

1371 9. Supplementary Information I: Mild nonuniformity

1372 The applicability of the mild nonuniformity approximation is examined below, in the context
 1373 of the ocean-seafloor system. As discussed in the main text, the acoustic speed in the water
 1374 column is assumed to be a function of the vertical coordinate y , and the pressure wave
 1375 and shear wave phase speeds in the seafloor are assumed to be functions of the horizontal
 1376 coordinates x_1 and x_2 . The speeds are assumed not to be time-dependent. Under the mild
 1377 nonuniformity approximation, the linear (first-order) wave equations can be used, with the
 1378 acoustic speeds appearing as functions the appropriate spatial variables (Whitham 1973).
 1379 Here, some conditions are proposed under which this approximation is justified.

1380 Letting φ represent one of the displacement potentials (ϕ , ϕ' , and H_z) for the acoustic-
 1381 gravity-Scholte wave system, the linear wave equation can be expressed in a self-adjoint form
 1382 as,

$$1383 \quad \frac{\partial^2 \varphi}{\partial t^2} - \nabla \cdot (c_i^2 \nabla \varphi) = 0, \quad (9.1)$$

1384 where $c_l = c_l(x_1, x_2, y)$, represents one of the speeds c_1 , c_p , and c_s and is a function of the
 1385 spatial coordinates. Equation (9.1) expands into,

$$1386 \quad \frac{\partial^2 \varphi}{\partial t^2} - \nabla c_i^2 \cdot \nabla \varphi - c_i^2 \nabla^2 \varphi = 0. \quad (9.2)$$

1387 The media are thought to be mildly nonuniform when the second term in equation (9.1) is
 1388 an order of magnitude smaller than the first and third terms, or,

$$1389 \quad |\nabla c_i^2 \cdot \nabla \varphi| \ll \left| \frac{\partial^2 \varphi}{\partial t^2} \right|, |c_i^2 \nabla^2 \varphi|. \quad (9.3)$$

1390 Specifically, with the seawater acoustic speed $c_1 = c_1(y)$ in the present study, equation (9.2)
 1391 becomes,

$$1392 \quad \frac{\partial^2 \phi}{\partial t^2} - \frac{\partial c_1^2}{\partial y} \frac{\partial \phi}{\partial y} - c_1^2 \frac{\partial^2 \phi}{\partial y^2} = 0. \quad (9.4)$$

1393 For the pressure wave and shear wave speeds $c_p(x_1, x_2)$ and $c_s(x_1, x_2)$ in the seafloor, the
 1394 system becomes,

$$1395 \quad \frac{\partial^2 \phi'}{\partial t^2} - \frac{\partial c_p^2}{\partial x_i} \frac{\partial \phi'}{\partial x_i} - c_p^2 \frac{\partial}{\partial x_i} \left(\frac{\partial}{\partial x_i} \phi' \right) = 0,$$

$$1396 \quad \frac{\partial^2 H_z}{\partial t^2} - \frac{\partial c_s^2}{\partial x_i} \frac{\partial H_z}{\partial x_i} - c_s^2 \frac{\partial}{\partial x_i} \left(\frac{\partial}{\partial x_i} H_z \right) = 0. \quad (9.5)$$

1397 where z is the direction perpendicular to the propagation direction of the wave group and H_z
 1398 is the only non-zero component of the vector potential \mathbf{H} [see (Graff 1991)].

1399 For the acoustic speed nonuniformity $c_1(y)$ in the water column, if

$$1400 \quad \left| \frac{\partial^2 \phi}{\partial t^2} \right|, c_1^2(y) \left| \frac{\partial^2 \phi}{\partial y^2} \right|, c_1(y) \left| \frac{\partial \phi}{\partial y} \right| \sim \mathcal{O}(1),$$

$$1401 \quad \text{then } \left| \frac{\partial c_1(y)}{\partial y} \right| \lesssim \mathcal{O}(10^{-1}) \quad (9.6)$$

1402 is needed. For the well known Munk profile (see Figure 5 and (Munk 1974)), c_1 changes by
 1403 about 60 m/s from its nominal value of 1500 m/s over a depth of 1000 m, so the average
 1404 slope is less than $\mathcal{O}(10^{-1})$. A more exact estimation for $\partial c_1 / \partial y$ for the Munk profile can be

1405 obtained knowing that,

$$c_1(y) = c_{1o}(1 + \epsilon f(y)), \text{ where } \epsilon f(y) = 7.37 \times 10^{-3} \left(-\frac{2(y+1300)}{1300} - 1 + \exp\left(\frac{-2(y+1300)}{1300}\right) \right). \quad (9.7)$$

1406

1407 Calculation of $\epsilon f'(y)$ shows that the mild nonuniformity approximation is satisfied by Munk
 1408 profile when particle oscillations are of $O(10^{-3})$. If particle oscillations become larger than
 1409 this but accelerations and the vertical gradients of particle oscillations do not experience
 1410 equivalent increase, the present approximation may not be able to model accurately the
 1411 propagation through the Munk acoustic speed profile.

1412 Whereas the seafloor propagation speeds c_p and c_s may be difficult to quantify in
 1413 some regions, it is assumed here that complex variations are amenable to expansion using
 1414 polynomial basis functions. Here it is assumed further that the seafloor acoustic speeds vary
 1415 linearly over a distance. Using the following variation for c_p (c_s variation being assumed to
 1416 be similar),

$$c_p(\mathbf{x}) = c_{p0} + \frac{\Delta c_p}{|X_c|} \mathbf{x}, \quad (9.8)$$

1418 where $|X_c|$ is the horizontal distance over which c_p changes by Δc_p . Then,

$$\nabla c_p = \frac{\Delta c_p}{|X_c|} \nabla \cdot \mathbf{x}. \quad (9.9)$$

1419

1420 Now if

$$\left| \frac{\partial^2 \phi'}{\partial t^2} \right|, c_p^2 |\nabla^2 \phi'| \sim O(1), \text{ then}$$

$$|\nabla c_p \cdot \nabla \cdot \phi'| \leq \frac{\Delta c_p}{|X_{c1}|} \left| \frac{\partial \phi'}{\partial x_1} \right| + \frac{\Delta c_p}{|X_{c2}|} \left| \frac{\partial \phi'}{\partial x_2} \right| \quad (9.10)$$

1423 needs to be $\lesssim O(10^{-1})$ for the mild nonuniformity approximation to be valid. For example, if
 1424 speed c_p changes linearly from 5200 m/s to 2800 m/s over 70 km, then $\Delta c_p/|X_c| \sim O(10^{-2})$
 1425 and the present approximation is justified. Similar arguments apply to changes in c_s in the
 1426 horizontal plane.

1427 **10. Supplementary Information II: Purely vertical acoustic-gravity waves**

1428 The seawater acoustic speed variation with y only appears implicitly in S_A , S_W , Π , and S_R
 1429 above through the partial derivatives G_ω and $G_{\omega k_i}$. The effect of $c_1(y)$ on the vertically
 1430 trapped waves can be understood more clearly by considering the case $\mathbf{k} = 0$, or $k_1 = 0$, and
 1431 $k_2 = 0$. The function $G(\omega, \mathbf{k}, \alpha, \alpha', \beta', \mathbf{x}, y)$ then reduces to,

$$1432 \quad G(\omega, \alpha, \alpha', \beta', \mathbf{x}, y) = [(\omega^2 - c_1^2(y)\alpha^2)(1 + F_1(\alpha)) + (\omega^2 - c_p^2(\mathbf{x})\alpha'^2)F_2(\alpha, \alpha', \beta)] \\ 1433 \quad + [(\omega^2 - c_s^2(\mathbf{x})\beta'^2)F_3(\alpha, \alpha', \beta')]. \quad (10.1)$$

1434 For vertical propagation with $\mathbf{k} = 0$, it is found more insightful to use the expansion
 1435 containing dC_1 and dC_2 separately (equation (2.12)) with $k = 0$. In the analysis below, the
 1436 part of the vertical wave system that goes into the seafloor but decays exponentially thereafter
 1437 is neglected. The consistency conditions for downward and upward propagating waves are
 1438 then, respectively,

$$1439 \quad \frac{\partial \alpha}{\partial t} + \bar{C}_\alpha \frac{\partial \alpha}{\partial y} = -\frac{\partial \omega}{\partial y}, \\ 1440 \quad \frac{\partial \alpha}{\partial t} - \bar{C}_\alpha \frac{\partial \alpha}{\partial y} = \frac{\partial \omega}{\partial y}, \quad (10.2)$$

1441 where,

$$1442 \quad \bar{C}_\alpha = \frac{\partial \omega}{\partial \alpha}, \quad (10.3)$$

1443 with the overbar indicating that \bar{C}_α is a vertical energy transfer rate for the downward and
 1444 upward waves, which together make up the vertically trapped component of the acoustic-
 1445 gravity waves.

1446 A variational principle similar to equation (3.10) is proposed for the purely vertical system,
 1447 with,

$$1448 \quad d\mathcal{L} = G(\omega, \alpha, \alpha', \beta', \mathbf{x}, y)dC_1dC_1^* + G(\omega, \alpha, \alpha', \beta', \mathbf{x}, y)dC_2dC_2^*. \quad (10.4)$$

1449 The necessary conditions for the $k = 0$ case then are,

$$1450 \quad \frac{\partial(d\mathcal{L})}{\partial(dC_1)} = 0, \quad \frac{\partial(d\mathcal{L})}{\partial(dC_2)} = 0, \text{ etc.}, \\ 1451 \quad \frac{\partial}{\partial t} \left(\frac{\partial d\mathcal{L}}{\partial \omega} \right) - \frac{\partial}{\partial y} \left(\frac{\partial d\mathcal{L}}{\partial \alpha} \right) = 0. \quad (10.5)$$

1452 For a particular \mathbf{x} , the conditions in the first line of equation (10.5) imply that,

$$1453 \quad G(\omega, \alpha, \alpha', \beta', \mathbf{x}, y) = 0. \quad (10.6)$$

1454 A partial differentiation with respect to α provides,

$$1455 \quad G_\omega \bar{C}_\alpha + G_\alpha = 0, \Rightarrow G_\alpha = -\bar{C}_\alpha G_\omega. \quad (10.7)$$

1456 Following a procedure similar to steps (3.19)–(3.25) independently for dC_1 and dC_2 , for
 1457 the downward component dC_1 ,

$$1458 \quad \frac{\partial}{\partial t} (dC_1dC_1^*) + \frac{\partial}{\partial y} (\bar{C}_\alpha dC_1dC_1^*) + \frac{1}{G_\omega} \left[\frac{\partial G_\omega}{\partial \alpha} \left(-\frac{\partial \omega}{\partial y} \right) + \frac{\partial G_\omega}{\partial y} \bar{C}_\alpha \right] dC_1dC_1^* = 0. \quad (10.8)$$

1459 For the upward component dC_2 ,

$$1460 \quad \frac{\partial}{\partial t} (dC_2dC_2^*) - \frac{\partial}{\partial y} (\bar{C}_\alpha dC_2dC_2^*) + \frac{1}{G_\omega} \left[\frac{\partial G_\omega}{\partial \alpha} \left(\frac{\partial \omega}{\partial y} \right) - \frac{\partial G_\omega}{\partial y} \bar{C}_\alpha \right] dC_2dC_2^* = 0. \quad (10.9)$$

1461 Here,

$$1462 \quad \frac{\partial G_y}{\partial y} = \frac{\partial G}{\partial c_1} \frac{\partial c_1}{\partial y} + \frac{\partial G}{\partial c_1} \frac{\partial c_1}{\partial y}. \quad (10.10)$$

1463 A spectral distribution in terms of the vertical wave-number α can be expressed by dividing
1464 both equations by $d\alpha$ as,

$$1465 \quad \frac{\partial}{\partial t} (S_{C_1}(\alpha)) + \frac{\partial}{\partial y} (\bar{C}_\alpha S_{C_1}(\alpha)) + \frac{1}{G_\omega} \left[\frac{\partial G_\omega}{\partial \alpha} \left(-\frac{\partial \omega}{\partial y} \right) + \frac{\partial G_\omega}{\partial y} \bar{C}_\alpha \right] S_{C_1}(\alpha) = 0. \quad (10.11)$$

1466 For the upward component dC_2 ,

$$1467 \quad \frac{\partial}{\partial t} (S_{C_2}(\alpha)) - \frac{\partial}{\partial y} (\bar{C}_\alpha S_{C_2}(\alpha)) + \frac{1}{G_\omega} \left[\frac{\partial G_\omega}{\partial \alpha} \left(\frac{\partial \omega}{\partial y} \right) - \frac{\partial G_\omega}{\partial y} \bar{C}_\alpha \right] S_{C_2}(\alpha) = 0. \quad (10.12)$$

1468 Equations (10.11) and (10.12) just describe the distribution of upward and downward
1469 moving energy in the wave field trapped between the seafloor and the water surface, for
1470 the purely vertical free acoustic-gravity waves. The effect of acoustic speed dependence on
1471 y is represented by the third and fourth terms in each of the two equations, which capture
1472 change in ω and α for particular (ω, α) pairs and the corresponding distribution rate \bar{C}_α as
1473 the downward and upward components travel through the water column.