

Electrokinetically Enhanced Cross-stream Particle Migration in Viscoelastic Flows: Supplementary Material

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I. ADDITIONAL EXPERIMENTAL DETAILS

Here we provide additional details of the experiments carried out. We dissolved polyethylene oxide (PEO, molecular weight = 2×10^6 g/mol, Sigma-Aldrich) powder into a buffer solution (0.01 mM phosphate buffer mixed with 0.5% Tween 20 (Fisher Scientific)) at a concentration of 250 ppm. The particle suspension was prepared by suspending polystyrene spheres (Thermo Scientific) in the viscoelastic solution. The particle concentration was kept low ($< 0.1\%$ in volume fraction) in the fluid, and hence particle-particle interaction and its effect on fluid viscosity can be neglected. The microchannel was primed with the particle-free suspending fluid prior to the introduction of the particle suspension. The microchannel used in the experiment was 2 cm long with a rectangular cross-section of $66 \mu\text{m} \times 54 \mu\text{m}$. Particle motion was visualized at the outlet of the microchannel through an inverted microscope (Nikon Eclipse TE2000U) equipped with a CCD camera (Nikon DS-Qi1MC). Digital videos were recorded at a rate of 15 frames per second, from which the superimposed images were obtained. We further processed these images in the Nikon imaging software (NIS-Elements AR 3.22).

II. RECIPROCAL THEOREM FOR CROSS-STREAM MIGRATION

We follow Ho and Leal [1] to find the migration velocity in this section. The momentum of the unknown $O(De)$ field is governed by

$$\nabla \cdot \boldsymbol{\sigma}_{H(1)} = \mathbf{0}, \quad \text{where } \boldsymbol{\sigma}_{H(1)} = -p_{(1)}\mathbf{I} + (\nabla \mathbf{v}_{(1)} + \nabla \mathbf{v}_{(1)}^T) + \mathbf{s}_{(0)}, \quad (1)$$

where \mathbf{I} is the identity matrix and T denotes transpose. The boundary conditions at the particle surface are

$$\mathbf{v}_{(1)} = \mathbf{U}_{s(1)} + \boldsymbol{\Omega}_{s(1)} \times \mathbf{r} \quad \text{at } r = 1 \quad (2)$$

The test field is chosen to be that generated by a sphere moving in the positive z-direction with a unit velocity in a quiescent Newtonian medium.

$$\nabla \cdot \boldsymbol{\sigma}_t = \mathbf{0}, \quad \text{where } \boldsymbol{\sigma}_t = -p^t\mathbf{I} + (\nabla \mathbf{u}^t + \nabla \mathbf{u}^{tT}). \quad (3)$$

The boundary condition for test field is

$$\mathbf{u}^t = \mathbf{e}_z \quad \text{at } r = 1. \quad (4)$$

Taking the inner product of (1) with \mathbf{u}^t and (3) with $\mathbf{v}_{(1)}$ over the entire fluid domain (from particle surface to infinity) and equating:

$$\int_{V_f} \mathbf{u}^t \cdot (\nabla \cdot \boldsymbol{\sigma}_{H(1)}) dV = \int_{V_f} \mathbf{v}_{(1)} \cdot (\nabla \cdot \boldsymbol{\sigma}_t) dV. \quad (5)$$

A rearrangement provides

$$\int_{V_f} \nabla \cdot (\mathbf{u}^t \cdot \boldsymbol{\sigma}_{H(1)}) dV - \int_{V_f} \boldsymbol{\sigma}_{H(1)} : \nabla \mathbf{u}^t dV = \int_{V_f} \nabla \cdot (\mathbf{v}_{(1)} \cdot \boldsymbol{\sigma}_t) dV - \int_{V_f} \boldsymbol{\sigma}_t : \nabla \mathbf{v}_{(1)} dV. \quad (6)$$

Using Gauss-divergence theorem and rearranging the integrals, we obtain

$$-\int_{S_p} (\mathbf{u}^t \cdot \boldsymbol{\sigma}_{H(1)}) \cdot \mathbf{n} dS + \int_{S_p} (\mathbf{v}_{(1)} \cdot \boldsymbol{\sigma}_t) \cdot \mathbf{n} dS = \int_{V_f} \boldsymbol{\sigma}_{H(1)} : \nabla \mathbf{u}^t dV - \int_{V_f} \boldsymbol{\sigma}_t : \nabla \mathbf{v}_{(1)} dV, \quad (7)$$

where \mathbf{n} is the outward unit vector, normal to the surface. Using the boundary conditions (2) and (4), we write

$$-\mathbf{e}_z \cdot \int_{S_p} \boldsymbol{\sigma}_{H(1)} \cdot \mathbf{n} dS + \mathbf{U}_{s(1)} \cdot \int_{S_p} \boldsymbol{\sigma}_t \cdot \mathbf{n} dS = \int_{V_f} \boldsymbol{\sigma}_{H(1)} : \nabla \mathbf{u}^t dV - \int_{V_f} \boldsymbol{\sigma}_t : \nabla \mathbf{v}_{(1)} dV. \quad (8)$$

The first term on the left hand side in the above equation is zero for a freely suspended neutrally buoyant sphere. Accounting for the leading order wall correction¹, the second term on the left hand side is the hydrodynamic drag which is $-6\pi(1+O(\kappa))U_{sz(1)}$. The $O(\kappa)$ corrections are due to wall effects. Expanding the right hand side, we obtain

$$-6\pi(1+O(\kappa))U_{sz(1)} = \int_{V_f} \left(-p_{(1)}\mathbf{I} + \nabla \mathbf{v}_{(1)} + \nabla \mathbf{v}_{(1)}^T + \mathbf{s}_{(0)} \right) : \nabla \mathbf{u}^t dV - \int_{V_f} \left(-p^t\mathbf{I} + \nabla \mathbf{u}^t + \nabla \mathbf{u}^{tT} \right) : \nabla \mathbf{v}_{(1)} dV. \quad (9)$$

The incompressibility condition results in: $-p(\mathbf{I} : \nabla \mathbf{u}^t) = -p(\mathbf{I} : \nabla \mathbf{u}_{(1)}) = 0$. Upon further simplifications, we obtain (9) as

$$6\pi(1+O(\kappa))U_{sz(1)} = - \int_{V_f} \mathbf{s}_{(0)} : \nabla \mathbf{u}^t dV. \quad (10)$$

Thus, we obtain the migration velocity as

$$De U_{sz(1)} = U_{mig}^H = - \frac{1}{6\pi(1+O(\kappa))} De \int_{V_f} \mathbf{s}_{(0)} : \nabla \mathbf{u}^t dV. \quad (11)$$

Superscript H denotes the hydrodynamic contribution.

III. EVALUATION OF TRANSLATIONAL AND ROTATIONAL VELOCITY

Here we provide the details of evaluation of $U_{sx(0)}$ and $\Omega_{sy(0)}$. To estimate the wall correction, we require the third reflection of velocity field because the particle is absent in the second reflection[3].

¹For $\kappa \ll 1$, the wall correction can be calculated using both method of reflections and the expression provided by Brenner [2, p.246] (originally derived by Hendrik Lorentz *Theoret. Phys.* 1907 1 23). In Section IV, we compare the wall correction, obtained from method of reflections, with [2].

A. Second reflection of the disturbance velocity

In this subsection, we provide the details of the evaluation of ${}_{(2)}\mathbf{v}_{(0)}$. Equations governing the second reflection are

$$\left. \begin{aligned} \nabla \cdot {}_{(2)}\mathbf{v}_{(0)} &= 0, \quad \nabla^2 {}_{(2)}\mathbf{v}_{(0)} - \nabla {}_{(2)}p_{(0)} = \mathbf{0}, \\ {}_{(2)}\mathbf{v}_{(0)} &= Ha\zeta_w (\nabla_{(1)}\psi + \nabla_{(2)}\psi) - {}_{(1)}\mathbf{v}_{(0)} \quad \text{at the walls,} \\ {}_{(2)}\mathbf{v}_{(0)} &\rightarrow \mathbf{0} \quad \text{at } r \rightarrow \infty. \end{aligned} \right\} \quad (12)$$

The solution is determined by the form of non-homogeneity in the boundary condition at the walls. Following the procedure described in Appendix A.1 (main text), the non-homogeneities ($Ha\zeta_w\nabla_{(1)}\psi$, $Ha\zeta_w\nabla_{(2)}\psi$ and ${}_{(1)}\mathbf{v}_{(0)}$) are represented in the outer scale coordinates before applying Faxén's integral transformation. ${}_{(2)}\psi$ is already defined in the integral form (see A10 of main text), whereas ${}_{(1)}\psi$ and ${}_{(1)}\mathbf{v}_{(0)}$ have been defined in the particle scale (A4 and 3.34, respectively). Upon performing Faxén transformation of the non-homogeneities, we find that $\tilde{\nabla}_{(2)}\tilde{\psi}$ has a different integral form in comparison to ${}_{(1)}\tilde{\mathbf{v}}_{(0)}$ and $\tilde{\nabla}_{(1)}\tilde{\psi}$. Therefore, we use superposition and seek ${}_{(2)}\tilde{\mathbf{v}}_{(0)}$ as ${}_{(2i)}\tilde{\mathbf{v}}_{(0)} + {}_{(2ii)}\tilde{\mathbf{v}}_{(0)}$. These components satisfy the following boundary conditions:

$${}_{(2i)}\tilde{\mathbf{v}}_{(0)} = Ha\zeta_w\kappa\tilde{\nabla}_{(1)}\tilde{\psi} - {}_{(1)}\tilde{\mathbf{v}}_{(0)} \quad \text{at the walls,} \quad (13)$$

$${}_{(2ii)}\tilde{\mathbf{v}}_{(0)} = Ha\zeta_w\kappa\tilde{\nabla}_{(2)}\tilde{\psi} \quad \text{at the walls.} \quad (14)$$

Solution to ${}_{(2i)}\tilde{\mathbf{v}}_{(0)}$: In view of the wall boundary condition in (13), ${}_{(1)}\psi$ (A4) and ${}_{(1)}\mathbf{v}_{(0)}$ (3.34) are represented in the outer coordinates (${}_{(1)}\tilde{\psi}$ and ${}_{(1)}\tilde{\mathbf{v}}_{(0)}$) and then Faxén transformation is applied. $\tilde{\psi}_1$ has already been represented in outer coordinates and transformed into integral form (see (A9)); ${}_{(1)}\mathbf{v}_{(0)}$ is represented into outer coordinates and then Faxén's transformation is applied. Various terms present in the expression for ${}_{(1)}\mathbf{v}_{(0)}$ (such as: $1/r$, x^2/r^3 , \dots in (3.34)) are transformed into Faxén's integral form. Upon deriving each term, we obtain the RHS of wall boundary condition (13) as:

$$Ha\zeta_w\kappa\tilde{\nabla}_{(1)}\tilde{\psi} - {}_{(1)}\tilde{\mathbf{v}}_{(0)} = -\frac{1}{2\pi} \left[\begin{aligned} &\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{(i\Theta - \frac{\lambda|\tilde{z}|}{2})} \left(\ell_1 + (\xi^2/\lambda^2) \left(\ell_2 + \frac{\lambda|\tilde{z}|}{2}\ell_3 \right) \right) d\xi d\eta \\ &\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{(i\Theta - \frac{\lambda|\tilde{z}|}{2})} \left(\ell_2 + \frac{\lambda|\tilde{z}|}{2}\ell_3 \right) ((\eta\xi)/\lambda^2) d\xi d\eta \\ &\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{(i\Theta - \frac{\lambda|\tilde{z}|}{2})} \left(\ell_1 + \ell_2 + \left(1 + \frac{\lambda|\tilde{z}|}{2} \right) \ell_3 \right) ((i\xi)/\lambda) \frac{\tilde{z}}{|\tilde{z}|} d\xi d\eta \end{aligned} \right] \quad (15)$$

Here, $\Theta = (\tilde{x}\xi + \tilde{y}\eta)/2$ and $\lambda = (\xi^2 + \eta^2)^{1/2}$. The terms ℓ_1 , ℓ_2 , and ℓ_3 are given by:

$$\begin{aligned} \ell_1 &= \frac{A_1\kappa}{\lambda} + \frac{\kappa^2}{4} \left(C_1 + \frac{D_1}{3} \right) \frac{\tilde{z}}{|\tilde{z}|} - \frac{F_1\kappa^3}{12}\lambda + \frac{5G_1\kappa^3}{12}\lambda, \\ \ell_2 &= \frac{-A_1\kappa}{2\lambda} - \frac{B_1\lambda\kappa^3}{8} + \frac{Ha\zeta_w b_1\lambda\kappa^3}{2} + \frac{F_1\kappa^3}{24}\lambda + \frac{13G_1\kappa^3}{24}\lambda + \frac{E_1\kappa^4\lambda^2}{48} \frac{\tilde{z}}{|\tilde{z}|} - \frac{H_1\kappa^5}{96}\lambda^3, \\ \ell_3 &= \frac{-A_1\kappa}{2\lambda} - \frac{D_1\kappa^2}{12} \frac{\tilde{z}}{|\tilde{z}|} - \frac{5G_1\kappa^3}{8}\lambda. \end{aligned} \quad (16)$$

Following the procedure carried out in Appendix A.1, we assume the form of ${}_{(2i)}\tilde{\mathbf{v}}_{(0)} = \{ {}_{(2i)}\tilde{\mathbf{u}}_{(0)}, {}_{(2i)}\tilde{\mathbf{v}}_{(0)}, {}_{(2i)}\tilde{\mathbf{w}}_{(0)} \}$ as:

$${}_{(2i)}\tilde{u}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \begin{pmatrix} e^{(-\frac{\lambda\tilde{z}}{2})} \left(\ell_4 + \frac{\xi^2}{\lambda^2} (\ell_5 + \frac{\lambda\tilde{z}}{2} \ell_6) \right) \\ + e^{(+\frac{\lambda\tilde{z}}{2})} \left(\ell_7 + \frac{\xi^2}{\lambda^2} (\ell_8 - \frac{\lambda\tilde{z}}{2} \ell_9) \right) \end{pmatrix} d\xi d\eta \quad (17)$$

$${}_{(2i)}\tilde{v}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \begin{pmatrix} e^{(-\frac{\lambda\tilde{z}}{2})} (\ell_5 + \frac{\lambda\tilde{z}}{2} \ell_6) \\ + e^{(+\frac{\lambda\tilde{z}}{2})} (\ell_8 - \frac{\lambda\tilde{z}}{2} \ell_9) \end{pmatrix} \left(\frac{\xi\eta}{\lambda^2} \right) d\xi d\eta \quad (18)$$

$${}_{(2i)}\tilde{w}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \begin{pmatrix} e^{(-\frac{\lambda\tilde{z}}{2})} (\ell_4 + \ell_5 + (1 + \frac{\lambda\tilde{z}}{2}) \ell_6) \\ - e^{(+\frac{\lambda\tilde{z}}{2})} (\ell_7 + \ell_8 + (1 - \frac{\lambda\tilde{z}}{2}) \ell_9) \end{pmatrix} \left(\frac{i\xi}{\lambda} \right) d\xi d\eta \quad (19)$$

Here, the terms $\ell_4, \ell_5, \dots, \ell_9$ are functions of the Fourier variable λ and coefficients (A_1, B_1, C_1 and D_1) defined in eq.3.36 (of main text). The terms $\ell_4, \ell_5, \dots, \ell_9$ in the above equations can be expressed in terms of the known ℓ_1, ℓ_2 , and ℓ_3 . Towards this, we form a system of six equations by substituting (15) into RHS of (13). The LHS of (13) is represented by (17)-(19). Since the integrals on both the sides are identical, we obtain the following linear system of equations:

$$\begin{bmatrix} e^{\frac{s\lambda}{2}} & e^{\frac{s\lambda}{2}} \xi^2/\lambda^2 & -e^{\frac{s\lambda}{2}} s\xi^2/2\lambda & e^{-\frac{s\lambda}{2}} & e^{-\frac{s\lambda}{2}} \xi^2/\lambda^2 & e^{-\frac{s\lambda}{2}} s\xi^2/2\lambda \\ 0 & e^{\frac{s\lambda}{2}} & -e^{\frac{s\lambda}{2}} s\lambda/2 & 0 & e^{-\frac{s\lambda}{2}} & e^{-\frac{s\lambda}{2}} s\lambda/2 \\ e^{\frac{s\lambda}{2}} & e^{\frac{s\lambda}{2}} & e^{\frac{s\lambda}{2}} (1 - s\lambda/2) & -e^{-\frac{s\lambda}{2}} & -e^{-\frac{s\lambda}{2}} & -e^{-\frac{s\lambda}{2}} (1 + s\lambda/2) \\ e^{-\frac{1}{2}(1-s)\lambda} & e^{-\frac{1}{2}(1-s)\lambda} \xi^2/\lambda^2 & e^{-\frac{1}{2}(1-s)\lambda} (1 - s) \xi^2/2\lambda & e^{\frac{1}{2}(1-s)\lambda} & e^{\frac{1}{2}(1-s)\lambda} \xi^2/\lambda^2 & -e^{\frac{1}{2}(1-s)\lambda} (1 - s) \xi^2/2\lambda \\ 0 & e^{-\frac{1}{2}(1-s)\lambda} & e^{-\frac{1}{2}(1-s)\lambda} (1 - s) \lambda/2 & 0 & e^{\frac{1}{2}(1-s)\lambda} & -e^{\frac{1}{2}(1-s)\lambda} (1 - s) \lambda/2 \\ e^{-\frac{1}{2}(1-s)\lambda} & e^{-\frac{1}{2}(1-s)\lambda} & e^{-\frac{1}{2}(1-s)\lambda} (1 + (1 - s) \lambda/2) & -e^{\frac{1}{2}(1-s)\lambda} & -e^{\frac{1}{2}(1-s)\lambda} & -e^{\frac{1}{2}(1-s)\lambda} (1 - (1 - s) \lambda/2) \end{bmatrix} \begin{bmatrix} \ell_4 \\ \ell_5 \\ \ell_6 \\ \ell_7 \\ \ell_8 \\ \ell_9 \end{bmatrix} = \begin{bmatrix} -e^{-\frac{s\lambda}{2}} (\ell_{1b} + (\ell_2 + \frac{\ell_{3b}s\lambda}{2}) \xi^2/\lambda^2) \\ -e^{-\frac{s\lambda}{2}} (\ell_2 + \ell_{3b}s\lambda/2) \\ e^{-\frac{s\lambda}{2}} (\ell_{1b} + \ell_2 + \ell_{3b}(1 + s\lambda/2)) \\ -e^{-\frac{1}{2}(1-s)\lambda} (\ell_{1t} + (\ell_2 + \frac{1}{2}\ell_{3t}(1 - s) \lambda) \xi^2/\lambda^2) \\ -e^{-\frac{1}{2}(1-s)\lambda} (\ell_2 + \frac{1}{2}\ell_{3t}(1 - s) \lambda) \\ -e^{-\frac{1}{2}(1-s)\lambda} (\ell_{1t} + \ell_2 + \ell_{3t}(1 + (1 - s) \lambda/2)) \end{bmatrix} \quad (20)$$

Here, ℓ_{1b}, ℓ_{3b} and ℓ_{1t}, ℓ_{3t} correspond to the boundary condition at the bottom wall $\tilde{z}/|\tilde{z}| < 0$ and the top wall $\tilde{z}/|\tilde{z}| > 0$, respectively.

Solution to ${}_{(2ii)}\tilde{\mathbf{v}}_{(0)}$: Upon substituting ${}_{(2)}\tilde{\psi}$ in (14), we obtain ${}_{(2ii)}\tilde{\mathbf{v}}_{(0)} = \{ {}_{(2ii)}\tilde{u}_{(0)}, {}_{(2ii)}\tilde{v}_{(0)}, {}_{(2ii)}\tilde{w}_{(0)} \}$:

$${}_{(2ii)}\tilde{u}_{(0)} = \frac{Ha\zeta_w\kappa^3}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(e^{(-\frac{\lambda\tilde{z}}{2})} b_2 + e^{(+\frac{\lambda\tilde{z}}{2})} b_3 \right) \left(\frac{i^2\xi^2}{2\lambda} \right) d\xi d\eta \quad (21)$$

$${}_{(2ii)}\tilde{v}_{(0)} = \frac{Ha\zeta_w\kappa^3}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(e^{(-\frac{\lambda\tilde{z}}{2})} b_2 + e^{(+\frac{\lambda\tilde{z}}{2})} b_3 \right) \left(\frac{i^2\xi\eta}{2\lambda} \right) d\xi d\eta \quad (22)$$

$${}_{2(ii)}\tilde{w}_{(0)} = \frac{Ha\zeta_w\kappa^3}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(-e^{(-\frac{\lambda\tilde{z}}{2})} b_2 + e^{(+\frac{\lambda\tilde{z}}{2})} b_3 \right) \left(\frac{\lambda\tilde{z}}{2} \right) \left(\frac{i\xi}{\lambda} \right) d\xi d\eta \quad (23)$$

Combining (17)-(19) and (21)-(23), we obtain the second reflection of velocity field:

$${}_{2}\tilde{u}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(\begin{array}{l} e^{(-\frac{\lambda\tilde{z}}{2})} \left(\ell_4 + \frac{\xi^2}{\lambda^2} \left(\ell_5 + \frac{\lambda\tilde{z}}{2} \ell_6 - \frac{Ha\zeta_w\kappa^3\lambda}{2} b_2 \right) \right) \\ + e^{(+\frac{\lambda\tilde{z}}{2})} \left(\ell_7 + \frac{\xi^2}{\lambda^2} \left(\ell_8 - \frac{\lambda\tilde{z}}{2} \ell_9 - \frac{Ha\zeta_w\kappa^3\lambda}{2} b_3 \right) \right) \end{array} \right) d\xi d\eta, \quad (24)$$

$${}_{2}\tilde{v}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(\begin{array}{l} e^{(-\frac{\lambda\tilde{z}}{2})} \left(\ell_5 + \frac{\lambda\tilde{z}}{2} \ell_6 - \frac{Ha\zeta_w\kappa^3\lambda}{2} b_2 \right) \\ + e^{(+\frac{\lambda\tilde{z}}{2})} \left(\ell_8 - \frac{\lambda\tilde{z}}{2} \ell_9 - \frac{Ha\zeta_w\kappa^3\lambda}{2} b_3 \right) \end{array} \right) \left(\frac{\xi\eta}{\lambda^2} \right) d\xi d\eta, \quad (25)$$

$${}_{2}\tilde{w}_{(0)} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} e^{i\Theta} \left(\begin{array}{l} e^{(-\frac{\lambda\tilde{z}}{2})} \left(\ell_4 + \ell_5 + \left(1 + \frac{\lambda\tilde{z}}{2}\right) \ell_6 - \frac{Ha\zeta_w\kappa^3\lambda\tilde{z}}{2} b_2 \right) \\ - e^{(+\frac{\lambda\tilde{z}}{2})} \left(\ell_7 + \ell_8 + \left(1 - \frac{\lambda\tilde{z}}{2}\right) \ell_9 - \frac{Ha\zeta_w\kappa^3\lambda\tilde{z}}{2} b_3 \right) \end{array} \right) \left(\frac{i\xi}{\lambda} \right) d\xi d\eta. \quad (26)$$

Since the particle is absent in the formulation of even-numbered reflections, the hydrodynamic drag and torque due to even fields vanishes [3]. Thus, the correction to particle translational and rotational velocity arises from the odd-numbered reflections. Hence, we evaluate the next reflection.

B. Third reflection of the disturbance velocity

The equations governing the third reflection are

$$\left. \begin{array}{l} \nabla \cdot \mathbf{v}^{(0)} = 0, \nabla^2 \mathbf{v}_3^{(0)} - \nabla p_3^{(0)} = \mathbf{0}, \\ \mathbf{v}_3^{(0)} = -\mathbf{v}_2^{(0)} \quad \text{at } r = 1, \\ \mathbf{v}_3^{(0)} \rightarrow \mathbf{0} \quad \text{at } r \rightarrow \infty. \end{array} \right\} \quad (27)$$

The particle boundary condition in (27) requires us to calculate ${}_{(2)}\tilde{\mathbf{v}}_{(0)}$ in the vicinity of the particle. Since, ${}_{(2)}\tilde{\mathbf{v}}_{(0)}$ is represented in outer scaled coordinates, the particle surface is equivalent to $\tilde{r} \rightarrow 0$. Upon expanding ${}_{(2)}\tilde{\mathbf{v}}_{(0)}$ about the origin, we obtain:

$${}_{(2)}\mathbf{v}_{(0)}|_{r=1} = \int_0^\infty \left[\begin{array}{l} (2\ell_4 + \ell_5 + 2\ell_7 + \ell_8) \lambda/2 - (2\ell_4 + \ell_5 - \ell_6 - 2\ell_7 - \ell_8 + \ell_9) \lambda^2 \kappa z/4 + \dots \\ 0 \\ (-\ell_4 - \ell_5 - \ell_6 + \ell_7 + \ell_8 + \ell_9) \lambda^2 \kappa x/4 + \dots \end{array} \right] d\lambda \quad (28)$$

Having obtained the boundary condition for $\mathbf{v}_3^{(0)}$ at the particle surface, we use Lamb's method to obtain the third reflection. The resulting solution has a form similar to eq.3.34 (of main text) with coefficients A_3 , B_3 , C_3 and D_3 . These coefficients are in the integral form, owing to the integral form of (28). Since the force-free and torque free arguments require only the coefficients of stokeslet and rotlet field [4, p. 88], here we only report the coefficients A_3 and C_3 for brevity:

$$\begin{aligned} A_3 &= \frac{-3}{4} \int_0^\infty \frac{1}{2} (2\ell_4 + \ell_5 + 2\ell_7 + \ell_8) \lambda d\lambda \\ C_3 &= \frac{1}{4} \int_0^\infty \left(\frac{1}{2} (\ell_4 - 2\ell_6 - \ell_7 + 2\ell_9) \lambda^2 \kappa \right) d\lambda. \end{aligned} \quad (29)$$

Substitution of $\ell_4, \ell_5, \dots, \ell_9$ (obtained from eq.20) into the above equations results in representation of A_3, C_3 in terms of A_1, B_1, C_1 and D_1 :

$$A_3 \equiv A_1 (\kappa W_A) + B_1 (\kappa^3 W_B) + C_1 (\kappa^2 W_C) + D_1 (\kappa^2 W_D) + \dots, \quad (30)$$

$$C_3 \equiv A_1 (\kappa^2 \mathcal{X}_A) + B_1 (\kappa^3 \mathcal{X}_B) + C_1 (\kappa^4 \mathcal{X}_C) + \dots. \quad (31)$$

Here, $\kappa W_A, \kappa^3 W_B, \kappa^2 W_C$ and $\kappa^2 W_D$ represent the wall corrections to hydrodynamic drag due to the reflection of stokeslet, source-dipole, rotlet and stresslet disturbances, respectively. Similarly, $\kappa^2 \mathcal{X}_A, \kappa^3 \mathcal{X}_B$, and $\kappa^4 \mathcal{X}_C$ represent wall correction to the hydrodynamic torque. It should be noted that the form of equations (30)-(31) is valid for a general problem of a particle suspended in wall bounded flow [5]. These equations show that the leading order correction to viscous drag is $O(\kappa)$ (through κW_A) and that to torque is $O(\kappa^2)$ (through $\kappa^2 \mathcal{X}_A$).

C. Evaluation of Translational and Rotational velocity

Translational and rotational velocity of the particle can be found by imposing force-free and torque-free conditions on the particle at $O(De^0)$: $\mathbf{F}_{H(0)} + \mathbf{F}_M = \mathbf{0}$ and $\mathbf{L}_{H(0)} + \mathbf{L}_M = \mathbf{0}$. Since the Maxwell force \mathbf{F}_M acts only along the z-axis ($\sim O(\kappa^4)$) and the torque \mathbf{L}_M is zero, $U_{sx(0)}$ and $\Omega_{sy(0)}$ are found by hydrodynamic force and torque balance in x and y directions, respectively.

The force and torque on a spherical particle can be expressed through the coefficients of stokeslet and rotlet disturbances, respectively. Following Kim and Karrila [4, p. 88], we write the force-free and torque free condition as:

$$F_{Hx(0)} = -4\pi (A_1 + A_3 + \dots) \text{ and } L_{Hy(0)} = -8\pi (C_1 + C_3 + \dots). \quad (32)$$

The coefficients A_1, C_1 and A_3, C_3 are associated with the Lamb's solution of the first reflection of the velocity disturbance (eq.3.36 of main text) and third reflection (30-31), respectively. Substitution of (30) and (31) into (32) results in a system of two equations for: $U_{sx}^{(0)}$ and $\Omega_{sy}^{(0)}$. Imposing the hydrodynamic force and torque to be zero and upon expanding the coefficients A_1, B_1, \dots, H_1 , we obtain:

$$U_{sx(0)} \approx \alpha + \frac{\gamma}{3} - \frac{10\kappa^2\beta W_D}{9(1 + \kappa W_A)}, \quad (33)$$

$$\Omega_{sy(0)} \approx \frac{\beta}{2} - \frac{5\mathcal{X}_D\kappa^3\beta/3}{(1 + \kappa W_A)}. \quad (34)$$

Since the correction to particle velocity is $O(\kappa^2)$ and higher, we neglect the wall contribution to $U_{sx(0)}$ and $\Omega_{sy(0)}$.

D. Order of magnitude of the disturbance velocity field and test field

We substitute the leading order estimates derived in (33-34): $U_{sx(0)} = \alpha + \frac{\gamma}{3}$ and $\Omega_{sy(0)} = \beta/2$ in the coefficients (eq.3.36 main text). We then substitute the coefficients in $(1)\mathbf{v}_{(0)}$ (eq.3.34main text) and $(2)\mathbf{v}_{(0)}$

(eq.24-26). The order of magnitude of reflections of the velocity fields is obtained as:

$${}_{(1)}\mathbf{v}_{(0)} \sim Ha\zeta_p O(1/r^3) + \beta O(1/r^2) + \beta O(1/r^4) + \gamma O(1/r^3) + \gamma O(1/r^5), \quad (35a)$$

$${}_{(2)}\tilde{\mathbf{v}}_{(0)} \sim \beta O(\kappa^2) + Ha\zeta_p O(\kappa^3) + \dots. \quad (35b)$$

In the second reflection, the outer scale coordinate $\tilde{r} \sim O(1)$. Similarly, following the framework of Ho and Leal [5], the order of magnitude of test velocity field can be obtained

$${}_{(1)}\mathbf{u}^t \sim O(1/r) + O(1/r^2), \quad (36a)$$

$${}_{(2)}\tilde{\mathbf{u}}^t \sim O(\kappa) + O(\kappa^3) + \dots. \quad (36b)$$

IV. EVALUATION OF $O(\kappa)$ WALL CORRECTION TO MIGRATION VELOCITY

Here we provide the expression for first order correction to viscous drag (it appears in the denominator of eq-3.26 and eq-3.30 in the main text). The cross-stream migration of the particle generates stokeslet and source dipole disturbances. Eq. (30) showed that the leading order correction to drag arrives as κW_A . Thus, the relationship between non-dimensional cross-stream force and velocity is $F_{mig} = 6\pi(1 + \kappa W_A)U_{mig}$. Here,

$$W_A = \int_0^\infty \frac{-3e^{\lambda(-s)}}{16(-e^\lambda(\lambda^2 + 2) + e^{2\lambda} + 1)} \left(-4e^{\lambda s} - e^{\lambda + 2\lambda s} (\lambda^2(s-1)^2 - 2\lambda(s-1) + 2) \right. \\ \left. + e^{2\lambda s} (\lambda^2 s^2 - 2\lambda s + 2) + e^\lambda (\lambda^2(s-1)^2 + 2\lambda(s-1) + 2) \right. \\ \left. - 2e^{\lambda + \lambda s} (\lambda^2 + 2\lambda + \lambda^3(-(s-1))s + 2) - e^{2\lambda} (\lambda^2 s^2 + 2\lambda s + 2) \right) d\lambda. \quad (37)$$

Fig.1(a) shows that W_A increases near the walls i.e. the migration velocity becomes slower as the particle approaches walls. Using a bispherical coordinate system for a particle approaching a wall, Brenner [2, p.246] reported a similar increase in viscous resistance. He provided an approximate expression for a single wall configuration: $\kappa W_A \approx \frac{9}{8s}\kappa$ (originally derived by Hendrik Lorentz *Theoret. Phys.* 1907 1 23). Fig.1(b) shows a good agreement between our predictions and Brenner [2]. The slight mismatch near $s = 0.5$ is due to the effect of second wall.

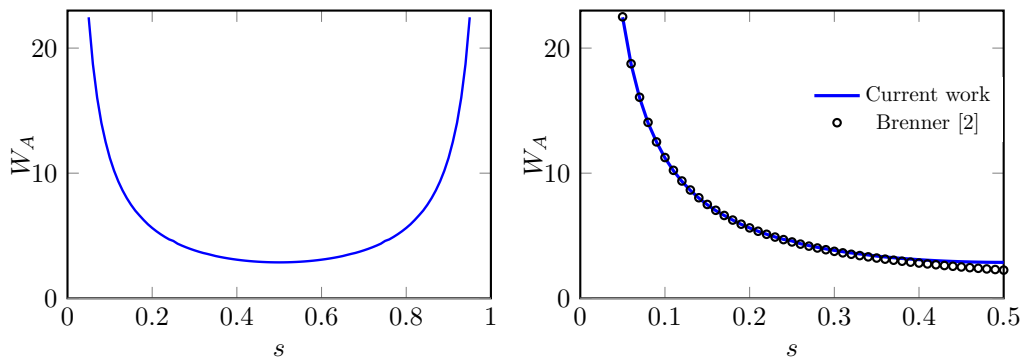


FIG. 1: (a) Variation of leading order viscous resistance to hydrodynamic drag. (b) Comparison with the single wall expression provided by Brenner [2].

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