

Generalization of the Rotne-Prager-Yamakawa mobility and shear disturbance tensors -other supplementary materials

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1. Calculation of integrals for overlapping particles

The configuration of the two spheres i and j and the notation is presented on figure 1. The z axis is chosen in the direction of the vector \mathbf{R}_{ij} connecting the centres of the spheres. The variable \mathbf{r}_i is a position vector from the centre of the sphere i and thus \mathbf{r}' - a position vector from the centre of the sphere j . To demonstrate the method it is enough to calculate explicitly one of the integrals appearing in (3.6)-(3.7) and (3.21)-(3.22). We take the first one,

$$\mathbf{u}^t(\mathbf{R}_{ij}) = \frac{1}{4\pi a^2} \int_{S_i} \mathbf{v}_0^t(\mathbf{r}') d\sigma_i. \quad (1.1)$$

The integration is done over the surface of sphere i , thus \mathbf{r}_i is expressed in spherical coordinates (r, θ, ϕ) associated with sphere i which leads to

$$\mu_{ij}^{tt} = \frac{1}{32\pi^2 \eta} \int_0^{\theta_0} d\theta \sin \theta \int_0^{2\pi} d\phi \frac{1}{r'} \left[\left(1 + \frac{a^2}{3r'^2}\right) \mathbf{1} + \left(1 - \frac{a^2}{r'^2}\right) \hat{\mathbf{r}} \hat{\mathbf{r}}' \right] + \frac{1}{2\zeta^{tt}} \mathbf{1} \left(1 - \frac{R_{ij}}{2a}\right), \quad (1.2)$$

where θ_0 is the meridional angle at which the two spheres intersect (see figure 1), defined by

$$\cos \theta_0 = -\frac{R_{ij}}{2a}, \quad (1.3)$$

and the vector $\mathbf{r}' = \mathbf{R}_{ij} + \mathbf{r}_i$ in the cartesian basis has the form

$$\mathbf{r}' = a \sin \theta \cos \phi \hat{\mathbf{e}}_x + a \sin \theta \sin \phi \hat{\mathbf{e}}_y + (R_{ij} + a \cos \theta) \hat{\mathbf{e}}_z, \quad r'^2 = R_{ij}^2 + 2R_{ij}a \cos \theta + a^2. \quad (1.4)$$

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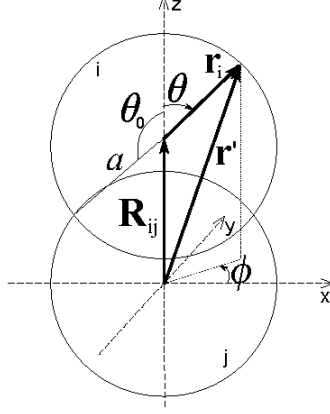


Figure 1. The axes positions and notation for calculation of the expressions for overlapping spheres.

The last term in (1.2) results from integration of the $r \leq a$ expression in (3.2) from θ_0 to π . All the azimuthal integrals in (1.2) are easily done to give

$$\begin{aligned} \mu_{ij}^{tt} = \frac{1}{\zeta^{tt}} \mathbf{1} & \left[\frac{1}{2} \left(1 - \frac{R_{ij}}{2a} \right) + \frac{3}{8} \int_0^{\theta_0} d\theta \sin \theta \left(\frac{a}{r'} + \frac{a^3}{3r'^3} \right) + \frac{3}{16} \int_0^{\theta_0} d\theta \sin^3 \theta \left(\frac{a^3}{r'^3} - \frac{a^5}{r'^5} \right) \right] \\ & + \frac{3}{16\zeta^{tt}} \hat{\mathbf{R}}_{ij} \hat{\mathbf{R}}_{ij} \int_0^{\theta_0} d\theta \sin \theta \left(\frac{a^3}{r'^3} - \frac{a^5}{r'^5} \right) \left[2 \left(\frac{R_{ij}}{a} + \cos \theta \right)^2 - \sin^2 \theta \right], \end{aligned} \quad (1.5)$$

and for the choice of coordinate axes as in figure 1 we have

$$\hat{\mathbf{R}}_{ij} \hat{\mathbf{R}}_{ij} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (1.6)$$

The calculation of μ_{ij}^{tt} is now straightforward. Since

$$\int_0^{\theta_0} d\theta \frac{a \sin \theta}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{1/2}} = 1, \quad (1.7)$$

$$\int_0^{\theta_0} d\theta \frac{a^3 \sin \theta}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{3/2}} = \frac{a}{R_{ij} + a}, \quad (1.8)$$

$$\int_0^{\theta_0} d\theta \frac{a^3 \sin^3 \theta}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{3/2}} = \frac{8a - 3R_{ij}}{12a}, \quad (1.9)$$

$$\int_0^{\theta_0} d\theta \frac{a^5 \sin^3 \theta}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{5/2}} = \frac{-R_{ij}^2 - R_{ij}a + 8a^2}{12a(R_{ij} + a)}, \quad (1.10)$$

$$\int_0^{\theta_0} d\theta \frac{a \sin \theta (R_{ij} + a \cos \theta)^2}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{3/2}} = \frac{3R_{ij} + 4a}{12a}, \quad (1.11)$$

$$\int_0^{\theta_0} d\theta \frac{a^3 \sin \theta (R_{ij} + a \cos \theta)^2}{(R_{ij}^2 + 2R_{ij}a \cos \theta + a^2)^{5/2}} = \frac{R_{ij}^2 + R_{ij}a + 4a^2}{12a(R_{ij} + a)}, \quad (1.12)$$

the tt component of the mobility matrix takes the form

$$\boldsymbol{\mu}_{ij}^{tt} = \frac{1}{\zeta^{tt}} \left[\left(1 - \frac{9R_{ij}}{32a} \right) \mathbf{1} + \frac{3R_{ij}}{32a} \hat{\mathbf{R}}_{ij} \hat{\mathbf{R}}_{ij} \right], \quad (1.13)$$

as in (3.11).