

Analytical solution to the aeroelastic response of a two-dimensional elastic plate in axial potential flow

Online supplementary material

Mathematica script

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Airfoil deformation

M is the order of the Chebychev expansion, which can be set to any arbitrary positive integer. M=4 is shown in this example. Mathematica 11 is used.

```
In[1]:= M = 4;
Do[Tn[n] = ChebyshevT[n, x*], {n, 0, M}];
ψi = 0; Do[ψi = ψi + ci[n]*Tn[n], {n, 0, M}];
w* = ψi*τi[t*];
v* = w* + h*[t*];
Framed[Row[{"v*(x*,t*) = ", v*}]]
```

```
v*(x*,t*) =
(ci[0] + ci[1] x* + ci[2] (-1 + 2 (x*)^2) + ci[3] (-3 x* + 4 (x*)^3) + ci[4] (1 - 8 (x*)^2 + 8 (x*)^4)) τi[t*] +
h*[t*]
```

```
Out[6]=
```

Noncirculatory flow

■ Source/sink strength per unit length

```
In[7]:= σ = 2 (UD[v*, x*] + b f D[v*, t*]);
Framed[Row[{"σ(x*,t*) = ", σ // Simplify}]]
```

```
σ(x*,t*) = 2 (U (ci[1] - 3 ci[3] + 4 (ci[2] - 4 ci[4]) x* + 12 ci[3] (x*)^2 + 32 ci[4] (x*)^3) τi[t*] +
b f ((ci[0] - ci[2] + ci[4] + (ci[1] - 3 ci[3]) x* +
2 (ci[2] - 4 ci[4]) (x*)^2 + 4 ci[3] (x*)^3 + 8 ci[4] (x*)^4) τi'[t*] + (h*)'[t*]))
```

```
Out[8]=
```

■ Velocity potential for source/sink pair

```
In[9]:= (* φnc(x*,t*) =  $\frac{b}{4\pi} \int_{-1}^1 \sigma(x_1^*, t^*) * \text{Log}\left[\frac{(x^* - x_1^*)^2 + (\sqrt{1-x^*^2} - \sqrt{1-x_1^*^2})^2}{(x^* - x_1^*)^2 + (\sqrt{1-x^*^2} + \sqrt{1-x_1^*^2})^2}\right] dx_1^* */)$ 
```

It is easier for Mathematica to evaluate the integral term by term. We tabulate the first M+1 terms.

```

In[10]:= For[n = 0, n ≤ M, n++, Int[n] = Integrate[x_1^{*n} Log[(x^* - x_1^*)^2 + (Sqrt[1 - x^*^2] - Sqrt[1 - x_1^*^2])^2, (x^* - x_1^*)^2 + (Sqrt[1 - x^*^2] + Sqrt[1 - x_1^*^2])^2], {x^*, -1, 1}, Assumptions → {-1 <= x^* <= 1}, PrincipalValue → True] // Factor];
For[n = 0, n ≤ M, n++, Print[Int[n]]]

-2 π √1 - (x^*)^2
-π x^* √1 - (x^*)^2
π (-1 + x^*) (1 + x^*) (1 + 2 (x^*)^2)
3 √1 - (x^*)^2
π (-1 + x^*) x^* (1 + x^*) (1 + 2 (x^*)^2)
4 √1 - (x^*)^2
π (-1 + x^*) (1 + x^*) (3 + 4 (x^*)^2 + 8 (x^*)^4)
20 √1 - (x^*)^2

```

Evaluate the noncirculatory potential.

```

In[12]:= φnc = 0; Do[φnc = φnc + b/(4 π) Int[n] * Coefficient[σ, x^*, n], {n, 0, M}]
Framed[Row[{"φnc(x^*, t) = ", φnc // Simplify}]]

```

```

Out[13]= φnc(x^*, t) =
-1/30 b √1 - (x^*)^2 (30 U (ci[1] - ci[3] + 2 (ci[2] - 2 ci[4]) x^* + 4 ci[3] (x^*)^2 + 8 ci[4] (x^*)^3) τi[t^*] +
b f ((30 ci[0] - 20 ci[2] + 8 ci[4] + 15 (ci[1] - 2 ci[3]) x^* +
4 (5 ci[2] - 14 ci[4]) (x^*)^2 + 30 ci[3] (x^*)^3 + 48 ci[4] (x^*)^4) τi'[t^*] + 30 (h^*)'[t^*])

```

■ Pressure difference for noncirculatory flow (Linearized Bernoulli's equation)

```

In[14]:= Δpnc = 2 ρ (U/b D[φnc, x^*] + f D[φnc, t^*]);
Framed[Row[{"Δpnc(x, t) = ", Δpnc // Simplify}]]

```

```

Out[15]= Δpnc(x, t) =
1
15 √1 - (x^*)^2
ρ (30 U^2 (-2 ci[2] + 4 ci[4] + (ci[1] - 9 ci[3]) x^* + 4 (ci[2] - 8 ci[4]) (x^*)^2 +
12 ci[3] (x^*)^3 + 32 ci[4] (x^*)^4) τi[t^*] +
b f (15 U (-3 ci[1] + 4 ci[3] + 2 (ci[0] - 4 ci[2] + 8 ci[4]) x^* + 4 (ci[1] - 5 ci[3]) (x^*)^2 +
8 (ci[2] - 6 ci[4]) (x^*)^3 + 16 ci[3] (x^*)^4 + 32 ci[4] (x^*)^5) τi'[t^*] + 15 b f (ci[1] - 4 ci[3]) (x^*)^3 τi''[t^*] +
4 b f (5 ci[2] - 26 ci[4]) (x^*)^4 τi''[t^*] + 30 b f ci[3] (x^*)^5 τi''[t^*] +
48 b f ci[4] (x^*)^6 τi''[t^*] + 15 x^* (2 U (h^*)'[t^*] - b f (ci[1] - 2 ci[3]) τi''[t^*]) -
2 b f ((15 ci[0] - 10 ci[2] + 4 ci[4]) τi''[t^*] + 15 (h^*)''[t^*]) +
2 b f (x^*)^2 ((15 ci[0] - 20 ci[2] + 32 ci[4]) τi''[t^*] + 15 (h^*)''[t^*])) )

```

■ Non circulatory lift

```
In[16]:= Lnc = (int[b*Δpnc // Expand]
  // . int[a_ + b_] → int[a] + int[b]
  // . int[i_] → Integrate[i, {x*, -1, 1}, GenerateConditions → False]);
Framed[Row[{"Lnc'(t*) = ", Lnc // Simplify}]]
```

$$\text{Out}[17]= \boxed{\text{Lnc}'(t^*) = -\frac{1}{2} b^2 f \pi \rho (2 U \text{ci}[1] \tau i'[t^*] + b f ((2 \text{ci}[0] - \text{ci}[2]) \tau i''[t^*] + 2 (h^*)''[t^*]))}$$

Circulatory flow

■ Kutta condition at TE

```
In[18]:= (* ∂x*·φc + ∂x*·φnc = finite @ x*=1 *)
```

$$(* K = \frac{1}{2\pi} \int_1^\infty \sqrt{\frac{x_\theta^*+1}{x_\theta^*-1}} \gamma_w(x_\theta^*, t^*) dx_\theta^* *)$$

$$K = \text{Limit}\left[-D[\phi_{nc}, x^*] \frac{\sqrt{1-x^{*2}}}{b}, x^* \rightarrow 1\right];$$

```
Framed[Row[{"K(t*) = ", K // Simplify}]]
```

$$\text{Out}[19]= \boxed{K(t^*) = -U (\text{ci}[1] + 2 \text{ci}[2] + 3 \text{ci}[3] + 4 \text{ci}[4]) \tau i[t^*] - \frac{1}{2} b f ((2 \text{ci}[0] + \text{ci}[1]) \tau i'[t^*] + 2 (h^*)'[t^*])}$$

■ Pressure difference for vortex pair in terms of K and C(k)

```
In[20]:= (* Theodorsen's Function: C(k) = \frac{\int_1^\infty \left(\frac{x\theta}{\sqrt{x\theta^2-1}}\right) \gamma[x\theta, t] dx\theta}{\int_1^\infty \left(\sqrt{\frac{x\theta+1}{x\theta-1}}\right) \gamma[x\theta, t] dx\theta} *)
```

$$\Delta p_c = 2 \rho U K \frac{Ck + x^* (1 - Ck)}{\sqrt{1 - x^{*2}}};$$

```
Framed[Row[{"Δp_c(x^*, t^*) = ", Δp_c // Simplify}]]
```

$$\text{Out}[21]= \boxed{\Delta p_c(x^*, t^*) = \frac{1}{\sqrt{1 - (x^*)^2}} U \rho (-Ck + (-1 + Ck) x^*) (2 U (\text{ci}[1] + 2 \text{ci}[2] + 3 \text{ci}[3] + 4 \text{ci}[4]) \tau i[t^*] + b f ((2 \text{ci}[0] + \text{ci}[1]) \tau i'[t^*] + 2 (h^*)'[t^*]))}$$

■ Circulatory lift force

```
In[22]:= Lc = (int[b*Δpc // Expand]
  // . int[a_ + b_] → int[a] + int[b]
  // . int[i_] → Integrate[i, {x*, -1, 1}, GenerateConditions → False]);
Framed[Row[{"Lc(t*)' = ", Lc // Simplify}]]
```

$$\text{Out}[23]= \boxed{Lc(t^*)' = -b Ck \pi U \rho (2 U (\text{ci}[1] + 2 \text{ci}[2] + 3 \text{ci}[3] + 4 \text{ci}[4]) \tau i[t^*] + b f ((2 \text{ci}[0] + \text{ci}[1]) \tau i'[t^*] + 2 (h^*)'[t^*]))}$$

Total pressure difference

In[24]:= $\Delta p = \Delta p_{nc} + \Delta p_c$;

Framed[Row[{" $\Delta p(x^*, t^*) =$ ", $\Delta p // Simplify$ }]]

Out[25]=

$$\begin{aligned}\Delta p(x^*, t^*) &= \frac{1}{15 \sqrt{1 - (x^*)^2}} \\ &\rho (-1 + x^*) (30 U^2 (2 (ci[2] - 2 ci[4]) + Ck (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4])) + \\ &4 (ci[2] + 3 ci[3]) x^* + 4 (3 ci[3] + 8 ci[4]) (x^*)^2 + 32 ci[4] (x^*)^3) \tau i[t^*] + \\ &b f (15 U (3 ci[1] + Ck (2 ci[0] + ci[1])) - 4 ci[3] + 4 (ci[1] + 2 ci[2] - ci[3] - 4 ci[4]) x^* + \\ &8 (ci[2] + 2 ci[3] - 2 ci[4]) (x^*)^2 + 16 (ci[3] + 2 ci[4]) (x^*)^3 + 32 ci[4] (x^*)^4) \tau i'[t^*] + \\ &30 Ck U (h^*)'[t^*] + b f (1 + x^*) ((30 ci[0] - 20 ci[2] + 8 ci[4] + 15 (ci[1] - 2 ci[3]) x^* + \\ &4 (5 ci[2] - 14 ci[4]) (x^*)^2 + 30 ci[3] (x^*)^3 + 48 ci[4] (x^*)^4) \tau i''[t^*] + 30 (h^*)''[t^*]))\end{aligned}$$

■ Verify Kutta condition: $\Delta p(x^*=1) = \text{finite}$

In[26]:= Framed[Row[{" $\Delta p(x^* \rightarrow 1) =$ ", $\text{Limit}[\Delta p, x^* \rightarrow 1] // Simplify$ }]]

Out[26]=

$$\Delta p(x^* \rightarrow 1) = 0$$

Fluid force of of 2-way coupled aeroelastic model

In[27]:= $\psi j = 0$; Do[$\psi j = \psi j + cj[n] * Th[n]$, {n, 0, M}] ;

$\Delta p^* = \Delta p / (\rho U^2)$;

$Qj^* = \text{int}[\Delta p^* * \psi j // Expand]$

//. int[a_ + b_] \rightarrow int[a] + int[b]

//. int[i_] \rightarrow Integrate[i, {x^*, -1, 1}, GenerateConditions \rightarrow False];

Framed[Row[{" $Qj^*(t^*) =$ ", $Qj^* // Simplify$ }]]

Out[30]=

$$\begin{aligned}Qj^*(t^*) &= -\pi (Ck (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4]) (2 cj[0] - cj[1]) + 3 ci[3] cj[1] + \\ &4 ci[4] cj[1] + 2 ci[2] (cj[1] - cj[2]) - 3 ci[3] cj[3] - 4 ci[4] cj[4]) \tau i[t^*] + \frac{1}{240 U^2} \\ &b f \pi (-120 U (Ck (2 ci[0] + ci[1]) (2 cj[0] - cj[1]) + ci[1] (2 cj[0] + cj[1] - 2 cj[2]) + \\ &2 (ci[2] (cj[1] - cj[3]) + ci[4] cj[3] + ci[3] (cj[2] - cj[4]))) \tau i'[t^*] - \\ &240 Ck U (2 cj[0] - cj[1]) (h^*)'[t^*] + b f ((-30 ci[1] cj[1] + 30 ci[3] cj[1] - 120 ci[0] \\ &(2 cj[0] - cj[2]) + 20 ci[4] cj[2] + 30 ci[1] cj[3] - 45 ci[3] cj[3] - 32 ci[4] cj[4] + \\ &20 ci[2] (6 cj[0] - 4 cj[2] + cj[4]))) \tau i''[t^*] + 120 (-2 cj[0] + cj[2]) (h^*)''[t^*]))\end{aligned}$$

■ Total Lift force

In[31]:= $L = L_{nc} + L_c // Simplify$;

Framed[Row[{" $L'(t^*) =$ ", $\text{Collect}[L, Ck, Simplify]$ }]]

Out[32]=

$$\begin{aligned}L'(t^*) &= b Ck \pi U \rho \\ &(-2 U (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4]) \tau i[t^*] - b f ((2 ci[0] + ci[1]) \tau i'[t^*] + 2 (h^*)'[t^*])) - \\ &\frac{1}{2} b^2 f \pi \rho (2 U ci[1] \tau i'[t^*] + b f ((2 ci[0] - ci[2]) \tau i''[t^*] + 2 (h^*)''[t^*]))\end{aligned}$$

■ Thrust

```
In[33]:= dvdx = D[v^*, x^*];
Tp = (int[b * Δp * dvdx // Expand]
      // . int[a_ + b_] → int[a] + int[b]
      // . int[i_] → Integrate[i, {x^*, -1, 1}, GenerateConditions → False]);
Out[35]= S =  $\frac{\sqrt{2}}{2} K (2 Ck - 1) + \text{Limit}\left[\partial_{x^*} \phi_{nc} \frac{1}{b} \sqrt{1+x^*}, x^* \rightarrow -1\right];$ 
(*Leading-edge suction (von Karman & Burgers 1935)*)
TLES = π ρ b S2;
In[37]:= Framed[Row[{"Tp(t^*) = ", Tp // Simplify}]]
Framed[Row[{"TLES(t^*) = ", TLES // Simplify}]]
```

$$T_p(t^*) = -b \pi \rho \tau i[t^*] \left(2 U^2 (4 (ci[2] + 2 ci[4]))^2 + Ck (ci[1]^2 - 4 ci[2]^2 + 6 ci[1] ci[3] + 9 ci[3]^2 - 16 ci[2] ci[4] - 16 ci[4]^2) \right) \tau i[t^*] + b f (U (ci[1]^2 + 4 ci[2]^2 + 6 ci[3]^2 + Ck (2 ci[0] + ci[1]) (ci[1] - 2 ci[2] + 3 ci[3] - 4 ci[4])) + 8 ci[4]^2 + ci[1] (2 ci[2] - 3 ci[3] + 4 ci[4])) \tau i'[t^*] + 2 Ck U (ci[1] - 2 ci[2] + 3 ci[3] - 4 ci[4]) (h^*)'[t^*] + b f ci[1] (ci[0] \tau i''[t^*] + (h^*)''[t^*]))$$

$$T_{LES}(t^*) = \frac{1}{2} b \pi \rho (2 U (-2 (ci[2] + 2 ci[4])) + Ck (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4])) \tau i[t^*] + b f ((2 Ck ci[0] - ci[1] + Ck ci[1]) \tau i'[t^*] + 2 Ck (h^*)'[t^*])^2$$

■ Power

```
In[39]:= dvdt = f D[v^*, t^*];
P = (int[b2 Δp * dvdt // Expand]
      // . int[a_ + b_] → int[a] + int[b]
      // . int[i_] → Integrate[i, {x^*, -1, 1}, GenerateConditions → False]);
Out[41]= Framed[Row[{"P'(t^*) = ", P // Simplify}]]
```

$$P'(t^*) = -\frac{1}{240} b^2 f \pi \rho (240 U^2 \tau i[t^*] ((-2 ci[2]^2 - 3 ci[3]^2 - 4 ci[4]^2 + ci[1] (2 ci[2] + 3 ci[3] + 4 ci[4])) + Ck (2 ci[0] - ci[1]) (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4])) \tau i'[t^*] + 2 Ck (ci[1] + 2 ci[2] + 3 ci[3] + 4 ci[4]) (h^*)'[t^*]) + b f (120 U (2 ci[0] + ci[1]) (2 Ck ci[0] + ci[1] - Ck ci[1]) \tau i'[t^*]^2 + 120 (h^*)'[t^*] (4 Ck U (h^*)'[t^*] + b f ((2 ci[0] - ci[2]) \tau i''[t^*] + 2 (h^*)''[t^*])) + \tau i'[t^*] (240 U (4 Ck ci[0] + ci[1]) (h^*)'[t^*] + b f ((240 ci[0]^2 + 30 ci[1]^2 - 240 ci[0] ci[2] + 80 ci[2]^2 - 60 ci[1] ci[3] + 45 ci[3]^2 - 40 ci[2] ci[4] + 32 ci[4]^2) \tau i''[t^*] + 120 (2 ci[0] - ci[2]) (h^*)''[t^*])))$$

Summation symbol verifications

```
In[42]:= Σ1i = Sum[i ci[i], {i, 1, M, 1}];  
Σ2i = Sum[(i ci[i]), {i, 2, M, 2}];  
Σ3i = Sum[(i ci[i]), {i, 1, M, 2}];  
Σ4i = Sum[(i/2 ci[i]), {i, 2, M, 2}];  
  
Σ5ji = Sum[i ci[i] cj[i], {i, 1, M}];  
Σ5ii = Sum[i ci[i]^2, {i, 1, M}];  
Σ6ji = Sum[i/(2 (i - 1) (i + 1)) ci[i] cj[i], {i, 2, M}];  
Σ6ii = Sum[i/(2 (i - 1) (i + 1)) ci[i]^2, {i, 2, M}];  
Σ7ji = Sum[1/(4 (i + 1)) (ci[i + 2] cj[i] + ci[i] cj[i + 2]), {i, 1, M - 1}];  
Σ7ii = Sum[1/(2 (i + 1)) (ci[i] ci[i + 2]), {i, 1, M - 1}];  
Σ8ji = Sum[(ci[i + 1] cj[i] - ci[i] cj[i + 1]), {i, 1, M - 1}];
```

■ Lift summation verification

```
In[53]:= Lver = -πρ b^2 (b f^2 (h^*)''[t^*] + 1/2 b (2 ci[0] - ci[2]) f^2 τi''[t^*] + U ci[1] f τi'[t^*]);  
Lver = Lver - 2 πρ U b Ck (b f (h^*)'[t^*] + 1/2 b (2 ci[0] + ci[1]) f τi'[t^*] + U Σ1i τi[t^*]);  
L - Lver // Simplify (* should be zero *)
```

Out[55]= 0

■ Thrust summation verification

```
In[56]:= TLESver = 2 U^2 (Ck Σ1i - 2 Σ4i)^2 τi[t^*]^2;  
TLESver = TLESver + 2 b^2 Ck (Ck (2 ci[0] + ci[1]) - ci[1]) f^2 τi'[t^*] (h^*)'[t^*];  
TLESver = TLESver + 1/2 b^2 (ci[1] - Ck (2 ci[0] + ci[1]))^2 f^2 τi'[t^*]^2;  
TLESver = TLESver + 4 U b Ck (Ck Σ1i - 2 Σ4i) f τi[t^*] (h^*)'[t^*];  
TLESver = TLESver + 2 U b (Ck (2 ci[0] + ci[1]) - ci[1]) (Ck Σ1i - 2 Σ4i) f τi[t^*] τi'[t^*];  
TLESver = TLESver + 2 b^2 Ck^2 f^2 (h^*)'[t^*]^2;  
TLESver = (πρ b) TLESver;  
TLES - TLESver // Simplify (* Should be zero *)
```

Out[63]= 0

```
In[64]:= Tpver = 2 U^2 (4 Σ4i^2 + Ck (Σ3i - Σ2i) Σ1i) τi[t^*]^2;
Tpver = Tpver + 2 Ub Ck (Σ3i - Σ2i) f τi[t^*] (h^*)'[t^*];
Tpver = Tpver + Ub (2 Σ5ii + (Ck (2 ci[0] + ci[1]) - ci[1]) (Σ3i - Σ2i)) f τi[t^*] τi'[t^*];
Tpver = Tpver + b^2 ci[0] ci[1] f^2 τi[t^*] τi''[t^*];
Tpver = Tpver + b^2 ci[1] f^2 τi[t^*] (h^*)''[t^*];
Tpver = -(πρ b) Tpver;
Tp - Tpver // Simplify (* Should be zero *)
```

Out[70]= 0

■ Power summation verification

```
In[71]:= Pver = U^2 (ci[1] Σ1i - Σ5ii + Ck (2 ci[0] - ci[1]) Σ1i) f τi[t^*] τi'[t^*];
Pver = Pver + 2 U^2 Ck Σ1i f τi[t^*] (h^*)'[t^*];
Pver = Pver + 1/2 Ub (2 ci[0] + ci[1]) (Ck (2 ci[0] - ci[1]) + ci[1]) f^2 τi'[t^*]^2;
Pver = Pver + 2 Ub Ck f^2 (h^*)'[t^*]^2;
Pver = Pver + Ub (4 Ck ci[0] + ci[1]) f^2 τi'[t^*] (h^*)'[t^*];
Pver = Pver + b^2 (ci[0]^2 + 1/8 ci[1]^2 - ci[0] ci[2] + Σ6ii - Σ7ii) f^3 τi'[t^*] τi''[t^*];
Pver = Pver + 1/2 b^2 (2 ci[0] - ci[2]) f^3 τi''[t^*] (h^*)'[t^*];
Pver = Pver + 1/2 b^2 (2 ci[0] - ci[2]) f^3 τi'[t^*] (h^*)''[t^*];

Pver = Pver + b^2 f^3 (h^*)'[t^*] (h^*)''[t^*];
Pver = -(πρ b^2) Pver;
P - Pver // Simplify (* Should be zero *)
```

Out[81]= 0

■ Kappa summation verification

```
In[82]:= c = 2 b;
k = π f c / U; (*reduced frequency*)
κm = k^2 / (4 π) (ci[0] cj[0] + 1/8 ci[1] cj[1] - 1/2 (ci[0] cj[2] + ci[2] cj[0]) + Σ6ji - Σ7ji);
κc = k / 4 (Ck (2 ci[0] + ci[1]) (2 cj[0] - cj[1]) + ci[1] (2 cj[0] + cj[1]) + 2 Σ8ji);
κk = π (Ck (2 cj[0] - cj[1]) Σ1i + cj[1] Σ1i - Σ5ji);
μ = k^2 / (8 π) (2 cj[0] - cj[2]);
η = k / 2 Ck (2 cj[0] - cj[1]);
Qjver = -κm τi''[t^*] - κc τi'[t^*] - κk τi[t^*] - μ (h^*)''[t^*] - η (h^*)'[t^*];
Qj* - Qjver // Simplify (* Should be zero *)
```

Out[90]= 0