

```

=====
#!/usr/bin/python
#
# Python script function to calculate
# the minimum thickness of the gas layer beneath the impacting drop.
#
# Article title: The skating of drops impacting over gas or vapor layers
# Authors: Paula Garcia-Geijo, Guillaume Riboux, Jos\ 'e Manuel Gordillo
# Journal: Journal of Fluid Mechanics
# Date: 2023, October
#
# References:
# [1] J. M. Gordillo & G. Riboux. 2022 The initial impact of drops cushioned by an air
# or vapour layer with applications to the dynamic Leidenfrost regime, J. Fluid Mech.,
# 941, A10:1--19.
# [2] Zhang, Peng & Law, Chung K. 2011 An analysis of head-on droplet collision with l
# arge deformation in gaseous medium. Physics of Fluids 23 (4), 042102.
# [3] Sharipov, Felix, Cumin, Liliana M. Gramani & Kalempa, Denize. 2007 Heat flux bet
# ween parallel plates through a binary gaseous mixture over the whole range of the knud
# sen number. Physica A: Statistical Mechanics and its Applications 378 (2), 183â€"193.

=====
import numpy as np
=====
#
# Inputs:
# prefac (scalar): Prefactor for the hm theoretical expression
# Ts (scalar) : Solid temperature (degree)
# V (array) : Impacting drop velocity (m/s)
# icas (integer) : icas=1 (Capillary regime) - icas=2 (Inertial regime)
#
# Output:
# hth (array) : Theoretical minimum thickness of the gas layour beneath the drop (m
# ).
# xi (array) : Value of the variable xi_bar=taus*xi (-), see eq. (3.16).
# In this case xi_bar is normalized by the value of taus
# in the isothermal case =12.4
#
#
=====
def calcul_rhov(rhov0, rhol, T, V, tau, St):
#
# Function to evaluate the overpressure and vapor density
# see equation (D.1) in [1]
#
#
=====

# Pressure ratio pg/p0 with p0=patm=1e5 and pg=p0+Dpm, see eq. (3.5)
pg_p0=(1.+rhol*(V**2.)*(3.*St**(2./3.)/(8*tau*1e5)));

# Definition of the vapor density as function of temperature
rhov=rhov0*((273+78)/(273+T))*pg_p0;

return (pg_p0, rhov);

=====
def calcul_taus(CC, betas, St):
#
# Determination of the solution of equation (4.13) for tau_start=taus
#
#
=====

# Equation (4.13)
aux=(CC**(5./2.))- (12.4**(3./2.))* (CC+betas*(St**(-1./3.)));

```

```

# Condition in the case there is not solution
index=np.where(aux<=0.0);
if len(index[0])>0:
    Caux=CC[index[0][-1]];
else:
    Caux=float('nan');

# Asignement of the solution of the equation Eq. (4.13) for taus
taus=Caux;

return(taus);

=====
def htheoriq_expr(prefac,icas,tau,St,We,y,R):
#
# Solution of the equation (3.17) in the article.
# prefac (scalar): Prefactor for the hm theoretical expression
# If icas==1 - capillary regime
# If icas==2 - inertial regime
#
=====

if icas==1:
    htheoriq=prefac*R*(tau**(2./3.))*(y**(2./3.))*(St**(-10./9.))*(We**(-1./3.));

if icas==2:
    htheoriq=prefac*R*tau*(St**(-7./6.))*(y**(1./2.));

return(htheoriq);

=====
def htheoriq_gke(prefac,icas,lamb,tau,St,We,DT,L,rhol,rhov,cpv,Prv,R,muv,mua,htheoriq)
:
#
# Function to calculate the solution of the equation (3.17) taking into account
# the gas kinetic effect with equation (4.4)-(4.12). See also ref. [2] and [3]
#
=====

# Minimum relative difference value of haux and htheoriq for the while loop
dhthmin=0.001;

# Initialization of haux and dhth
haux=htheoriq;
dhth=100;

while dhth > dhthmin:
    # Calcul of the Knudsen number with the last value of haux
    Kn=lamb/haux;

    # Calcul of the vapor viscosity (Pa.s) - Gas kinetic effect
    # see ref. [2] and also eq. (4.9)
    muv_kn=muv/(1+6.0966*Kn+0.965*Kn*Kn+0.6967*Kn*Kn*Kn);

    # Calcul of beta and betas - Gas kinetic effect
    # see ref. [3] and eq. (4.12)
    beta=(1./Prv)*(cpv*DT)/L
    betas=beta*(rhol/rhov)*(muv/mua)/(1.+3.91*Kn);

    # Analitical expression for "y", see Eq. (4.6)
    if DT==0:
        betas=0.0;

    y=3.*(muv_kn/mua)*(1.+np.sqrt(1.+(2./3.)*(mua/muv_kn)*betas));

```

```

# Expression for htheoriq, see eq. (3.17)
htheoriq=htheoriq_expr(prefac,icas,tau,St,We,y,R);

# Calculate the difference of haux
dhth=100*abs(haux-htheoriq)/haux;

# New iteration for htheoriq
haux=htheoriq;

# Condition in the case the solution is smaller
# than the mean free path of air
if htheoriq<70e-9:
    htheoriq=float('NaN');
    break;

return(htheoriq,y);

=====
#
#                               MAIN FUNCTION TO CALCULATE hm
#
=====
def calcul_hth(prefac,Ts,V,icas):
#
=====

Ta=25; # Ambient temperature definition (degree)
p0=1e5;# Atmospheric Pressure (Pa)

# Physical properties in the case of ethanol (liquid)
#-----
R=1.1e-3;    # Impacting drop radius (m)
rhol=789;   # Liquid drop density (kg/m^3)
sigma=0.017; # Superficial tension (liquid drop - air) (N/m)
kl=0.167;   # Liquid thermal conductivity (W/(m.K))
mul=1.07e-3; # Drop liquid dynamic viscosity (Pa.s)
L=853e3;   # Latent Heat coefficient (J/kg)
Tb=78;     # Boiling temperature (degree)
Prv=0.96;  # Vapor Prandtl number (-)
Pr=8;      # Prandtl number (-)

# The gas properties are evaluated at temperature
# which is the mean of the boiling temperature of ethanol
# and the solid temperature
#-----
T=0.5*(Tb+Ts);
DT=Ts-Tb; # Solid-boiling difference temperature (degree)

# Physical properties of the ethanol vapor
#-----
lambv0=50e-9; # Mean free path of ethanol vapor at p_atm (m)
rhov0=1.43;  # Vapor density (kg/m^3) appearing in the Eq. (D.1) in ref. [1]
muv0=1.03e-5;
muv=muv0*((273+T)/(273+78))**1.2 # Dynamic viscosity of the vapor (Pa.s)
# in Eq. (D.4) in ref. [1]
cpv=(1830+250*(T-78)/100); # Heat capacity of the vapor (J/(kg. K))
# see Eq. (D.3) in ref. [1]
kv=0.021; # Thermal conductivity of the vapor (W/(m.K))

# Physical properties of the air
#-----
mua0=1.846e-5;
mua=mua0*((T+273)/300)**0.7 # Dynamic viscosity of the air (Pa.s)
# in Eq. (D.5) in ref. [1]

```

```

lamba0=69e-9; # Mean free path of air (m) at p_atm=pa and T=Ta.

# Condition for the isothermal case
if Ts==Ta:
    DT=0;
    mua=mua0;
    muv=mua;
    tau=12.4; # Value of the constant tau, see ref. [1]
    sigma=0.022; # Superficial tension (liquid drop - air) (N/m)

# Initialization of hth and xi variables
xi_bar=float('nan')*np.ones((len(V)));
hth=float('nan')*np.ones((len(V)));

# Loops to calculate the minimum gas thickness
# for each impacting velocity V values and fixed solid Temperature Ts
#
#-----
for i in range(len(V)):

    St=rhol*V[i]*R/mua; # Stokes number for each impact drop velocity
    We=rhol*V[i]*V[i]*R/sigma; # Weber number for each impact drop velocity

    #-----
    # Isothermal cas - Ts=Ta - DT=0
    #-----
    if DT==0:

        # Calcul of pg_p0 at tau=12.4
        [pg_p0, rhov]=calcul_rhov(rhov0, rhol, T, V[i], tau, St);

        # 1/ Solution of the equation (3.11) with tau=taus and Knudsen Kn=0
        # In the case Ts=Ta=25 degree, y=6 and tau=12.4
        #-----
        betas=0.0;
        y=3.*(muv/mua)*(1+np.sqrt(1+(2./3.)*(mua/muv)*betas));

        # Expression for htheoriq (see Eq. (3.17) in the article)
        htheoriq0=htheoriq_expr(prefac, icas, tau, St, We, y, R);

        # 2/ Solution of the equation (3.17) with tau=taus and Knudsen Kn>0
        # where the gas kinetic effect were taken into account.
        # With the value of htheoriq0, we calculate the new value of Kn
        # and converge to the solution haux with a while loop for each
        # impact velocity V
        #-----
        lamb=lamba0*(1./pg_p0); # Mean free path (m)
        # function of the pressure ratio pg/p0

        [htheorique, y]=htheoriq_gke(prefac, icas, lamb, tau, St, We, DT, L, rhol, rhov, cpv, P
rv, R, muv, mua, htheoriq0);

    #-----
    # Leidenfrost - Ts>Ta - DT>0
    #-----
else:
    # 1/ Determination of taus - equation (4.13)
    #-----

    # Initialization of the variable CC~taus
    # for the numerical resolution of equation (4.13)
    # The values of taus should be closer to taus=12.4
    CC=np.array(np.arange(10, 20, 0.1));

    # Calcul of pg_p0, rhov and betas,

```

```

# see eq. (4.4) in the article and eq. (D.1) in ref. [1]
[pg_p0,rhov]=calcul_rhov(rhov0,rhol,T,V[i],CC,St);
beta=(1./Prv)*(cpv*DT)/L;
betas=beta*(rhol/rhov)*(muv/mua);

# Calcul of taus eq. (4.13)
taus=calcul_taus(CC,betas,St);

# 2/ Solution of the equation (3.17) with tau=taus and Knudsen Kn=0
#-----
tau=taus;

# Calcul of pg_p0, rhov, betas at taus obtained before
[pg_p0,rhov]=calcul_rhov(rhov0,rhol,T,V[i],tau,St);
beta=(1./Prv)*(cpv*DT)/L;
betas=(1./Prv)*(cpv*DT)/L*(rhol/rhov)*(muv/mua);

# Analitical expression for "y" (see Eq. (4.6))
y=3.*(muv/mua)*(1.+np.sqrt(1.+(2./3.)*(mua/muv)*betas));

# Expression for htheoriq
# (see Eq. (3.17) with y and taus obtained before)
htheoriq0=htheoriq_expr(prefac,icas,tau,St,We,y,R);

# 3/ Solution of the equation (3.17) with tau=taus and Knudsen Kn>0
# where the gas kinetic effect were taken into account.
# With the value of htheoriq0, we calculate the new value of Kn
# and converge to the solution haux with a while loop for each
# impact velocity V
#-----
lamb=lambv0*(1/pg_p0)*((273+T)/(273+Ta)); # Mean free path (m)
# as function of the temperature T and
# the pressure ratio pg/p0

[htheorique,y]=htheoriq_gke(prefac,icas,lamb,tau,St,We,DT,L,rhol,rhov,cpv,P
rv,R,muv,mua,htheoriq0);

#-----
# Final asignement of the solution for hth and xi
# as function of the impacting drop velocity V and solid temperature Ts
#-----
xi_bar[i]=(tau/12.4)*We*(St**(-1./6.))*(y**(-1./2.));
hth[i]=htheorique;

return(xi_bar,hth);

#=====

```