

Other supplementary materials

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1. Governing equations of two-layer fluids

The governing equations are as follows (Lamb 1932; Sutherland 2010)

$$\frac{\partial \phi_u^2}{\partial x^2} + \frac{\partial \phi_u^2}{\partial y^2} + \frac{\partial \phi_u^2}{\partial z^2} = 0, \quad (1.1)$$

$$\frac{\partial \phi_l^2}{\partial x^2} + \frac{\partial \phi_l^2}{\partial y^2} + \frac{\partial \phi_l^2}{\partial z^2} = 0. \quad (1.2)$$

The kinematics and dynamics boundary conditions at the surface $z = \eta_u$ are

$$\frac{\partial \eta_u}{\partial t} + \nabla \eta_u \cdot \nabla \phi_u - \phi_{u,z} = 0, \quad (1.3)$$

$$\frac{\partial \phi_u}{\partial t} + g\eta_u + \frac{1}{2} \nabla \phi_u \cdot \nabla \phi_u - \frac{\sigma_s}{\rho_u} \nabla \cdot \left[\frac{\nabla \eta_u}{\sqrt{1 + |\nabla \eta_u|^2}} \right] = 0. \quad (1.4)$$

At the interface $z = -h_u + \eta_l$, the boundary conditions yield

$$\frac{\partial \eta_l}{\partial t} + \nabla \eta_l \cdot \nabla \phi_u - \phi_{u,z} = 0, \quad (1.5)$$

$$\frac{\partial \eta_l}{\partial t} + \nabla \eta_l \cdot \nabla \phi_l - \phi_{l,z} = 0, \quad (1.6)$$

$$\frac{\partial \phi_u}{\partial t} + g\eta_l + \frac{1}{2} \nabla \phi_u \cdot \nabla \phi_u + \frac{p_u}{\rho_u} = 0, \quad (1.7)$$

$$\frac{\partial \phi_l}{\partial t} + g\eta_l + \frac{1}{2} \nabla \phi_l \cdot \nabla \phi_l + \frac{p_l}{\rho_l} = 0, \quad (1.8)$$

$$p_l - p_u = -\sigma_i \nabla \cdot \left[\frac{\nabla \eta_l}{\sqrt{1 + |\nabla \eta_l|^2}} \right], \quad (1.9)$$

where ϕ_u (respectively, ϕ_l), ρ_u (respectively, ρ_l), and h_u (respectively, h_l) are the velocity potential, density, and mean depth of the upper (respectively, lower) layer fluid, σ_s (respectively, σ_i) is the surface tension of the air-upper fluid surface (respectively, upper-lower fluid interface), p_u (respectively, p_l) is the interface pressure on the upper (respectively, lower) fluid side, and $\nabla = (\partial/\partial x, \partial/\partial y)$ denotes the gradient operator in the horizontal directions.

At the bottom $z = -h_u - h_l$, the boundary condition is

$$\phi_{l,z} = 0. \quad (1.10)$$

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2. Internal wave of permanent form

The following equations are compiled in Kodaira *et al.* (2016) and summarized here.

2.1. KdV theory

The interface elevation is

$$\eta_l(x) = a_{iw} \operatorname{sech}^2 \left(\frac{x - x_0}{D} \right), \quad (2.1)$$

where

$$D = \sqrt{\frac{12c_2}{a_{iw}c_1}}, \quad (2.2)$$

$$c_0 = \sqrt{\frac{gh_u h_l (1 - R)}{Rh_l + h_u}}, \quad (2.3)$$

$$c_1 = \frac{3c_0}{2h_l} \frac{1 + Rh_u h_l^2 / (c_0^2/g - h_u)^3}{1 + Rh_u h_l / (c_0^2/g - h_u)^2}, \quad (2.4)$$

$$c_2 = \frac{c_0 h_l^2}{6} \frac{1 + R(h_u/h_l) \left[3 + 3h_u / (c_0^2/g - h_u) + h_u^2 / (c_0^2/g - h_u)^2 \right]}{1 + Rh_u h_l / (c_0^2/g - h_u)^2}. \quad (2.5)$$

Before used as the initial condition of our simulation, η_l is subtracted by its mean to match our definition of interface elevation.

The internal wave speed is

$$c_{KdV} = c_0 + \frac{c_1 a_{iw}}{3}. \quad (2.6)$$

2.2. MCC theory

In the MCC theory (Miyata 1985; Choi & Camassa 1996), the surface elevation can be calculated by solving the equation

$$\frac{d\eta_l}{dx} = \sqrt{\frac{3\eta_l^2 [c_{MCC}^2 (R\eta_l + \eta_u) - g(1 - R)\eta_u \eta_l]}{c_{MCC}^2 (Rh_u^2 \eta_l + h_l^2 \eta_u)}}, \quad (2.7)$$

where the internal wave speed is

$$c_{MCC} = c_0 \sqrt{\frac{g(h_u - a_{iw})(h_l + a_{iw})}{gh_u h_l - c_0^2 a_{iw}}}. \quad (2.8)$$

3. Current gradient calculation

A functional is defined to calculate the spatial derivative of the current, following Chartrand (2011):

$$\mathcal{G}(f) = \alpha \int_0^{L_x} |f'|^2 dx + \frac{1}{2} \int_0^{L_x} \left| \int_0^x f(\xi) d\xi - U(x) \right| dx, \quad (3.1)$$

where α is a parameter to control the balance between these two terms. Note that if $\alpha = 0$, the optimal solution would be $f(x) = dU/dx$ in theory.

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