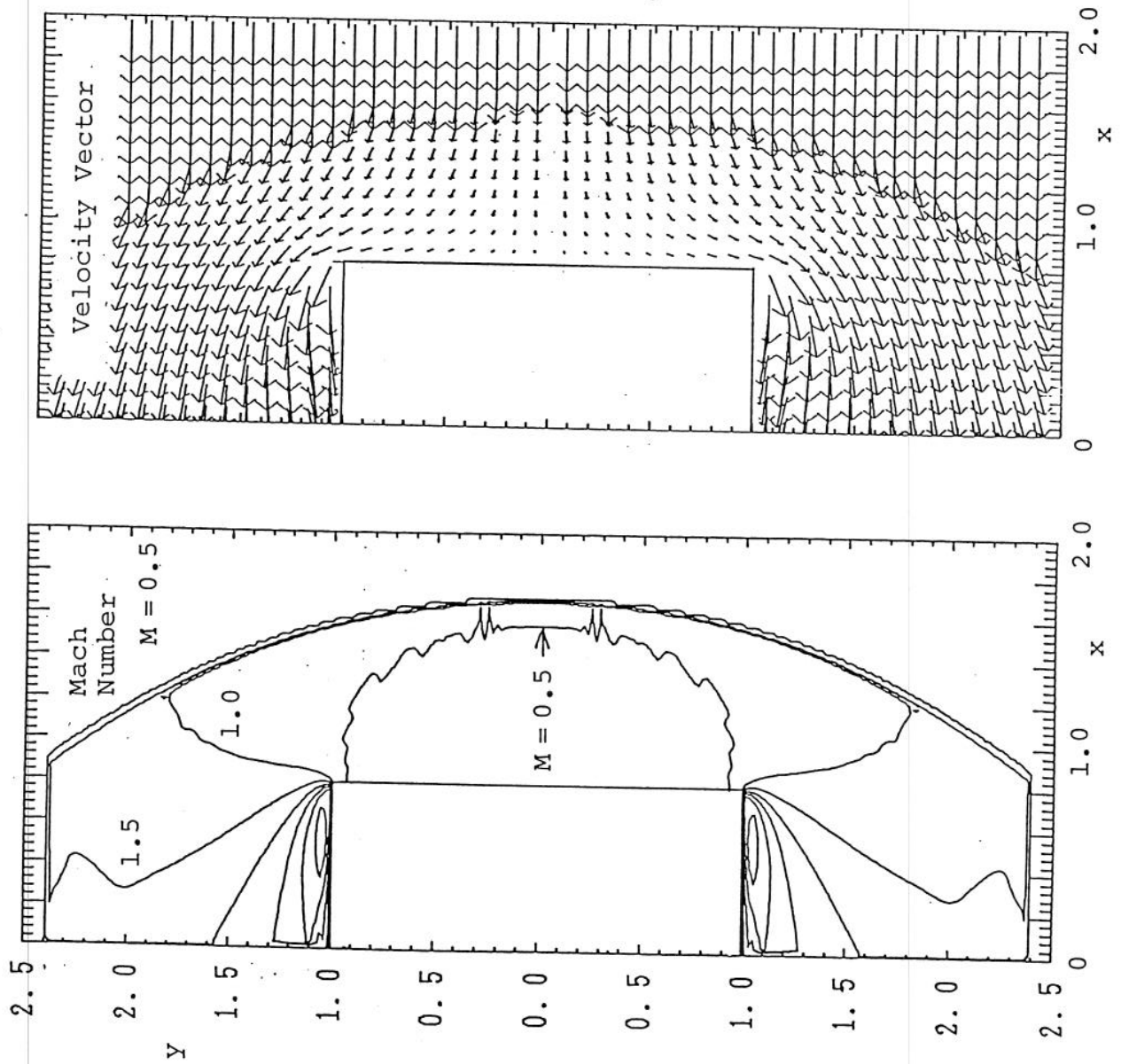


Fig. B-9 -1

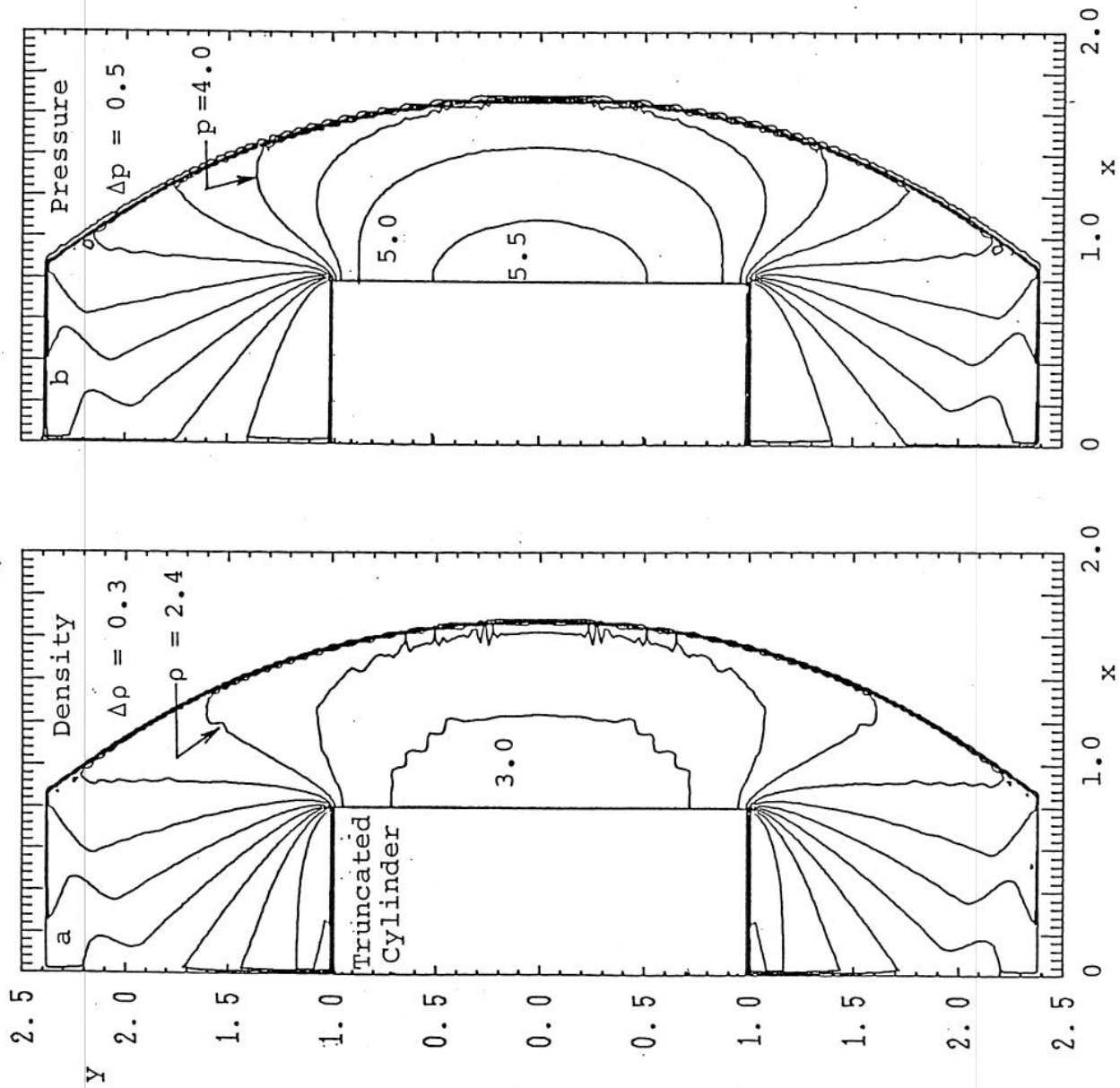


Fig. B-9-2

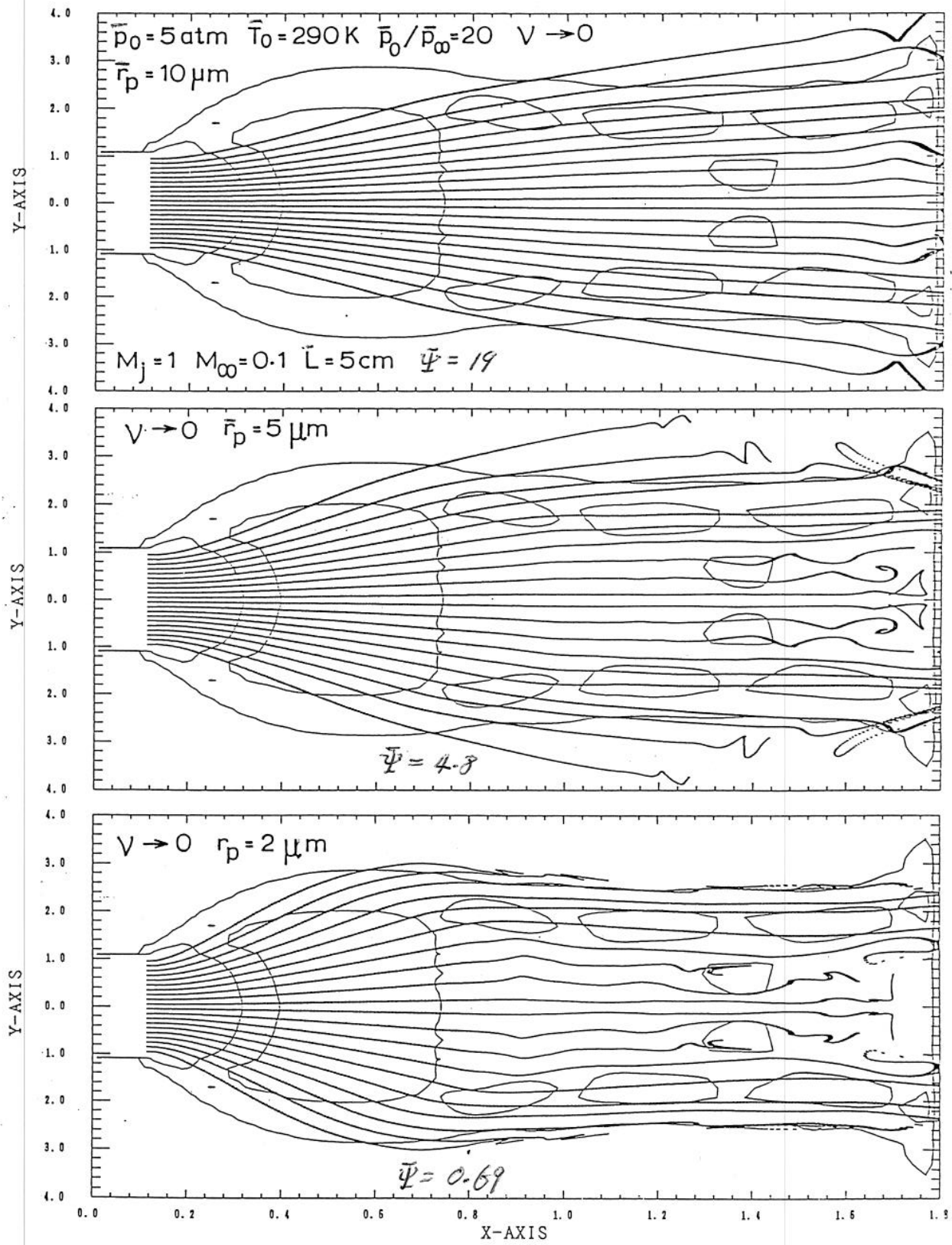


Fig. B-10-1

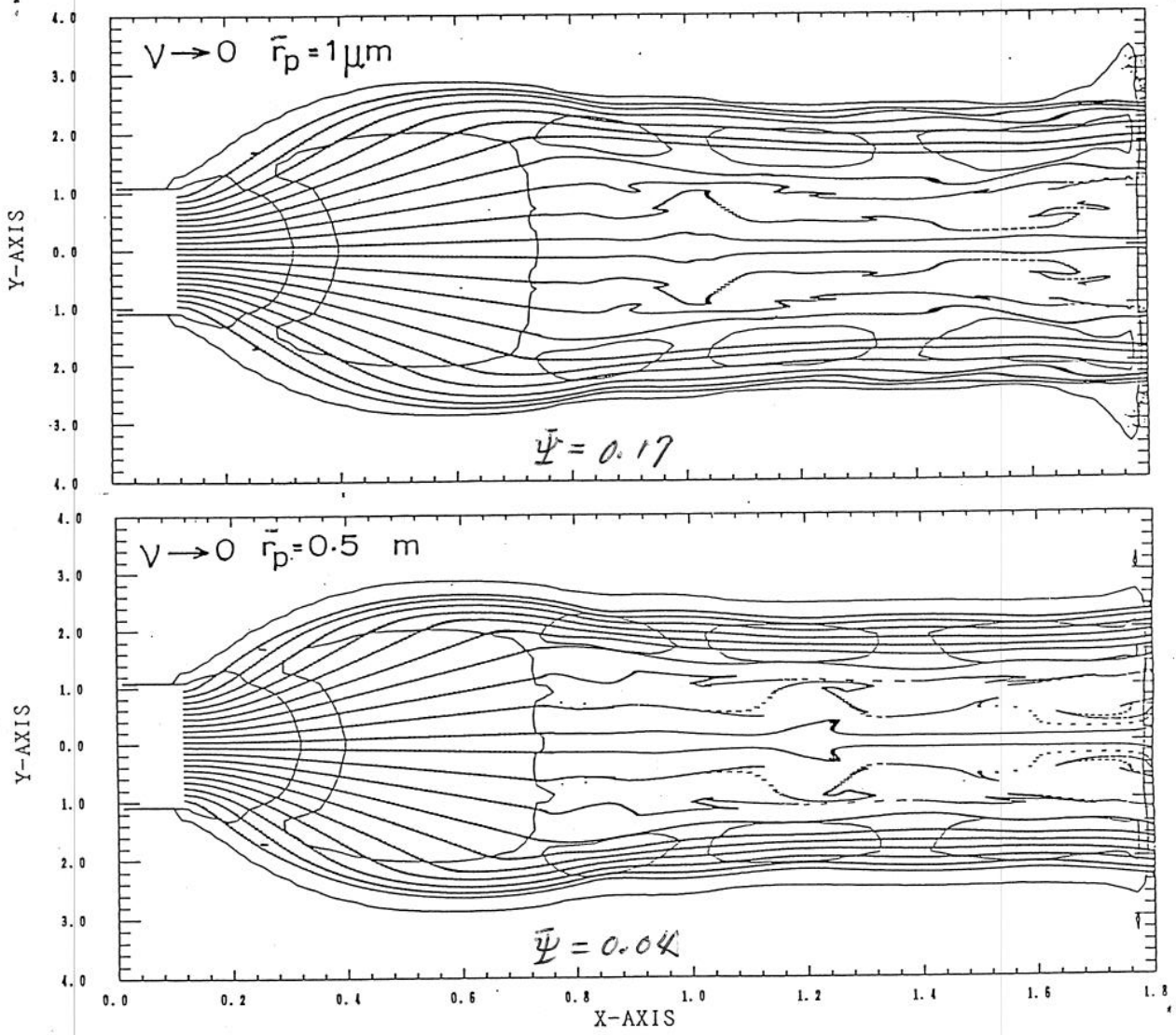


Fig. B-10-2

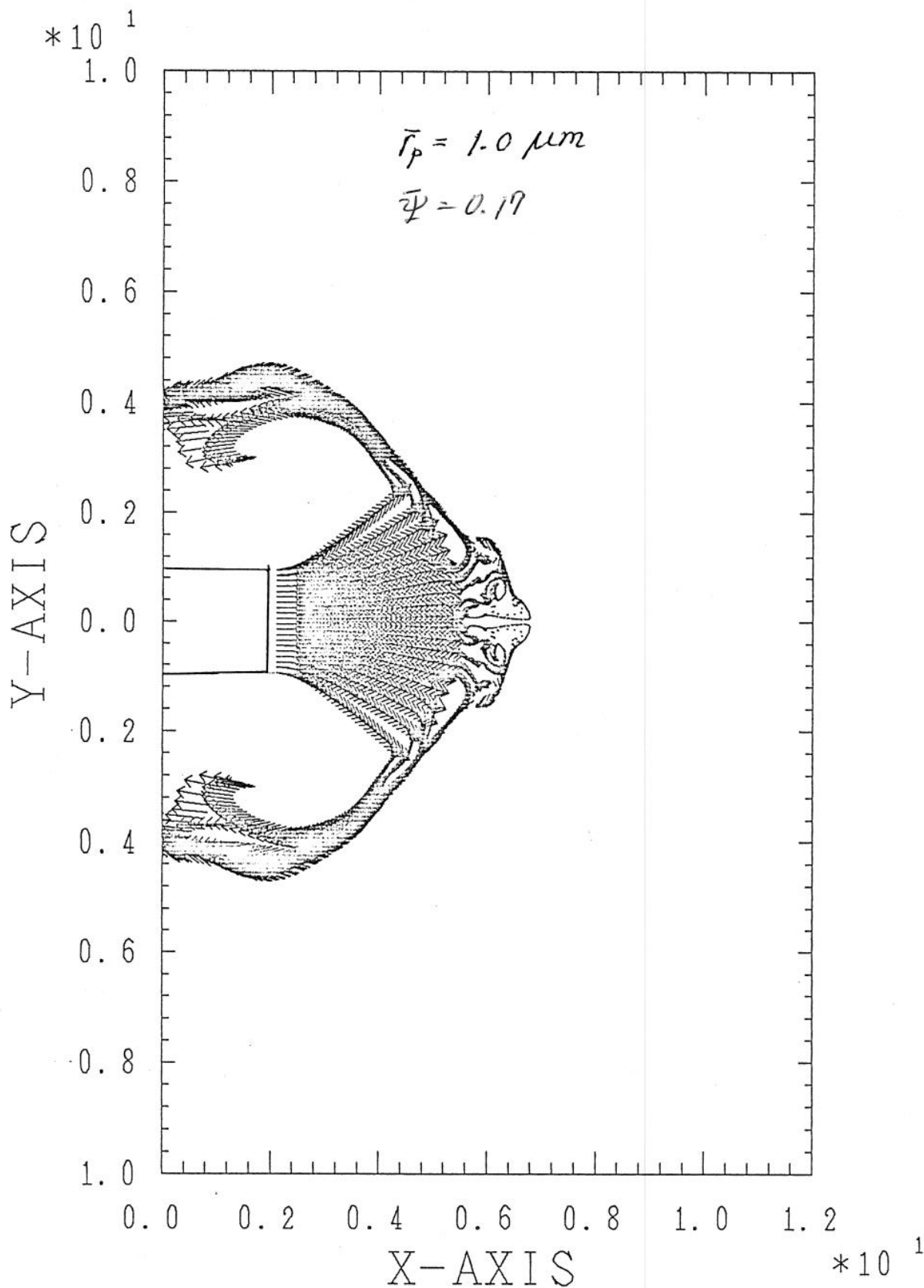


Fig. B-11-1

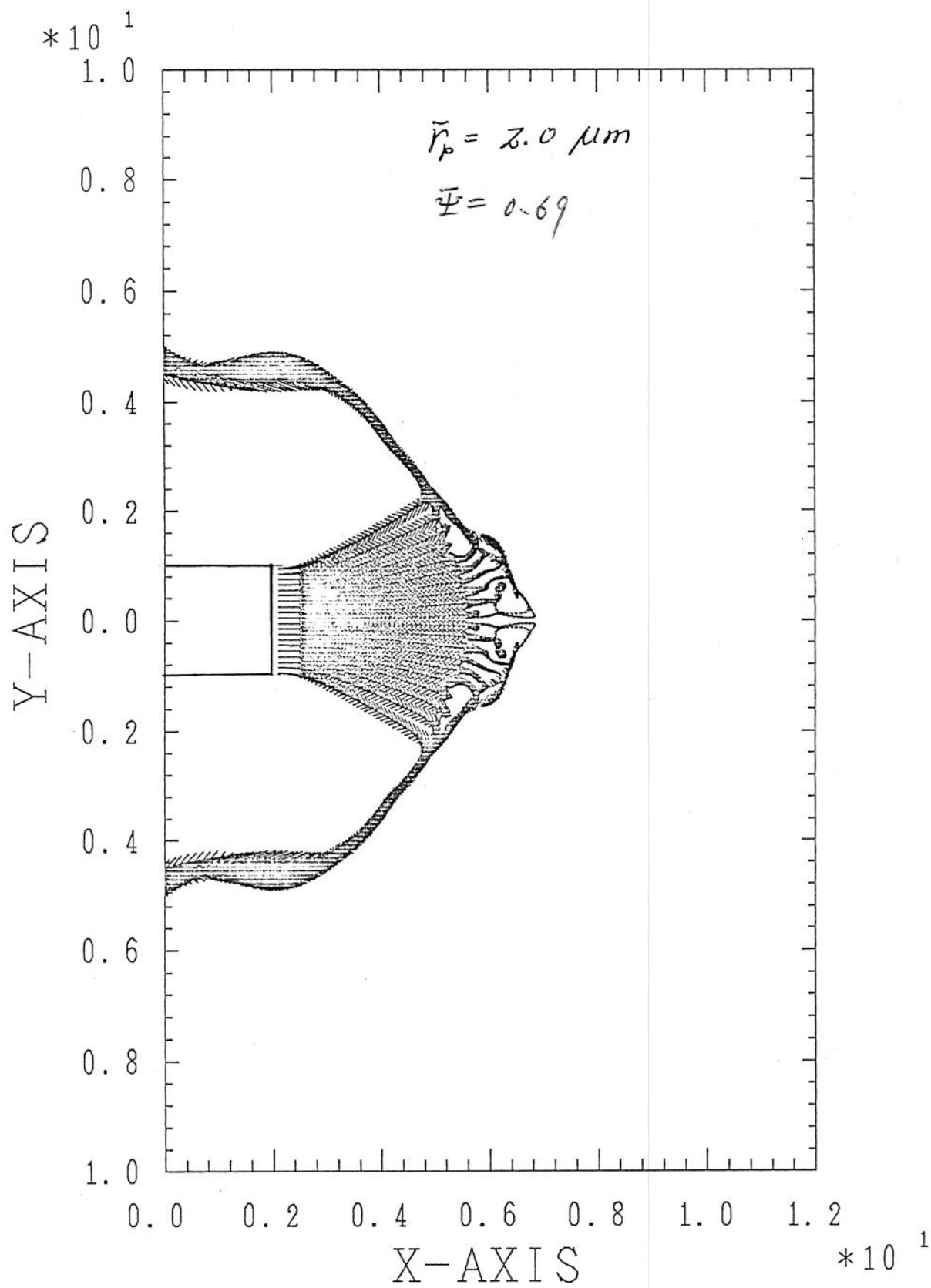


Fig. B-11-2

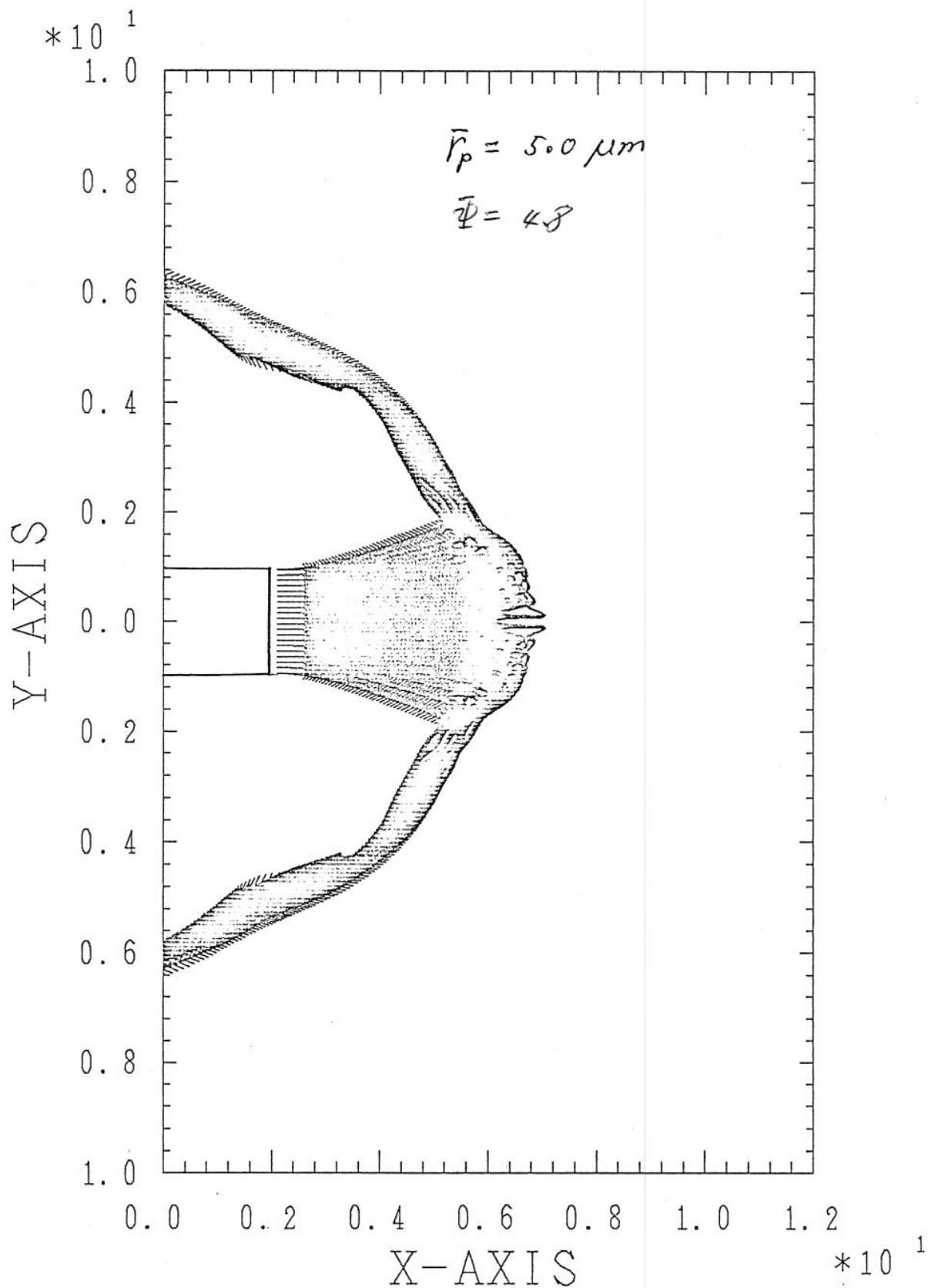


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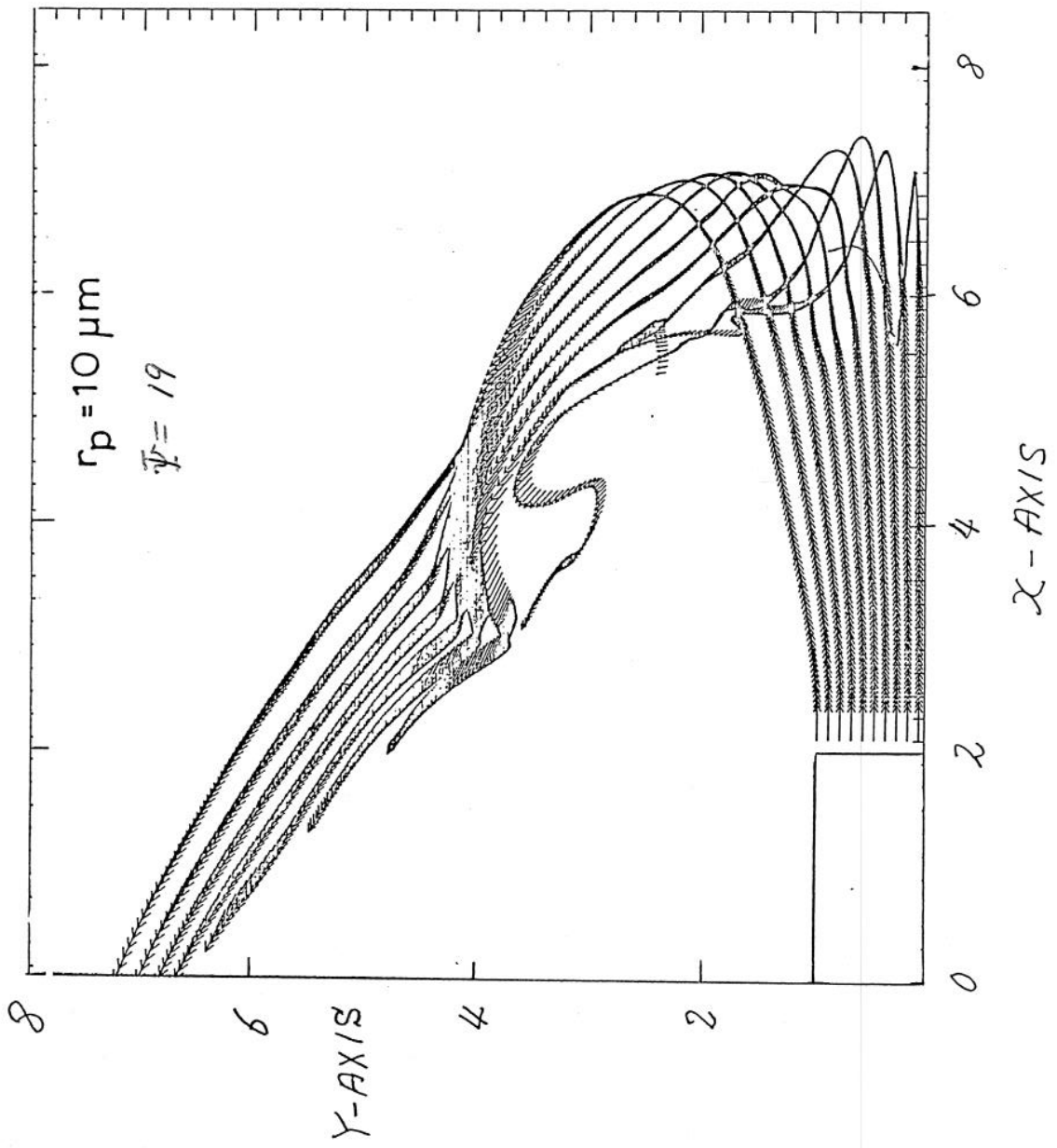


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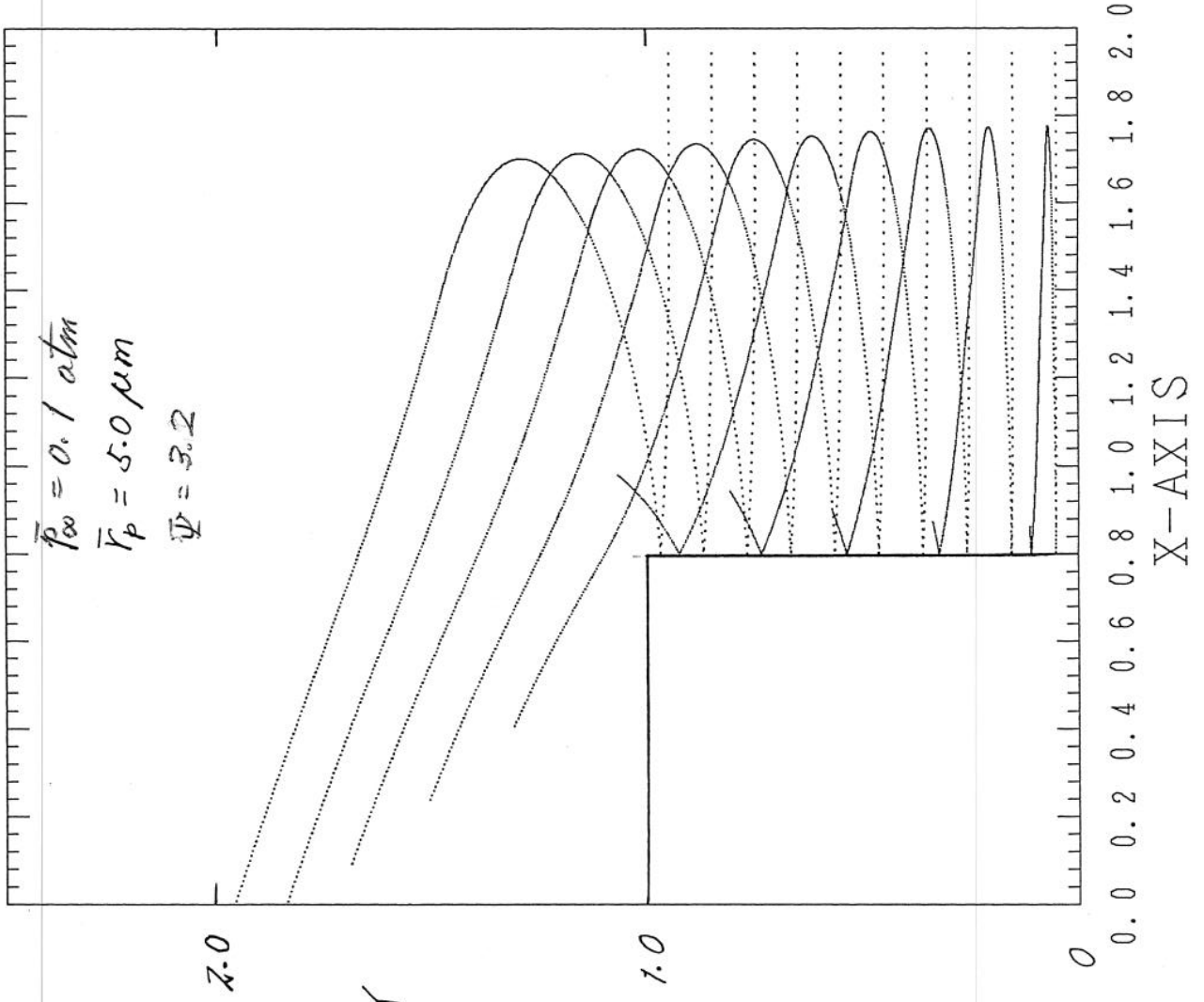


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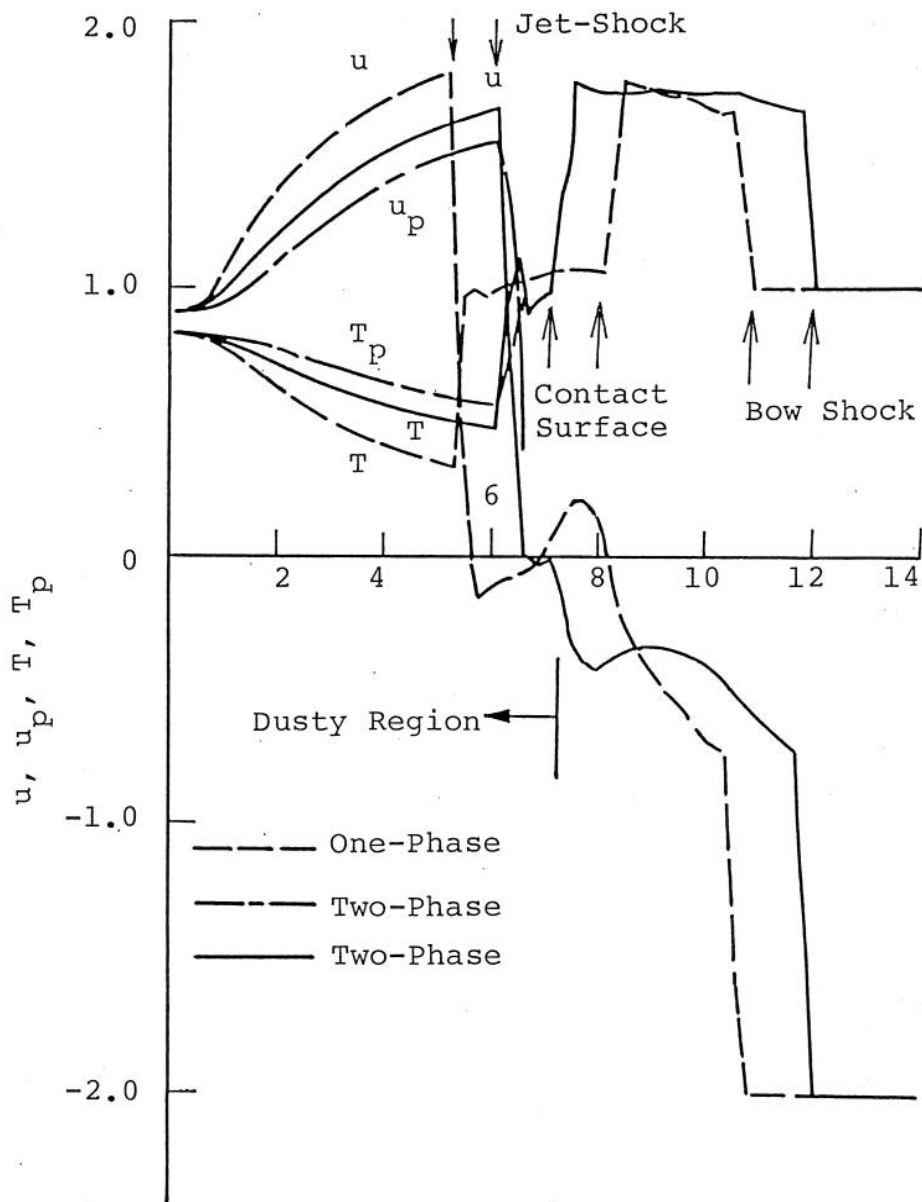
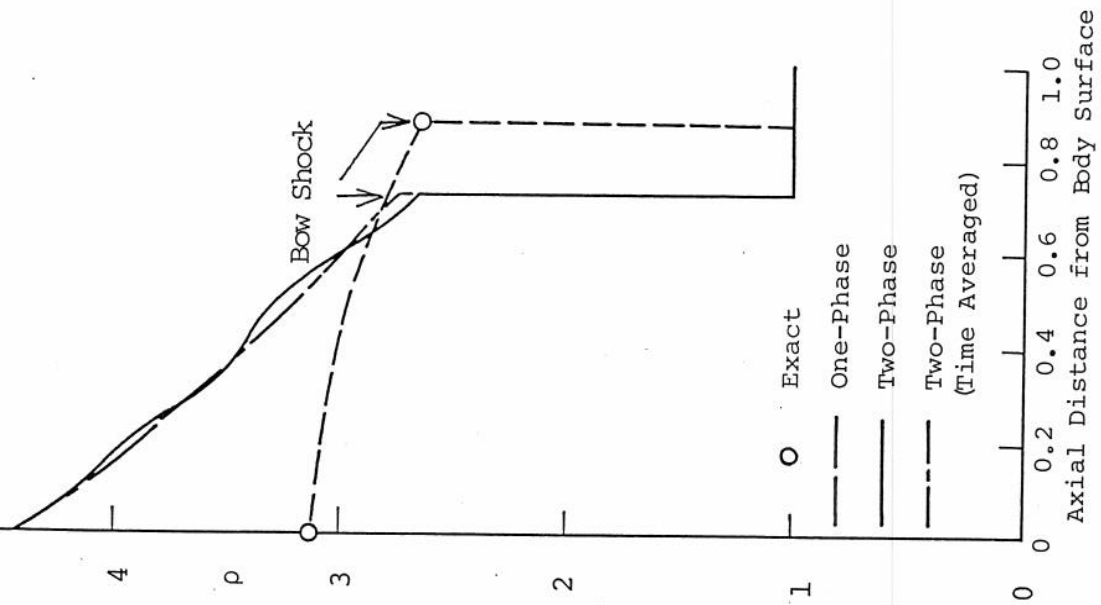


Fig. B-14

a



b

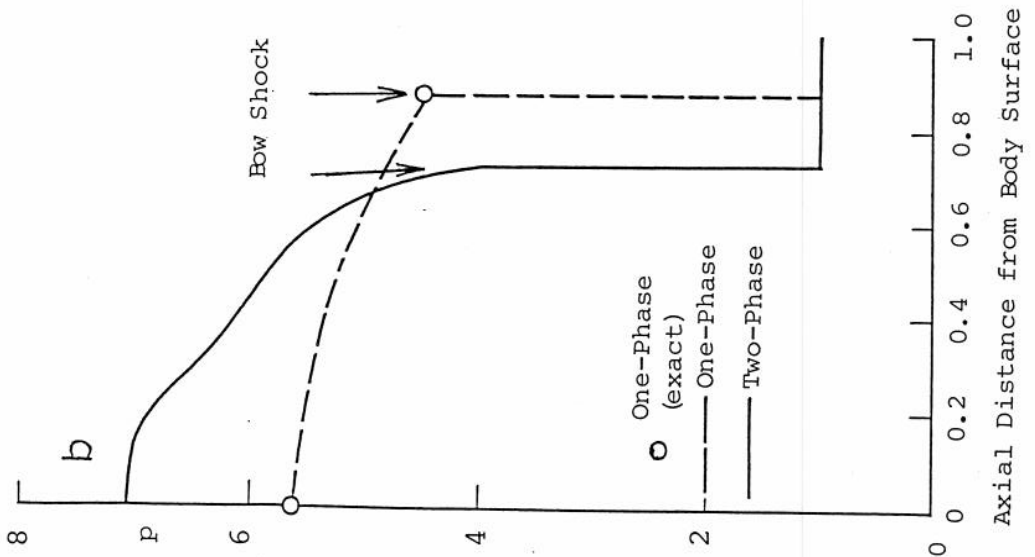


Fig. B-15-1

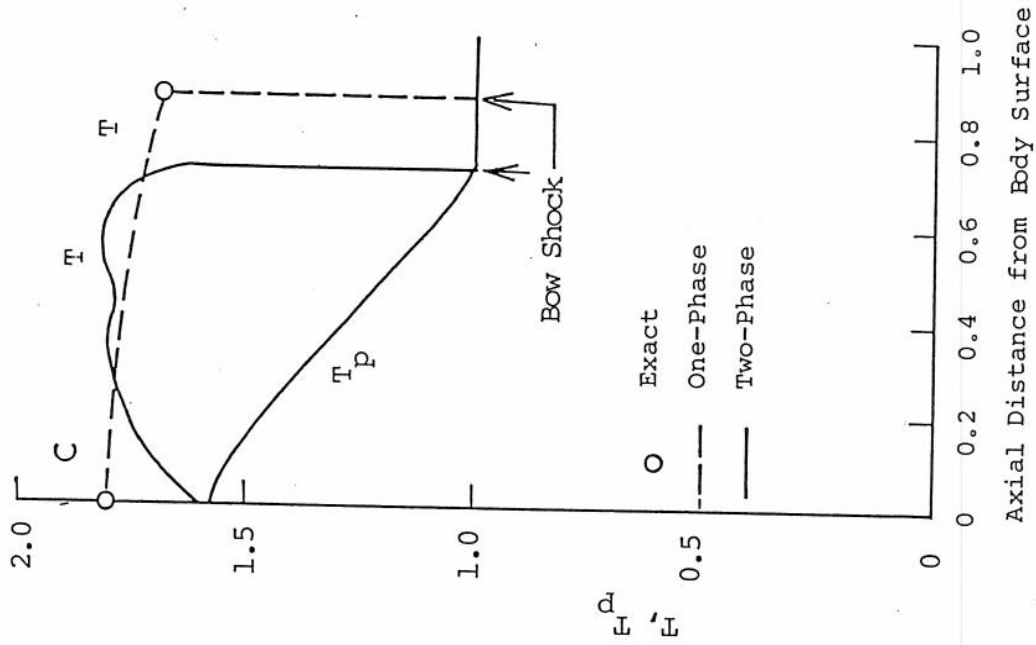
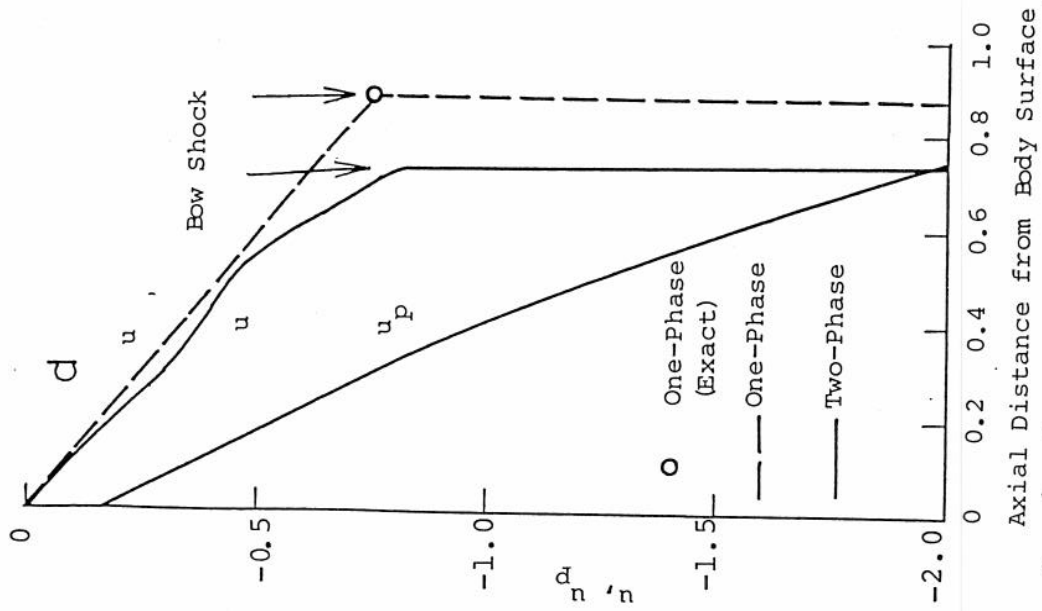


Fig. B-15-2

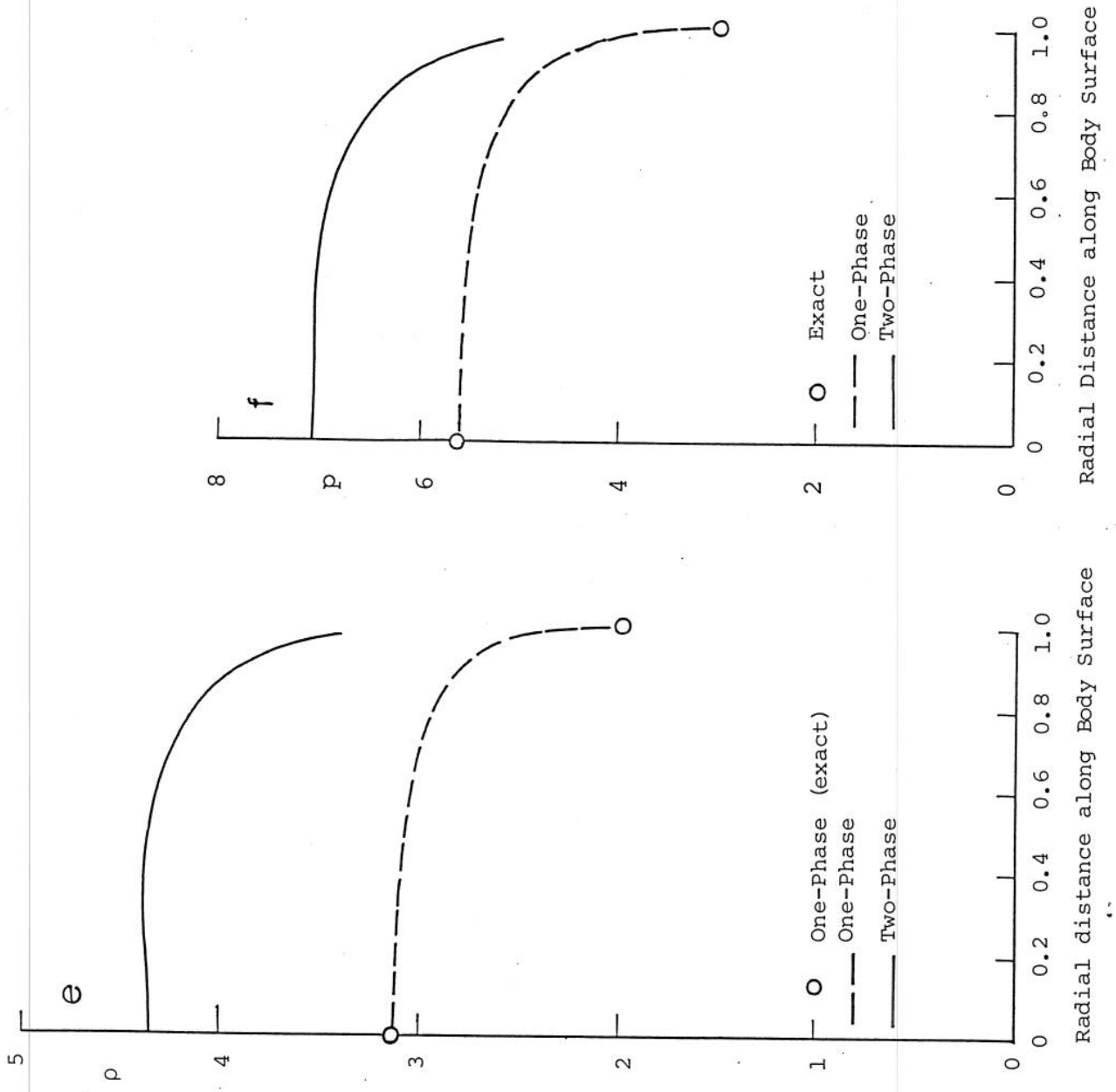


Fig. B-15-3

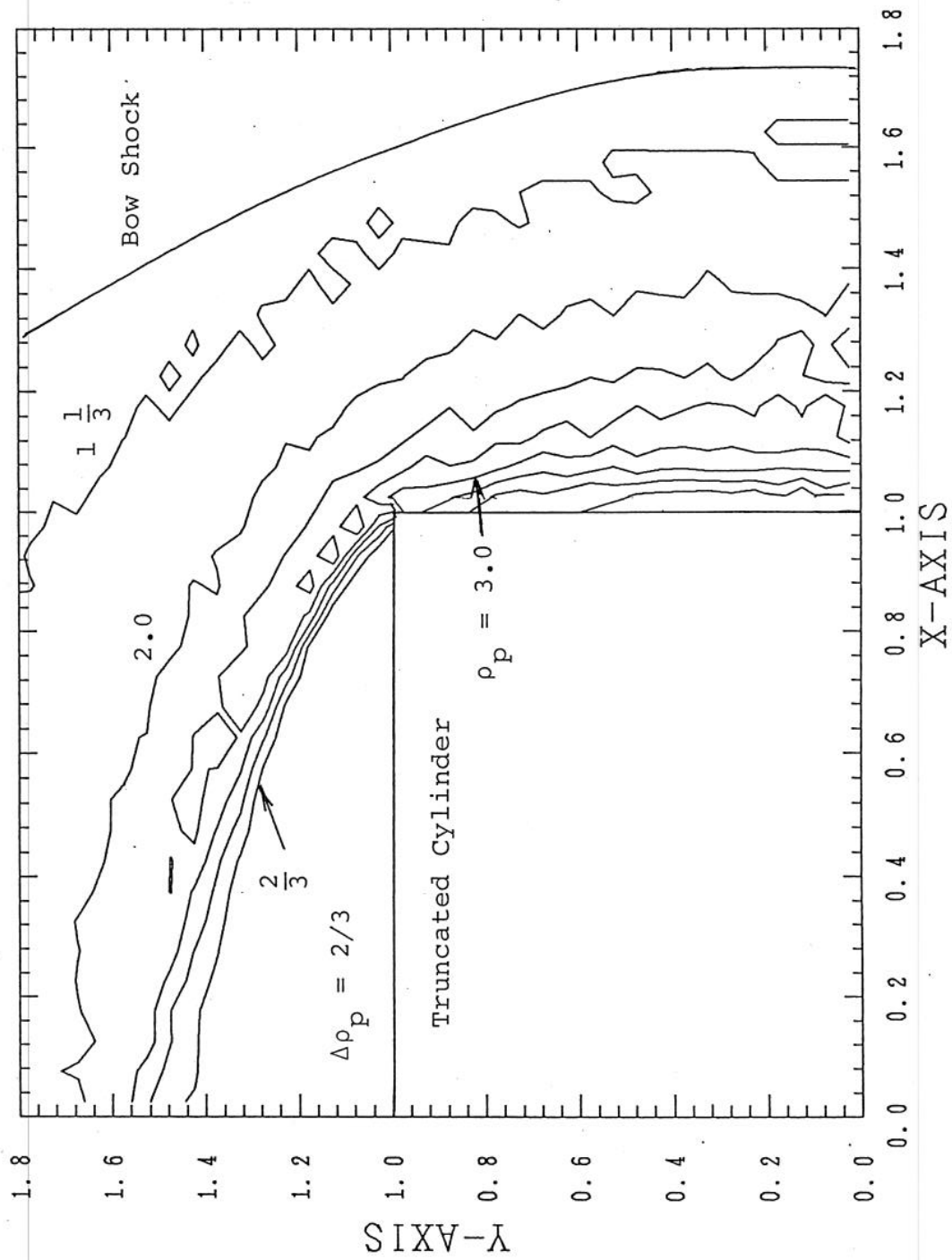


Fig. B-16

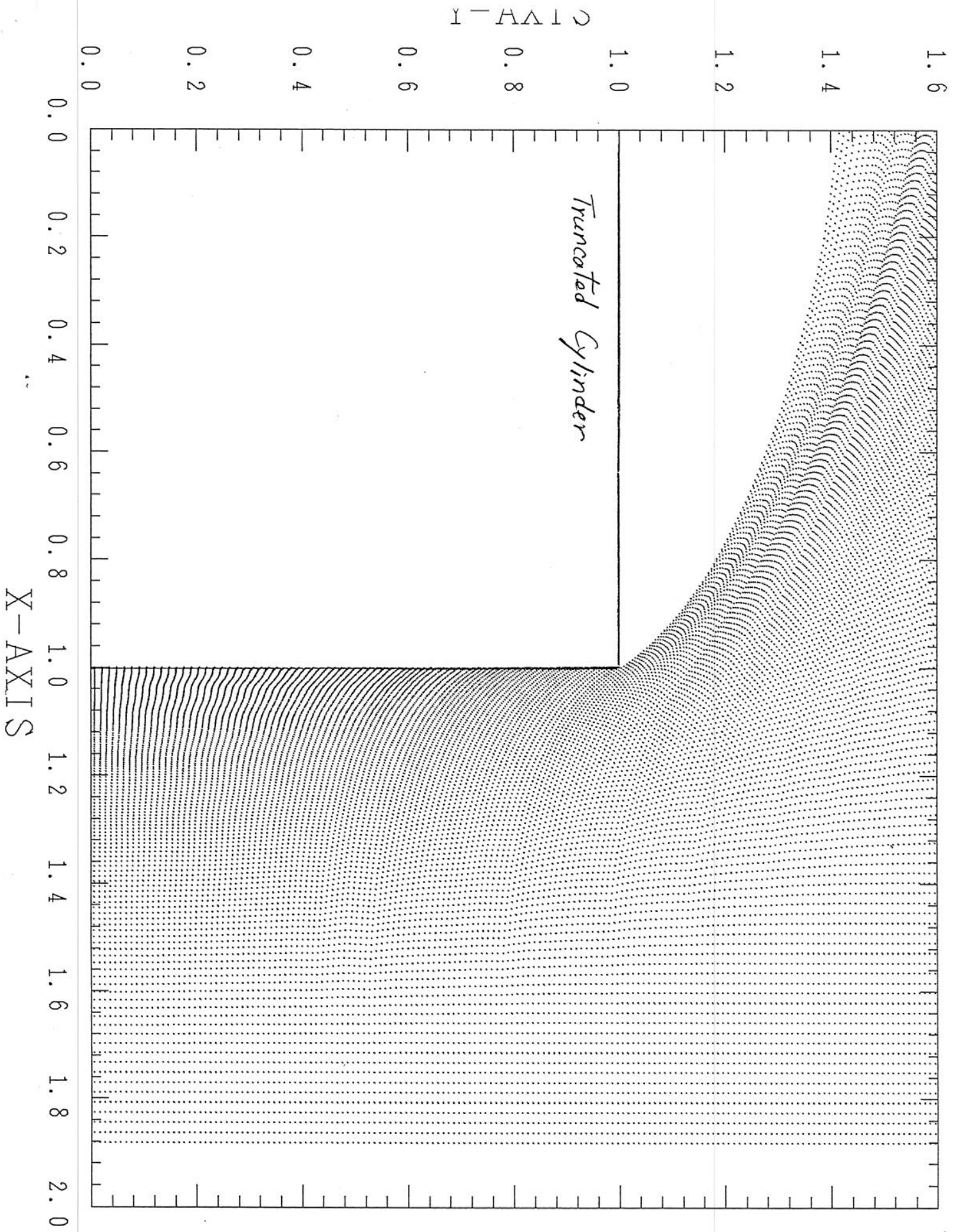


Fig. B-17