

FIGURE 1. Instantaneous fields of (a)  $u^T$ , (b)  $v^T$ , and (c)  $w^T$  on the  $x$ - $z$  plane near the bottom (located at  $y/h = 0.015$ ). The results of case 1 are shown.

## A. Instantaneous field of small-scale turbulence

Figure 1 shows the contours of the instantaneous background turbulence velocity fluctuations  $u_i^T$  near the water bottom at  $y/h = 0.015$ . As shown in figure 1(a), the magnitude of  $u^T$  is larger in the D-region than in the H- and U-regions. Moving from the D-region to the U-region, the magnitude of  $u^T$  decreases gradually. Similar to  $u^T$ , as shown in figures 1(b) and 1(c), the intensities of  $v^T$  and  $w^T$  are stronger in the D-region than in the U-region. The results shown in figure 1 indicate that the background turbulence is respectively enhanced and suppressed in the regions with positive and negative large-scale streamwise velocity fluctuations.

Figure 2 shows the contours of  $u_i^T$  in the  $x$ - $z$  plane at  $y/h = 1.985$ . Similar to the observation in the near-bottom region (figure 1a,b), the magnitudes of  $u^T$  and  $v^T$  near the surface are larger in the D-region than in the U-region (figure 2a,b). The localizing effect on the background turbulence spanwise velocity  $w^T$  is different from that on  $u^T$  and  $v^T$  near the water surface. As shown in figure 2(c), the intensities of  $w^T$  in the D- and U-regions are comparable.

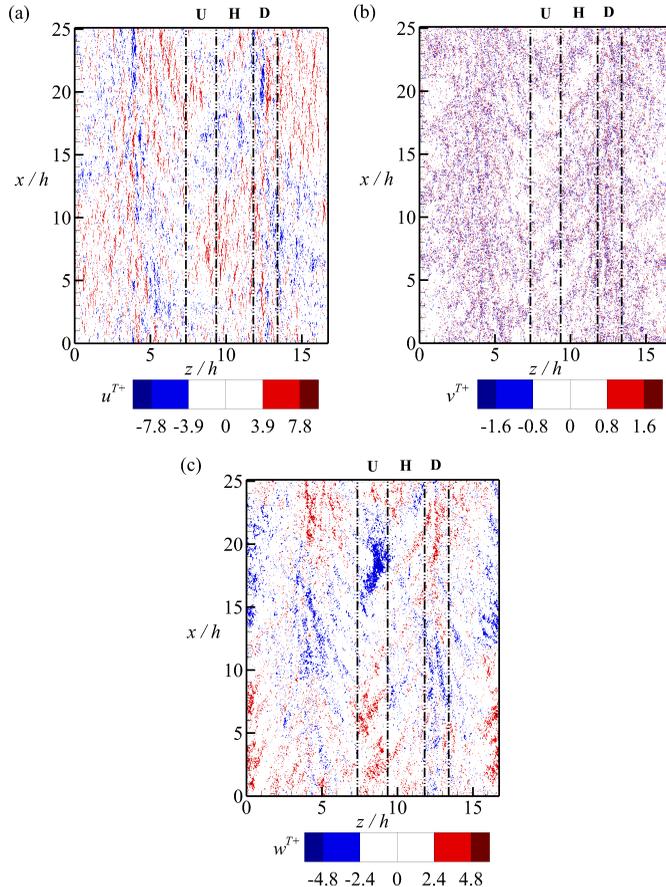


FIGURE 2. Instantaneous fields of (a)  $u^T$ , (b)  $v^T$ , and (c)  $w^T$  on the  $x$ - $z$  plane near the water surface (located at  $y/h = 1.985$ ). The results of case 1 are shown.

## B. Derivation of transport equations of localized Reynolds stresses

According to the triple decomposition of the velocity, the governing equation of the mean velocity  $\langle u_i \rangle$ , the Langmuir cell content velocity fluctuation  $u_i^L$ , and the background turbulence velocity fluctuation  $u_i^T$  can be obtained through the following steps. First, the governing equation of  $\langle u_i \rangle$  is obtained by applying the time and plane averaging to the C-L equation, which is expressed as

$$\langle u_j \rangle \frac{\partial \langle u_i \rangle}{\partial x_j} + \frac{\partial \langle u_i' u_j' \rangle}{\partial x_j} = -\frac{\partial \langle \Pi \rangle}{\partial x_i} + \nu \frac{\partial^2 \langle u_i \rangle}{\partial x_j \partial x_j} + \epsilon_{ijk} u_j^S \langle \omega_k \rangle + \frac{\partial \langle \tau_{ij}^{sgs} \rangle}{\partial x_j}. \quad (\text{B.1})$$

Then, subtracting (B.1) from the C-L equation gives the following governing equation for the total velocity fluctuation  $u_i'$ :

$$\begin{aligned} \frac{\partial u_i'}{\partial t} + u_j' \frac{\partial \langle u_i \rangle}{\partial x_j} + \langle u_j \rangle \frac{\partial u_i'}{\partial x_j} + u_j' \frac{\partial u_i'}{\partial x_j} - \frac{\partial \langle u_i' u_j' \rangle}{\partial x_j} = \\ -\frac{\partial \Pi'}{\partial x_i} + \nu \frac{\partial^2 u_i'}{\partial x_j \partial x_j} + \epsilon_{ijk} u_j^S \omega_k' + \frac{\partial (\tau_{ij}^{sgs})'}{\partial x_j}. \end{aligned} \quad (\text{B.2})$$

The streamwise averaging of (B.2) results in the governing equation for the Langmuir cell content velocity fluctuation  $u_i^L$ , expressed as

$$\begin{aligned} \frac{\partial u_i^L}{\partial t} + u_j^L \frac{\partial \langle u_i \rangle}{\partial x_j} + \langle u_j \rangle \frac{\partial u_i^L}{\partial x_j} + u_j^L \frac{\partial u_i^L}{\partial x_j} - \frac{\partial \langle u_i^L u_j^L \rangle}{\partial x_j} - \frac{\partial \langle u_i^T u_j^T \rangle - \langle u_i^T u_j^T \rangle_x}{\partial x_j} = \\ - \frac{\partial \Pi^L}{\partial x_i} + \nu \frac{\partial^2 u_i^L}{\partial x_j \partial x_j} + \epsilon_{ijk} u_j^S \omega_k^L + \frac{\partial (\tau_{ij}^{sgs})^L}{\partial x_j}. \end{aligned} \quad (\text{B.3})$$

Further subtracting (B.3) from (B.2) gives the following governing equation for the background turbulence velocity fluctuation  $u_i^T$ :

$$\begin{aligned} \frac{\partial u_i^T}{\partial t} + u_j^T \frac{\partial \langle u_i \rangle}{\partial x_j} + \langle u_j \rangle \frac{\partial u_i^T}{\partial x_j} + u_j^L \frac{\partial u_i^T}{\partial x_j} + u_j^T \frac{\partial u_i^L}{\partial x_j} + u_j^T \frac{\partial u_i^T}{\partial x_j} - \frac{\partial \langle u_i^T u_j^T \rangle_x}{\partial x_j} = \\ - \frac{\partial \Pi^T}{\partial x_i} + \nu \frac{\partial^2 u_i^T}{\partial x_j \partial x_j} + \epsilon_{ijk} u_j^S \omega_k^T + \frac{\partial (\tau_{ij}^{sgs})^T}{\partial x_j}. \end{aligned} \quad (\text{B.4})$$

Here,  $\Pi^T = u_j^S u_j^T + p^T$  is the effective pressure and  $\omega_k^T = \epsilon_{knm} \partial u_m^T / \partial x_n$  is the vorticity. To derive the transport equation of  $\langle u_i^T u_j^T \rangle_{xt}$ , the governing equation of  $u_i^T$  is rewritten as

$$\begin{aligned} \frac{\partial u_i^T}{\partial t} + (\langle u_k \rangle + u_k^S) \frac{\partial u_i^T}{\partial x_k} = -u_k^T \frac{\partial \langle u_i \rangle}{\partial x_k} - \frac{\partial p^T}{\partial x_i} - \frac{\partial u_i^T u_k^T}{\partial x_k} + \frac{\partial \langle u_i^T u_k^T \rangle_x}{\partial x_k} \\ + \nu \frac{\partial^2 u_i^T}{\partial x_k \partial x_k} + \frac{\partial (\tau_{ik}^{sgs})^T}{\partial x_k} - u_k^T \frac{\partial u_k^S}{\partial x_i} - u_k^L \frac{\partial u_i^T}{\partial x_k} - u_k^T \frac{\partial u_i^L}{\partial x_k}. \end{aligned} \quad (\text{B.5})$$

To derive (B.5) from (B.4), the two parts of the effective pressure are separated, and the identity  $\epsilon_{ijk} \epsilon_{knm} = \delta_{in} \delta_{jm} - \delta_{im} \delta_{jn}$  is applied. The transport equation of  $u_j^T$  is also obtained by substituting all superscripts  $i$  in (B.5) with  $j$ . Multiply the governing equations of  $u_i^T$  and  $u_j^T$  with  $u_j^T$  and  $u_i^T$ , respectively, and then take the summation of the two resultant equations, we obtain to the following transport equation of  $u_i^T u_j^T$ :

$$\begin{aligned} \frac{\partial u_i^T u_j^T}{\partial t} + (\langle u_k \rangle + u_k^S) \frac{\partial u_i^T u_j^T}{\partial x_k} = -u_j^T u_k^T \frac{\partial \langle u_i \rangle}{\partial x_k} - u_i^T u_k^T \frac{\partial \langle u_j \rangle}{\partial x_k} \\ - \left( \frac{\partial u_j^T p^T}{\partial x_i} + \frac{\partial u_i^T p^T}{\partial x_j} \right) + p^T \left( \frac{\partial u_j^T}{\partial x_i} + \frac{\partial u_i^T}{\partial x_j} \right) \\ - \frac{\partial u_i^T u_j^T u_k^T}{\partial x_k} + \left( u_j^T \frac{\partial \langle u_i^T u_k^T \rangle_x}{\partial x_k} + u_i^T \frac{\partial \langle u_j^T u_k^T \rangle_x}{\partial x_k} \right) \\ + \nu \frac{\partial^2 u_i^T u_j^T}{\partial x_k \partial x_k} + \left( \frac{\partial (\tau_{ik}^{sgs})^T u_j^T}{\partial x_k} + \frac{\partial (\tau_{jk}^{sgs})^T u_i^T}{\partial x_k} \right) \\ - 2\nu \frac{\partial u_j^T}{\partial x_k} \frac{\partial u_i^T}{\partial x_k} - \left( (\tau_{ik}^{sgs})^T \frac{\partial u_j^T}{\partial x_k} + (\tau_{jk}^{sgs})^T \frac{\partial u_i^T}{\partial x_k} \right) \\ - \left( u_j^T u_k^T \frac{\partial u_k^S}{\partial x_i} + u_i^T u_k^T \frac{\partial u_k^S}{\partial x_j} \right) - \frac{\partial u_i^T u_j^T u_k^L}{\partial x_k} - \left( u_j^T u_k^T \frac{\partial u_i^L}{\partial x_k} + u_i^T u_k^T \frac{\partial u_j^L}{\partial x_k} \right). \end{aligned} \quad (\text{B.6})$$

Applying the time and streamwise averaging to (B.6) yields the transport equations of the localized Reynolds stresses  $\langle u_i^T u_j^T \rangle_{xt}$ .

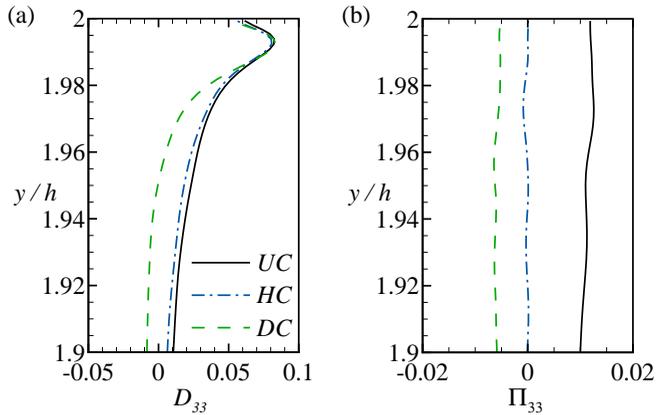


FIGURE 3. Vertical profiles of budget terms (a)  $D_{33}$  and (b)  $\Pi_{33}$  at UC, HC, and DC. The results of case 1 are shown. The budget terms are scaled by  $u_\tau^4/\nu$ .

### C. Comparison of pressure terms in the budget equation of localized spanwise Reynolds normal stress near the surface

Figure 3 compares  $D_{33}$  and  $\Pi_{33}$  among UC, HC, and DC. As shown,  $D_{33}$  is comparable at HC and UC. In contrast,  $\Pi_{33}$  acts as a secondary source at UC, while at HC the contribution of  $\Pi_{33}$  in the budget balance is unimportant.