

Figure 1: Benchmark: two-dimensional lid driven cavity flow. Horizontal and vertical velocity components along the vertical and horizontal centrelines, respectively. Lines: our lattice Boltzmann code with periodic boundaries in the $z$-direction. Markers: data from Ghia et al. (1982). Reynolds number $R e_{\mathrm{w}}$ defined from lid velocity and cavity height.

## Benchmark for the lattice Boltzmann code

The lid-driven cavity flow has been adopted as a benchmark case for the lattice Boltzmann code used for the simulations in this paper. This problem consists of a quadratic or cubic flow domain with walls on all sides, where the upper wall (orthogonal to the $y$-direction) moves in the positive $x$-direction, driving the flow within the cavity. Figure 1 shows the horizontal and vertical velocity components along the vertical and horizontal centrelines, respectively. Markers indicate the reference solution, computed by Ghia et al. (1982). This is a twodimensional problem solved with our three-dimensional lattice Boltzmann code by adopting periodic boundaries to the third dimension. Simulations have for verification been repeated permuted axis orientations. The result of a threedimensional cavity simulation is presented in table 1, listing the location of the main vortex centre (stagnation point) in various $x y$-planes. Reference values for a finite volume and a finite difference scheme is taken from Kristoffersen \& Andersson (1989). Reference simulations contain a restricted number of grid points, but our intention here is to demonstrate consistency.

## References

Ghia, U., Ghia, K. N. \& Shin, C. T. 1982 High-re solutions for incompressible flow using the Navier-Stokes equations and a multigrid method. Journal of Computational Physics 48, 387-411.

Kristoffersen, R. \& Andersson, H. I. 1989 The three-dimensional liddriven cavity as test case for numerical simulation algorithms. Tech. Rep. STF67 A 89004. SINTEF.

|  | finite volume |  | finite difference |  | lattice Boltzmann |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $z$ | $x$ | $y$ | $x$ | $y$ | $x$ | $y$ |
| 0.05 | 0.621 | 0.803 | 0.623 | 0.813 | 0.626 | 0.800 |
| 0.10 | 0.622 | 0.792 | 0.624 | 0.793 | 0.627 | 0.790 |
| 0.20 | 0.620 | 0.778 | 0.623 | 0.779 | 0.625 | 0.775 |
| 0.30 | 0.618 | 0.768 | 0.620 | 0.769 | 0.622 | 0.765 |
| 0.40 | 0.616 | 0.762 | 0.618 | 0.763 | 0.620 | 0.759 |
| 0.50 | 0.615 | 0.760 | 0.618 | 0.760 | 0.619 | 0.757 |

Table 1: Benchmark: three-dimensional lid driven cavity flow-vortex centres in the $x y$-plane slices for prescribed levels in $z . ~ R e_{\mathrm{w}}=100$. Data from finite volume and finite difference methods are taken form Kristoffersen \& Andersson (1989).

